## BM <br> BARRETT MAHONY <br> CONSULTING ENGINEERS <br> CIVIL \& STRUCTURAL



Proposed Strategic Housing Development on the Former Player Wills Site and Undeveloped Land Owned by Dublin City Council at South Circular Road, Dublin 8.
Structural Assessment Report for Planning

| Barrett Mahony Consulting Engineers |  |  |
| :--- | :---: | :---: |
| Civil. Structural . Project Management |  |  |
| Offices: Dublin, London | DOCUMENT | PAGE |
| Sandwith House, $52-54$ Lower Sandwith Street, Dublin 2, Ireland. | LEAD | $\mathbf{1}$ |
| Tel: (01) 6773200 Fax: (01) 6773164 Email: bmce@bmce.ie Web: www.bmce.ie | OF | $\mathbf{1 8 2}$ |
|  |  |  |

PROJECT:
PROPOSED STRATEGIC HOUSING DEVELOPMENT ON THE FORMER PLAYER WILLS SITE AND UNDEVELOPED LAND OWNED BY DUBLIN CITY COUNCIL AT SOUTH CIRCULAR ROAD, DUBLIN 8.

PROJECT NO.
19.117

DOCUMENT TITLE: STRUCTURAL ASSESSMENT REPORT FOR PLANNING

DOCUMENT NO:
19.117 - PWFR - 01

| Issue | Date | Description | Orig. | PE | PD | Issue <br> Check |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PL1 | $06 / 11 / 2020$ | ISSUE FOR PLANNING | CV | COR | CK | COR |
| PL2 | $11 / 12 / 2020$ | ISSUE FOR PLANNING | CV | COR | CK | COR |

```
STRUCTURAL ASSESSMENT REPORT
                    FOR
PROPOSED PLAYER WILLS SHD
                                    AT
    SOUTH CIRCULAR ROAD,
                DUBLIN 08
```


## TABLE OF CONTENTS

1.0 INTRODUCTION ..... 4
1.1 INTRODUCTION ..... 4
1.2 Existing Structure ..... 6
2.0 STRUCTURAL INVESTIGATIONS ..... 8
2.1 Steel Frame ..... 8
2.1.1 Steel Sections and Properties ..... 8
2.1.2 Ground and First Floor Internal Columns ..... 8
2.1.3 Second Floor Internal Columns ..... 8
2.1.4 Perimeter Steel Frame ..... 9
2.1.5 First and Second Floor Beams ..... 9
2.1.6 Third (roof) Floor Beams ..... 9
2.2 SLAB ON GRADE ..... 9
2.3 SUSPENDED SLABS ..... 10
2.3.1 First and Second Floor Slabs ..... 10
2.3.2 Third (roof) Slab ..... 10
2.4 FOUNDATIONS ..... 10
3.0 FINDINGS AND RECOMMENDATIONS ..... 12
3.1 Findings ..... 12
3.2 RECOMMENDATIONS ..... 12

## APPENDICES

## APPENDIX A

Photographs

## APPENDIX B

Existing Structure Mark-up

## APPENDIX C

Proposed Additional Level Structure

## APPENDIX D

United Metal Investigation Works

## APPENDIX E

McFarland Consulting Façade Steelwork Survey

## APPENDIX F

Load Test Solutions Material Testing

### 1.0 INTRODUCTION

### 1.1 INTRODUCTION

DBTR-SCR1 Fund, a Sub-Fund of the CWTC Multi Family ICAV intend to apply to An Bord Pleanála for permission for a mixed-use Build to Rent Strategic Housing Development at the former 'Player Wills' site ( 2.39 hectares) and adjoining lands ( 0.67 hectares) under the control of Dublin City Council. A public park, public road and works to South Circular Road and to facilitate connections to municipal services at Donore Avenue are proposed on the Dublin City Council land. The former 'Player Wills' site incorporates Eircode's: D08 T6DC, D08 PW25, D08 X7F8 and D08 EK00 and has frontage onto South Circular Road, St. Catherine's Avenue and Donore Avenue, Dublin 8. The Dublin City Council undeveloped land adjoins the former 'Player Wills' site to the west and the former 'Bailey Gibson' site to the east. The total area of the proposed development site is 3.06 hectares.

The design rationale is to create and deliver a high quality, sustainable, residential led mixed use strategic housing development within this inner city brownfield site which respects its setting and maximises the site's natural attributes while achieving maximum efficiency of existing infrastructure. The Proposed Site Layout is illustrated on Drawing No. PL0003 contained within the architectural suite of drawings.

The development will consist of;
i. the demolition of all buildings ( 15,454 sq.m GFA), excluding the original fabric of the former Player Wills Factory, to provide for the development of a mixed use(residential, community, arts and culture, creche, food and beverage and retail) scheme comprising predominantly build to rent apartment dwellings (492 no.) together with a significantly lesser quantity of single occupancy shared accommodation private living areas ( 240 no.), with an average private living floor area of 24.6 sq.m (double the minimum private living space size required for single occupancy shared accommodation) and a arts/culture/community hub within the repurposed ground floor of the former factory building;
ii. change of use, refurbishment, modifications and alterations to the former Player Wills Factory building (PW1) to include the removal of 1 no. later addition storey (existing 4th storey) and the later addition rear (northern) extension, retention and modification of 3 no. existing storeys and addition of 2 no. storeys set back on the building's south, east and west elevations with an 8 -storey projection (max. height 32.53 m ) on the north eastern corner, with a cumulative gross floor area of 17,630 sq.m including ancillary uses, comprising;
a. at ground floor 852 sq.m of floor space dedicated to community, arts and cultural and exhibition space together with artist and photography studios (Class 1 and Class 10 Use), 503 sq.m of retail floor space (Class 1 Use), 994 sq.m of café/bar/restaurant floor space, 217 sq.m of co-working office floor space (Class 3 Use) and ancillary floor space for welfare facilities, waste management and storage;
b. 240 no. single occupancy shared accommodation private living areas, distributed over levels 1-4, including 2 no. rooms of 30 sq.m, 49 no. rooms of 25 sq.m; 14 no. rooms of 23 sq.m, 58 no. rooms of 22.5 sq.m, 8 no. rooms of 20 sq.m, 104 no. rooms of 19 sq.m and 5 no. disabled access (Part M) rooms ( 3 no. 32 sq.m and 2 no. 26 sq.m); 21 no. kitchen/dining areas, and, 835 sq.m of dedicated shared accommodation services, amenities and facilities distributed across levels 1-4, to accommodate uses including lounge areas, entertainment (games) area, 2 no.
external terraces (Level 03 and 04), laundry facilities, welfare facilities and waste storage;
c. 47 no. build-to rent apartments distributed across levels 1-7 including 12 no. studio apartments; 23 no. 1 bed apartments, 8 no. 2 bed apartments: and, 4 no. 3-bed apartments;
d. 1,588 sq.m of shared (build to rent and shared accommodation) services, amenities and facilities including at ground floor reception/lobby area, parcel room, 2 no. lounges and administration facilities; at Level 01 entertainment area, TV rooms, entertainment (games room), library, meeting room, business centre; at Level 02 gym and storage and at Level 07, a lounge area.
e. Provision of communal amenity outdoor space as follows; PW1-450 sq.m in the form of roof terraces dedicated to shared accommodation and 285 sq.m roof terrace for the proposed apartments .
f. a basement ( 190 sq.m) underlying the proposed 8 -storey projection to the northeast of PW1 to accommodate plant.
iii. the construction of 445 no. Build to Rent apartment units, with a cumulative gross floor area of 48,455 sq.m including ancillary uses distributed across 3 no. blocks (PW 2, 4 and 5) comprising;
a. PW2 ( 45,556 sq.m gross floor area including ancillary uses) -415 no. apartments in a block ranging in height from 2-19 storeys (max. height 63.05m), incorporating 16 no. studio units; 268 no. 1 bed apartments, 93 no. 2 bed apartments and 38 no. 3-bed apartments. At ground floor, 2 no. retail unts (combined 198 sq.m) (Class 1 use), and a café/restaurant ( 142 sq.m). Tenant services, amenities and facilities (combined 673 sq.m) distributed across ground floor (lobby, mail room, co-working and lounge area), Level 06 (terrace access) and Level 17 (lounge). Provision of communal amenity open space including a courtyard of 1,123 sq.m and roof terraces of $1,535 \mathrm{sq} . \mathrm{m}$
b. Double basement to accommodate car parking, cycle parking, waste storage, general storage and plant.
c. PW4 (1,395 sq.m gross floor area including ancillary uses) - 9 no. apartments in a part 2-3 storey block (max. height 10.125 m ) comprising, 2 no. 2-bed duplex apartment units and 7 no. 3-bed triplex apartment units. Provision of communal amenity open space in the form of a courtyard 111 sq.m
d. PW5 (1,504 sq.m gross floor area including ancillary uses) -21 no. apartments in a 4 storey block (max. height 13.30 m ) comprising 12 no. studio apartments, 1 no. 1-bed apartment, 5 no. 2-bed apartments, and 3 no. 3-bed apartments. Provision of communal amenity space in the form of a courtyard 167sq.m. Provision of communal amenity open space in the form of a courtyard 167 sq.m
iv. the construction of a childcare facility (block PW4) with a gross floor area of 275 sq.m and associated external play area of 146 sq.m;
v. the provision of public open space with 2 no. permanent parks, 'Players Park' ( 3,960 sq.m) incorporating active and passive uses to the northwest of the former factory building on lands owned by Dublin City Council; 'St. Catherine's Park' (1,350 sq.m)a playground, to the north east of the Player Wills site adjacent to St. Catherine's National School. A temporary public park ( $1,158 \mathrm{sq} . \mathrm{m}$ ) to the northeast of the site set aside for a future school extension. The existing courtyard ( 690 sq.m) in block PW1 (former factory building) to be retained and enhanced and a public plaza ( 320 sq.m) between proposed blocks PW and PW4.
vi. $\quad 903$ no. long-stay bicycle parking spaces, with 861 no. spaces in the PW2 basement and 42 no. spaces at ground level in secure enclosures within blocks PW4 and PW5. 20 no. spaces reserved for non-residential uses and 110 no. short-stay visitor bicycle spaces provided at ground level.
vii. 4 no. dedicated pedestrian access points are proposed to maximise walking and cycling, 2 no. from South Circular Road, 1 no. from St. Catherine's Avenue and 1 no. from Donore Avenue.
viii. in the basement of PW2, 148 no. car parking spaces to serve the proposed build to rent apartments including 19 no. dedicated disabled parking spaces and 6 no. motorcycle spaces. 20 no. spaces for a car sharing club ('Go Car' or similar). $10 \%$ of parking spaces fitted with electric charging points.
ix. in the basement of PW2, use for 81 no. car parking spaces ( 1,293 sq.m net floor area) including 5 no. dedicated disabled parking spaces, 3 no. motorcycle spaces and $10 \%$ of parking spaces fitted with electric charging points to facilitate residential car parking associated with future development on neighbouring lands. The area will not be used for carparking without a separate grant of permission for that future development. In the alternative, use for additional storage (cage/container) for residents of the proposed development.
x. $\quad 37$ no. surface level car parking spaces including 3 no. disabled access and 3 no. creche set down spaces and 10\% fitted with electric charging points. 2 no. loading bays and 2 no. taxi set-down areas.
xi. development of internal street network including a link road ( 84 m long x 4.8 m wide) to the south of the proposed 'Players Park' on land owned by Dublin City Council that will provide connectivity between the former 'Bailey Gibson' site and the 'Player Wills' site.
xii. vehicular access will be provided via Donore Avenue with a one-way exit provided onto South Circular Road to the east of block PW1(the former factory building);
xiii. replacement and realignment of footpaths to provide for improved pedestrian conditions along sections of Donore Avenue and South Circular Road and realignment of centreline along sections of Donore Avenue with associated changes to road markings;
xiv. a contra-flow cycle lane is proposed at the one-way vehicular exit to the east of PW1 (former factory building) to allow 2-way cycle movements via this access point;
xv. decommissioning of existing 2 no. ESB substations and the construction of 2 no. ESB substations and associated switch rooms, 1 no. single ESB substation in PW 1 ( 43.5 sq.m) and 1 no. double ESB substation in PW2 (68 sq.m);
xvi. the construction of a waste and water storage building (combined 133 sq.m, height 4.35 m ) to the west of building PW1;
xvii. all ancillary site development works; drainage, rooftop solar photovoltaics ( 20 no. panels total), landscaping, boundary treatment and lighting.

This report focuses on the existing factory building, referenced as block PW1, the majority of which is proposed to be retained and integrated into the new development.

### 1.2 Existing Structure

The factory building structure consists of a masonry clad steel frame with insitu concrete slabs. The building was constructed in a number of phases dating from 1924-1949. The original building was a two-storey structure, with an additional level constructed in stages between the 1920 and 1930s. The third storey maintains the structural grid of the levels below, with a reduction in the column sizes to that of the lower floors. Also, in the late 1920's the building was extended to the north, with the internalization and removal of a significant portion of the original northern façade. The fourth storey, constructed in 1949, covers only part of the building footprint and does not maintain the same structural grid. This forth level is proposed to be demolished. Refer to Figure 1.1.


Figure 1.1 - Player Wills Factory - Construction Stages.
At the time of BMCE's appointment, the factory building had been derelict for some time. The building roof drainage outlets were blocked almost throughout and waterproof membranes on the roof had failed, leading to significant water ingress and associated deterioration of both structural and non-structural elements (refer to Photos 1-10 in Appendix A). In addition, the factory contained a high proportion of Asbestos Containing Materials (ACM's). No design or as-built information was available in relation to the building structure.

A large-scale asbestos remediation project was carried out on the building, along with an initial strip out, removal of all non-structural partitions from within the building, to allow better assessment of the original building structure.

Upon completion of those works, a schedule of structural opening-up works and fabric testing was prepared to allow a structural assessment of the building be carried out. The following testing was carried out over a number of months:

- Exposure of existing pad and strip footings at all typical locations.
- Concrete core sampling and compressive testing of suspended slabs at levels 1,2 \& 3 .
- Slabs exposures at levels $1,2 \& 3$ to determine slab depths, reinforcement details, cover.
- Steel sampling from typical columns and beams on all floors for strength tensile testing and metallurgy analysis (some testing ongoing).
- Surveying of the brick and concrete encased steel structure within the external brick façade.
- Cathodic protection trials of encased steel subsequently (ongoing).

Investigation works pertaining to the primary structural elements are discussed in more detail below. At the time of preparation of this report, some of the investigations into the external façade are ongoing. A mark-up of our findings of the primary steel frame is provided in Appendix B.

### 2.0 STRUCTURAL INVESTIGATIONS

This section discusses the various structural investigation works which have been carried out to enable an assessment of the existing structure and subsequently design for the proposed new building. Refer to the following appendices for further details of these opening up and testing regime:

- Appendix D - United Metals Investigation Works;
- Appendix E - McFarland Consulting Façade Steelwork Survey
- Appendix F - Load Test Solutions Material Testing.


### 2.1 Steel Frame

### 2.1.1 Steel Sections and Properties

Due to the age of the structure, the steel sections sizes are not standard section sizes as used today. To establish section properties, dimensional measurements were carried out to compare the steel sections against historical imperial size section tables. At the time of construction of this building, the use of mild steel had started to become commonplace but cast iron and wrought iron steel was still available as a structural building product (refer to Photos 11-15 for images of the steel structure). To establish definite material properties, a number of steel samples were taken from external façade columns, internal columns and beams, over a number of floors, due to the different construction stages. The results of this testing confirmed that the steel used to construct this building was mild steel, generally comparable in its material properties to that commonly in use today, although to a lower design strength than typically adopted in modern construction. The results for the steel testing can be seen in Appendix F.

### 2.1.2 Ground and First Floor Internal Columns

The ground floor columns are 180 mm diameter solid steel sections and the first floor columns are 160 mm diameter solid steel sections. Initial testing of the steel concluded that it is mild steel, however tensile testing indicate that the steel grade for these columns is less than the expect S235. Three tests across various columns indicate the steel stress capacity is $215 \mathrm{~N} / \mathrm{mm}^{2}$. Our calculations show that these columns are sufficient for the proposed new building loads above, including the additional levels based on the lightweight form of construction as discussed in Section 3.2 below

### 2.1.3 Second Floor Internal Columns

The roof over the second floor (third floor) was constructed in two separate phases. The earlier phase consisted of the west wing of the building north of the first three bays back from the South Circular Road. This was built in the late 1920's and here the columns are 100 mm diameter solid steel sections. These columns do not have the capacity to support the proposed additional levels due to their slender cross section. These columns will need to be replaced to provide sufficient capacity for support of the proposed additional floors.

The remainder of the roof over the second floor (third floor) was constructed in the 1930's, and here the columns are universal beam sections to historic imperial section tables. Testing confirms the applicable strength grade as S235. Calculations carried out to date show that these columns are also insufficient in strength to cater for the proposed extended building loads, and they will need to be replaced to provide sufficient capacity for support of the proposed additional floors.

### 2.1.4 Perimeter Steel Frame

During the investigations, it was discovered that the external brick façade piers encase structural steel columns, and that the concrete lintels are an encasement to structural steel beams (refer to Photos 16-20 in Appendix A). Corrosion of the steelwork was noted in the initial opening up works and the results of this initial opening up can be seen in Appendix E. As a result, specialist cathodic protection testing has been commissioned so as to investigate its effectiveness of protecting the steel within the facade. This is to establish if this method of corrosion protection will be successful in preventing further corrosion of the structural steelwork, which would affect its loadbearing capacity, and also result in expansive corrosion having deleterious effects on the encasing brick façade. This cathodic protection testing has commenced and a report outlining the findings and long term corrosion protection for the encased steel elements will be produced upon completion of the testing.

Upon completion of this testing, an analysis of the perimeter steelwork for the proposed development will be undertaken, and any strengthening works required identified. Where any invasive works are required to strengthen the steelwork within the façade, this work will primarily be carried out from within the building.

### 2.1.5 First and Second Floor Beams

The first and second floor beams are generally identical in layout and section size. Tensile testing indicates that a strength grade of at least S235 could be used, and up to S275 in place. Calculations show that these beams are sufficient for the proposed new building loads at level 1 and 2, including the higher loaded areas (communal and gym area).

### 2.1.6 Third (roof) Floor Beams

As noted in Section 2.1.3, the third level was constructed in two phases, after the main building was complete. Both primary and secondary beam sizes (in both phases) at this level are smaller than that of the floor below. Tensile testing indicates that a strength grade of S275. Calculations show that these beams are insufficient for the proposed new building loads.

The primary beams would have to be significantly strengthened to support the transferred columns for the proposed new structure above. These strengthening works would likely be invasive, result in major alterations to the original structure. Additional secondary transfer beams would be required at the lines of support for the new structure above, and to supplement the existing secondary beams so as to reduce the load per beam.

### 2.2 Slab ON Grade

A number of ground floor slab exposures were carried out. To do this, in conjunction with footing exposures, the slab was locally saw-cut and removed to expose typical cross sections of the slab. The existing ground floor slab consists of a 180 mm thick slab (thickness varies slightly due to variable subgrade levels) over a crushed rock base (refer to Photo 21-22 in Appendix A). The slab does not have either a radon barrier or damp-proof membrane in place. It also does not have any insulation. All of the above was expected given the age of the structure. To comply with the requirement of current building regulations, along with necessary works to install new drainage and other sub-floor services, it will be necessary to remove the existing ground floor slab and replace this will a new slab with a compliant radon and damp-proof membrane and insulation.

### 2.3 SuSPENDED SLABS

Local opening of the existing slabs (approximately $500 \mathrm{~mm} * 500 \mathrm{~mm}$ ) was carried out at each area related to a different construction period. The concrete around the reinforcement was broken away to identify the type, spacing and size of the reinforcement, along with concrete cover for determination of exposure and fire rating capacity (refer to Photos 23-27 in Appendix A). Concrete core samples were taken for compressive testing. Several samples of the reinforcement were also taken for tensile testing.

Non-structural screed containing timber batons at regular spacings have been cast above the structural slabs on levels 1 and 2 . Given that the building was exposed to years of wet and damp conditions, these timber batons have rotted. To ensure the new construction is not subject to the potential effects of leaving these screeds in place, the screeds shall be removed and replaced with new non-structural floor screeds.

### 2.3.1 First and Second Floor Slabs

The first and second floor slabs consist of 114-120mm reinforced concrete structural slabs with 6575 mm thick non-structural screeds. The reinforcement consists of $4.1-4.3 \mathrm{~mm}$ diameter round wire bars. Tensile testing on several steel samples confirmed the yield strength to be at least $500 \mathrm{~N} / \mathrm{mm}^{2}$. Compressive tests were carried out on concrete core samples which returned results in the range of $28.8-56.2 \mathrm{~N} / \mathrm{mm}^{2}$. Our analysis of these slabs confirms capacity to cater for the proposed new floor loads at these levels, including communal and gym areas. Results of the material testing are included in Appendix F.

The floor slab at both levels can provide the required fire rating without additional work.

### 2.3.2 Third (roof) Slab

The section of this slab constructed in the later 1920's covering the west wing of the building (approximately $30 \%$ of the full floor area) had a similar thickness, strength and reinforcement content to the original levels 1 and 2.

The section of the floor constructed in the 1930's has a slab thickness between $98-107 \mathrm{~mm}$. The reinforcing steel used in the slab is a wound wire type steel. The tensile test results for this slab show yield strengths as low as $384 \mathrm{~N} / \mathrm{mm} 2$, with a much lower quantity of tensile steel than provided in the other slabs. The cover to the reinforcement in this slab was found to be as little as 10 mm .

### 2.4 Foundations

A number of footing exposures were carried out, typically two each at internal atrium columns location, internal columns and at external façade piers (refer to Photos 28-31 in Appendix A). These exposures comprised of locally removing the ground floor slab around each element to establish the footing type, size, depth and founding material. As expected, all foundations were found to be conventional concrete spread footings, with tiered bases which were common at the time of construction. The concrete was found to be in good condition. Compressive tests on core samples were also carried out, giving results of 59.1 and $61.3 \mathrm{~N} / \mathrm{mm} 2$. The footings are founded on a soft to firm brown boulder clay with relatively low bearing capacity of $80 \mathrm{kN} / \mathrm{m} 2$.

An assessment of the building loads was carried out to compare the proposed five level residential development to that of the original three level factory building. Due to the reduction in live loading,
it is possible to found the proposed development on the existing foundations without additional strengthening, once any new concrete elements (floor slabs/screeds) are kept to a minimum, and the new roof constructed from lightweight material.

### 3.0 FINDINGS AND RECOMMENDATIONS

### 3.1 Findings

An extensive amount of testing, opening up and structural assessment has been carried out to determine the capacity of the existing structure of the Player Wills Factory Building, with some testing yet to be complete.

It was found that the foundations have the capacity for the proposed development once the additional building load does not exceed the original building loads.

It was found that the primary steel beams and concrete slabs for the First and Second Floor have the capacity for the proposed development.

Based on the proposed structure for the new levels, the existing internal 160 mm diameter columns at First floor level and the 180 mm diameter columns at Ground floor level have capacity for the proposed development. Further assessment is being carried out on the cathodic protection trials for the external façade columns to confirm they have capacity for the proposed development.

The third level extension to the original two storey building has been found to be inferior in quality and strength to that of the original building. The existing columns on the top level are small, and only fit for minor building loads. Likewise, the beams are undersized to take even typical floor loads as they were originally designed to support the roof.

The slab at this level is of very poor quality. The slab thickness, at less than 100 mm , does not meet the minimum thickness required for 90 minute fire rating. Both the reinforcement quantity and tensile strength are very low resulting in an insufficient flexural strength in the slab, even for residential floor loads.

### 3.2 ReCOMMENDATIONS

Considering the extremely poor quality of the existing roof slab, and low capacity of the supporting steel structure at level 2 , it is recommended that the third floor structure, including the columns from Level 2 up, be replaced with a new structural steel and composite metal slab (approximately 110 mm thick). This new structure would be designed so as to be suitable to transfer the loads from the new structure above to the existing structure below.

The façade, and the perimeter columns within the façade build up, would be protected and retained. Temporary works would be required during the construction works of the new third floor.

A cross section of the proposed structure for the additional levels for the development, including the replaced Level 3 is provided in Appendix C. This structure will require to be constructed from lightweight materials so as to allow the existing columns up to Level 2 and foundations be re-used.

Appendix A
Photographs


Photo 1: Original Building Condition


Photo 2: Original Building Condition


Photo 3: Original Building Condition


Photo 4: Original Building Condition


Photo 5: Original Building Condition


Photo 6: Original Building Condition


Photo 7: Original Building Condition


Photo 8: Original Building Condition


Photo 9: Original Building Condition


Photo 10: Original Building Condition


Photo 11: Typical Ground/First Column and beam


Photo 12: Typical column head connection


Photo 13: Level 2 column (1930's section) with level 3 beams


Photo 14: Level 2 column for 1920's section


Photo 15: Level 2 in 1930's section


Photo 16: Embedded Steel


Photo 17: Embedded Steel


Photo 18: Embedded Steel


Photo 19: Embedded Steel


Photo 20: Embedded Steel


Photo 21: Ground Floor Slab


Photo 22: Ground Floor Slab


Photo 23: Core sample, with non-structural screed with timber batons


Photo 24: Core Sample


Photo 25: Level 1 Reinforcement


Photo 26: Level 2 reinforcement


Photo 27: Level 3 reinforcement


Photo 28: Tiered spread footing


Photo 29: Tiered spread footing


Photo 30: Tiered spread footing


Photo 31: Tiered spread footing

Appendix B
Existing Structure Mark-up





Calculation Status: Preliminary $\square \quad$ Planning $\square \quad$ Tender $\square \quad$ Construction $\square$

| REF | CALCuLATIONS | OUTPUT |
| :---: | :---: | :---: |
|  | GROWD to fIRsT PLODR COLLMNS <br> $10^{\prime \prime} \times 6^{n}$ (REFER TO HISTO SECTIONS ATTACHED) WITH $2 \mathrm{NO} .250 \times 12 \mathrm{~mm}$ <br> $10^{11} \times 6^{n}$ <br> (REFER To attached hISTORICA SECTIONS WITM 2NO. $250 \times 12$ | rical plates |



## 



 ing ir
in in in ù í
 -000000000000000000000000000 in in o vio




00000000000000000000000000000













- Ao don




## Appendix C

Proposed Additional Level Structure

1. DEMOLISH EXISTING SLAB AND BEAMS
2. INSTALL NEW PRIMARY BEAMS ALONG EXISTING COLUMN LINE.
3. INSTALL SECONDARY TRANSFER BEAMS TO TRANSFER THE LOADS FROM THE COLUMNS ABOVE TO THE PRIMARY BEAMS
4. INSTALL NEW SECONDARY STEEL AND PERIMETER BEAMS.
5. INSTALL NEW COMFLOR 51+ WITH 110 mm SLAB (SIMILAR TO NEW FLOOR ABOVE).
6. INSTALL NEW COLUMNS LEVEL 02 - LEVEL 03

CDLUMNS FRDM LEVEL 04 AbIVE

- transfer secundary

BEAMS - $406 \times 178$ UB 74
NEW SECINDARY BEAMS -
$305 \times 127$ UB 48

- NEW PRIMARY BEAMS INSTALLED ALDNG EXISTING CDLUMN LINE $533 \times 210$ UB 109
- NEW PRIMARY BEAMS - $533 \times 165$ UB 66
$\leftrightharpoons$ CDMFLDR 51+ WITH 110mm SLAB
NEW PERIMETER BEAMS -
$305 \times 127$ UB 33
A^




ROOF
$\leftarrow 152$ UC 37

COMFLOR $51+$ WITH 110 mm SLAB + A252 MESH
$203 \times 1024823$
$203 \times 102$ UB 23

NEL CONNECTION TO EXISTING STEEL COLUMN IN EXTERNAL FACADE


Appendix D
United Metal Investigation Works

## Player Wills

## Address :

| Generated on | $-20 / 02 / 2020$ |
| :--- | :--- |
| Stages | - United Metals - Player Wills |
| Building trades | - Investigation Works |
| Stakeholders | - United Metals Recycling (Ireland) Ltd Casey Niall |
| Drawings | - 2019-10-16 (United Metals - Player Wills ) |
|  | - First floor plan (United Metals - Player Wills ) |
|  | - Second floor plan (United Metals - Player Wills ) |
|  | - Third floor plan (United Metals - Player Wills ) |
|  | gloor investigation 1 (United Metals - Player Wills ) |












E-1,








Drawing: First floor plan - Stage: United Metals - Player Wills




36 - 07/02/2020








44 © 07/02/2020





$47 \boldsymbol{\oplus} 07 / 02 / 2020$

$48 \oplus 07 / 02 / 2020$



## BUILDING SURVEY

CONFIRM THE BOTTOM FLANGE WIOTH AND THICKNESS OF ALL STEEL THE SURVELL LEVELS AND INCLUDE THIS INFORMATION ON THE SURVEY, THE SURVEYOR SHALL CONFIRM ALL COLUMN SIZES ON ALL LEVELS AND INCLUDE THIS INFORMATIONON THE SURVEY, UNNERSAL BEAM AND COLUMN SECTION FLANGE

## CONDITION SURVEY

A CONDTION SCHEDULE OF THE STRUCTURE SHALL BE CARRIED TO FACILTATE
IDENTFICATION ANO TENDERING OF RECTIFICATION WORKS TO STRUCTURE TO BE RETAINED. THE SURVEY IS TO FOCUS ON LOADBEARING ELEMENTS OF STRUCTURE - SLABS,
BEAMS COUUMNS AND MA SONRY OR CONCRETE WALS. THE SURVEY IS TO BE CARRIED OU ONA GRID BAASS THBOUGHOUT THE BULDING AND SHALL INCLUDE BOTH PHOTOGRAPHS
AND DESCRIPTIONS

| OPENING UP WORKS SCHEDULE |  |  |
| :---: | :---: | :---: |
| NUMBER | TITLE | DESCRIPTION |
| 1 | SUA EXPOSURE $3 \mathrm{No}$. | BREOK OUT SOONM-SOOMUAEEA OF YABAT MOSFAN BETNEEN <br>  <br>  |
| 2 | Subconcreticlommessme tiss |  COMPassem tists ons sur |













10 © 24/09/2019


11 © 24/09/2019
Steel Investigation





14 © 24/09/2019






## 17 - 25/09/2019






## 19 - 25/09/2019




20 - 25/09/2019



21 © 27/09/2019
Brick Investigation


## Appendix E

McFarland Consulting Façade Steelwork Survey

# Player Wills Factory - Column Condition Survey 19575-MCL-XX-RP-J-0001-P01 

| To: | Ciaran O'Rafferty | From: Jason Kearney |  |
| :--- | :--- | :--- | :--- |
| Re: | Player Wills Factory, Column Condition Survey | Date: | $22 / 06 / 2020$ |

### 1.0 INTRODUCTION

On the 10th March 2020, McFarland Consulting Limited (MCL) were instructed by Arran Timms, of Virtus, to commence investigative works concerning the remediation of cracked brickwork piers at the Player Wills Factory, Dublin. This report relates to the first phase of investigative works; a condition survey of affected columns and lintels by means of visual inspection. The survey was undertaken between the 27th and 28th May 2020 by 2no. MCL Corrosion Engineers.

### 2.0 SCOPE OF WORKS

The scope of works included undertaking a visual inspection of encased columns and lintels within the existing factory building and subsequently assigning a condition rating to each. The condition rating considers:

- Whether the columns/lintels are presently exhibiting cracking, spalling or delamination;
- Whether the columns/lintels are visibly saturated or stained; and
- The proximity of rainwater goods to the encased elements (as a likely source of water ingress to date).
Only those columns and lintels to be retained as part of the refurbishment works were surveyed. The findings of this condition survey will inform the selection of localised investigations, including nondestructive testing and cathodic protection trials, that are to be undertaken in subsequent phases of works.


### 3.0 CAVEATS AND EXCLUSIONS

Any information made available to us in the course of the investigation whether verbal or in the form of drawings, documents, reports etc. has been assumed to be bona fide and of reliable content.

Player Wills Factory, Column Condition Survey

### 4.0 DESCRIPTION OF THE STRUCTURE

This derelict factory building, constructed in 1923, is a masonry clad steel frame structure that is to be refurbished for residential use. The steel frame is exposed within the building interior, however, across the exterior elevations the steel columns have been encased within brick piers. The columns located along the perimeter of the central atrium are also encased; the ground floor columns are encased in concrete whilst the columns on the upper floors are encased in brick. It is evident from opening up works undertaken by others that no cavity space exists between the steel columns and the surrounding brick encasement at the majority of locations. There was evidence of a small cavity space having been incorporated within 1no. second floor encased column located adjacent to the internal atrium space.

Additionally, a combination of steel sections encased in concrete and reinforced concrete has been used in the construction of window lintels throughout the building. The encased steel lintels are present over ground, first and second floor windows. Reinforced concrete lintels are present over a selection of second floor windows.

### 5.0 FINDINGS AND OBSERVATIONS

The visual inspection of the encased columns and lintels was undertaken from ground level around the exterior of the building and from the respective floor levels within the building interior such that the exposed faces of each element could be inspected. The exterior faces of the atrium columns (those facing into the atrium void space) were visually inspected from the surrounding roof level.

The exterior and interior faces of each element were inspected and subsequently assigned a condition rating and corresponding colour indicator, in accordance with the convention outlined in Figure 1 below. Where the assigned condition rating for the interior and exterior faces of the same element differed, the more severe condition is considered to apply to the element overall.

An observation register for each element can be found in Appendix A. Plan drawings indicating the assigned condition rating for each element on a floor by floor basis can be found in Appendix B.

| Observed Condition | Colour <br> Rating |
| :---: | :---: |
| Visual inspection inhibited - i.e. obscured from view by surface finishes, increased pier thickness, mechanical damage (demolition activities) etc. Element not encased in brickwork/concrete. | No Colour |
| No obvious defects observed |  |
| Fine to moderate cracking of brickwork or concrete observed. Evidence of saturation observed increased likelihood of corrosion of embedded steel. |  |
| Heavy cracking of brickwork or concrete observed. Bulging or displacement of brickwork observed. Spalled or delaminated concrete observed. |  |

Figure 1: RAG Condition Rating

## Player Wills Factory, Column Condition Survey

A summary of observations is outlined below:

- Numerous instances of cracking were observed on the brickwork encasement at column locations. The severity of cracking ranged from hairline cracking to heavy cracking. The orientation of the observed cracking tended to be vertical, following the alignment of the embedded steel column (Plates 1 to 3 ). In the most severe of cases, 2 no. parallel vertical cracks, coinciding with alignment of the column flanges, were present over the full height (storey height) of the affected columns (Plates 4 to 6).


Plate 1


Plate 3


Plate 5


Plate 2


Plate 4


Plate 6

- Bulging and displacement of the brickwork encasement was identified at 1no. location (Plate 7).


Plate 7

- Evidence of saturation was identified at a number of encased column and lintel locations (Plates 8 and 9). Saturation was particularly prevalent across the south elevation internally (Plates 10 and 11). Whilst the areas where saturation was evident often also exhibited cracking, there were instances where saturation was not accompanied by observable defects. Nonetheless, there is an increased likelihood of corrosion occurring at these locations given the availability of moisture to support the corrosion process.


Plate 8


Plate 9


Plate 10


Plate 11

- Numerous instances of cracking were observed on concrete encased lintels. The cracking was predominantly vertical in orientation, likely coinciding with the position of supplementary stirrups (Plates 12 and 13) - this type of bar reinforcement was observed surrounding the steel lintel sections at locations where opening up works had been undertaken (by others). At a limited number of locations, horizontal cracking was also observed, likely coinciding with the bottom flange of the encased lintel (Plates 14 to 16). Localised cracking of the concrete encasement was also observed at the point of connection between encased lintels and secondary beams (Plate 17).


Plate 14


Plate 13


Plate 15


Plate 16


Plate 17

- Numerous instances of cracking were also observed on reinforced concrete lintels, likely coinciding with the position of shear links (Plate 18). At a selection of reinforced concrete lintels, spalled concrete and exposed corroded reinforcement was identified (Plate 19). Reinforced concrete lintels are believed only to be present over a selection of second floor window locations.


Plate 18


Plate 19

- Within the interior of the building, surface finishes (paint coatings, tiling, plasterwork, panelling etc.) may have inhibited the identification of defects (plate 20). Additionally, along the southern building elevation (gridline N ) the existence of inbuilt chimney flues, thickened brick piers and exterior stone cladding may have concealed defects (Plates 21 to 23).


Plate 20


Plate 21

## Player Wills Factory, Column Condition Survey



Plate 22


Plate 23

- Localised areas of brick/concrete encasement have been removed (by others) to expose the embedded steel sections or steel reinforcement. The condition of the steel present at these locations varied, from exhibiting little or no corrosion (Plates 24 and 25) to exhibiting moderate surface corrosion (Plates 26 and 27). From the limited number of elements exposed, it appears that the embedded columns located along the eastern elevation are worst affected.


Plate 24


Plate 26


Plate 25


Plate 27

### 6.0 CONCLUSIONS

Cracking of the encasement surrounding columns and lintels was observed at numerous locations throughout the building, both on external and internal faces. The survey also indicates a significant concentration of defects to the eastern aspect of the building on the first floor. In addition to the observed cracking, spalled and delaminated concrete was also identified on a selection of reinforced concrete lintels located on the second floor.

The nature of the observed cracking, in conjunction with the condition of the embedded steel exposed in localised areas, would suggest that steel corrosion is a likely cause of the observed defects. The lack of cavity space provided between the embedded steel columns and the surrounding brick encasement is likely contributing to the cracking observed at these locations. In the absence of a cavity space, the buildup of expansive corrosion products on the surface of the steel columns imposes increased stress directly onto the surrounding brickwork, subsequently causing it to crack. However, cracking arising from structural deficiencies or structural movement cannot be ruled out; these considerations should be checked by a suitably qualified structural engineer.

Nonetheless, it is recommended that further investigations are undertaken to determine whether the embedded steel is likely to be actively corroding, and the extent over which this may be occurring. It is also recommended that investigations are undertaken to determine the presence of deleterious contaminants or the action of deterioration processes which may be contributing to the corrosion of the embedded steel.

## Appendix A - Observation Register

| Element Ref: | Type | Level | Face | Notes | Face-by- Face <br> RAG Rating | Combined RAG Rating |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A3 | Column | 0 | Interior | Not Encased |  |  |
|  |  |  | Exterior | Heavy Vertical Cracking - (2no Parallel) |  |  |
| A2 | Column | 0 | Interior | Heavy Vertical Cracking - (1no ) |  |  |
|  |  |  | Exterior | Heavy Vertical Cracking - (2no Parallel) |  |  |
| A1 | Column | 0 | Interior | Moderate Vertical Cracking - ( ) |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| B1 | Column | 0 | Interior | Moderate Vertical Cracking - ( ) |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| C1 | Column | 0 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| D1 | Column | 0 | Interior | Isolated Fine Vertical Cracking - (1no ) |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| E1 | Column | 0 | Interior | Encasement Partially Removed |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| F1 | Column | 0 | Interior | Isolated Moderate Vertical Cracking - ( ) |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| G1 | Column | 0 | Interior | Encasement Partially Removed |  |  |
|  |  |  | Exterior | Heavy Vertical Cracking - ( ) |  |  |
| H1 | Column | 0 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| $J 1$ | Column | 0 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| K1 | Column | 0 | Interior | Obscured from View |  |  |
|  |  |  | Exterior | Isolated Heavy Vertical Cracking - (1no ) |  |  |
| L1 | Column | 0 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| M1 | Column | 0 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| N1 | Column | 0 | Interior | Obscured from View |  |  |
|  |  |  | Exterior | Visually Sound |  |  |


| Element Ref: | Type | Level | Face | Notes | Face-by- Face RAG Rating | $\begin{aligned} & \text { Combined RAG } \\ & \text { Rating } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| N2 | Column | 0 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Heavy Vertical Cracking - () |  |  |
| N3 | Column | 0 | Interior | Cracked Render and Saturation |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| N4 | Column | 0 | Interior | Heavy Vertical Cracking - () |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| N5 | Column | 0 | Interior | Heavy Vertical Cracking - () |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| N6 | Column | 0 | Interior | Isolated Moderate Vertical Cracking - ( ) |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| N7 | Column | 0 | Interior | Cracked Render |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| N8 | Column | 0 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| N9 | Column | 0 | Interior | Cracked Render |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| N10 | Column | 0 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Heavy Vertical Cracking - () |  |  |
| M10 | Column | 0 | Interior | Isolated Moderate Vertical Cracking - () |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| L10 | Column | 0 | Interior | Heavy Vertical Cracking - ( ) |  |  |
|  |  |  | Exterior | Isolated Heavy Vertical Cracking - (2no Parallel) |  |  |
| K10 | Column | 0 | Interior | Encasement Partially Removed |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| J10 | Column | 0 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| H10 | Column | 0 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| G10 | Column | 0 | Interior | Heavy Vertical Cracking - (2no Parallel) |  |  |
|  |  |  | Exterior | Visually Sound |  |  |


| Element Ref: | Type | Level | Face | Notes | Face-by- Face RAG Rating | $\begin{aligned} & \text { Combined RAG } \\ & \text { Rating } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| F10 | Column | 0 | Interior | Isolated Moderate Vertical Cracking - () |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| E10 | Column | 0 | Interior | Moderate Vertical Cracking - () |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| D10 | Column | 0 | Interior | Moderate Vertical Cracking - (2no Parallel) |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| D4 | Column | 0 | Interior | Mechanical Damage |  |  |
|  |  |  | Exterior | n/a |  |  |
| E4 | Column | 0 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | n/a |  |  |
| F4 | Column | 0 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | n/a |  |  |
| G4 | Column | 0 | Interior | Moderate Vertical Cracking - () |  |  |
|  |  |  | Exterior | n/a |  |  |
| H4 | Column | 0 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | n/a |  |  |
| J4 | Column | 0 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | n/a |  |  |
| K4 | Column | 0 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | n/a |  |  |
| K5 | Column | 0 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | n/a |  |  |
| K6 | Column | 0 | Interior | Moderate Horizontal Cracking - () |  |  |
|  |  |  | Exterior | n/a |  |  |
| K7 | Column | 0 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | n/a |  |  |
| J7 | Column | 0 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | n/a |  |  |
| H7 | Column | 0 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | n/a |  |  |


| Element Ref: | Type | Level | Face | Notes | Face-by- Face RAG Rating | Combined RAG Rating |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| G7 | Column | 0 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | n/a |  |  |
| F7 | Column | 0 | Interior | Mechanical Damage |  |  |
|  |  |  | Exterior | n/a |  |  |
| E7 | Column | 0 | Interior | Fine Horizontal Cracking - () |  |  |
|  |  |  | Exterior | n/a |  |  |
| D7 | Column | 0 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | n/a |  |  |


| Element Ref: | Type | Level | Face | Notes | Face-by- Face RAG Rating | Combined RAG <br> Rating |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A3 | Column | 1 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| A2 | Column | 1 | Interior | Isolated Moderate Vertical Cracking - ( ) |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| A1 | Column | 1 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| B1 | Column | 1 | Interior | Isolated Heavy Vertical Cracking - () |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| C1 | Column | 1 | Interior | Heavy Vertical Cracking - (2no Parallel) |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| D1 | Column | 1 | Interior | Isolated Moderate Vertical Cracking - ( ) |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| E1 | Column | 1 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| F1 | Column | 1 | Interior | Heavy Vertical Cracking - ( ) |  |  |
|  |  |  | Exterior | Isolated Fine Vertical Cracking - (1no ) |  |  |
| G1 | Column | 1 | Interior | Isolated Moderate Vertical Cracking - (2no Parallel) |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| H1 | Column | 1 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| J1 | Column | 1 | Interior | Heavy Vertical Cracking - () |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| K1 | Column | 1 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| L1 | Column | 1 | Interior | Heavy Vertical Cracking - (2no. Parallel) |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| M1 | Column | 1 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| N1 | Column | 1 | Interior | Visually Sound c/w Chimney Thickening |  |  |
|  |  |  | Exterior | Heavy Vertical Cracking - ( ) |  |  |


| Element Ref: | Type | Level | Face | Notes | Face-by- Face RAG Rating | Combined RAG Rating |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| N2 | Column | 1 | Interior | Visually Sound c/w Chimney Thickening |  |  |
|  |  |  | Exterior | Isolated Heavy Vertical Cracking - () |  |  |
| N3 | Column | 1 | Interior | Visually Sound c/w Thickened Pier |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| N4 | Column | 1 | Interior | Visually Sound c/w Chimney Thickening |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| N5 | Column | 1 | Interior | Visually Sound c/w Thickened Pier |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| N6 | Column | 1 | Interior | Visually Sound c/w Chimney Thickening |  |  |
|  |  |  | Exterior | Isolated Moderate Vertical Cracking - ( ) |  |  |
| N7 | Column | 1 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| N8 | Column | 1 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| N9 | Column | 1 | Interior | Visually Sound c/w Thickened Pier |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| N10 | Column | 1 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Heavy Vertical Cracking - () |  |  |
| M10 | Column | 1 | Interior | Heavy Vertical Cracking - () |  |  |
|  |  |  | Exterior | Isolated Heavy Vertical Cracking - () |  |  |
| L10 | Column | 1 | Interior | Heavy Vertical Cracking - (2no Parallel) |  |  |
|  |  |  | Exterior | Heavy Vertical Cracking - () |  |  |
| K10 | Column | 1 | Interior | Heavy Vertical Cracking - (2no Parallel) |  |  |
|  |  |  | Exterior | Isolated Heavy Vertical Cracking - (2no ) |  |  |
| $J 10$ | Column | 1 | Interior | Heavy Vertical Cracking - (2no Parallel) |  |  |
|  |  |  | Exterior | Isolated Moderate Vertical Cracking - (1no ) |  |  |
| H10 | Column | 1 | Interior | Visually Sound c/w Thickened Pier |  |  |
|  |  |  | Exterior | Heavy Vertical Cracking - () |  |  |
| G10 | Column | 1 | Interior | Heavy Vertical Cracking - (2no Parallel) |  |  |
|  |  |  | Exterior | Heavy Vertical Cracking - () |  |  |


| Element Ref: | Type | Level | Face | Notes | Face-by- Face RAG Rating | Combined RAG Rating |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| F10 | Column | 1 | Interior | Heavy Vertical Cracking - (2no Parallel) |  |  |
|  |  |  | Exterior | Heavy Vertical Cracking - () |  |  |
| E10 | Column | 1 | Interior | Heavy Vertical Cracking - () |  |  |
|  |  |  | Exterior | Heavy Vertical Cracking - ( ) |  |  |
| D10 | Column | 1 | Interior | Heavy Vertical Cracking - (2no Parallel) |  |  |
|  |  |  | Exterior | Heavy Vertical Cracking - () |  |  |
| D4 | Column | 1 | Interior | Moderate Vertical Cracking - () |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| E4 | Column | 1 | Interior | Isolated Moderate Vertical Cracking - ( ) |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| F4 | Column | 1 | Interior | Isolated Moderate Vertical Cracking - ( ) |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| G4 | Column | 1 | Interior | Heavy Vertical Cracking - (2no Parallel) |  |  |
|  |  |  | Exterior | Visually Sound \& Saturated |  |  |
| H4 | Column | 1 | Interior | Isolated Moderate Vertical Cracking - ( ) |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| J4 | Column | 1 | Interior | Isolated Heavy Vertical Cracking - (2no Parallel) |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| K4 | Column | 1 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| K5 | Column | 1 | Interior | Moderate Vertical Cracking - () |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| к6 | Column | 1 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| K7 | Column | 1 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| 17 | Column | 1 | Interior | Heavy Vertical Cracking - () |  |  |
|  |  |  | Exterior | Heavy Vertical Cracking - ( ) |  |  |
| H7 | Column | 1 | Interior | Isolated Heavy Vertical Cracking - (1no ) |  |  |
|  |  |  | Exterior | Heavy Vertical Cracking - () |  |  |


| Element Ref: | Type | Level | Face | Notes | Face-by- Face RAG Rating | Combined RAG Rating |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| G7 | Column | 1 | Interior | Heavy Vertical Cracking - (2no Parallel) |  |  |
|  |  |  | Exterior | Saturation Evident |  |  |
| F7 | Column | 1 | Interior | Heavy Vertical Cracking - (2no Parallel) |  |  |
|  |  |  | Exterior | Heavy Vertical Cracking - ( ) |  |  |
| E7 | Column | 1 | Interior | Heavy Vertical Cracking - (2no Parallel) |  |  |
|  |  |  | Exterior | Isolated Heavy Vertical Cracking - ( ) |  |  |
| D7 | Column | 1 | Interior | Heavy Vertical Cracking - (2no Parallel) |  |  |
|  |  |  | Exterior | Visually Sound |  |  |


| Element Ref: | Type | Level | Face | Notes | $\begin{aligned} & \text { Face-by-Face } \\ & \text { RAG Rating } \end{aligned}$ | Combined RAG Rating |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A3 | Column | 2 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| A2 | Column | 2 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| A1 | Column | 2 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| B1 | Column | 2 | Interior | Isolated Moderate Vertical Cracking - ( ) |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| C1 | Column | 2 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| D1 | Column | 2 | Interior | Isolated Moderate Vertical Cracking - () |  |  |
|  |  |  | Exterior | Isolated Heavy Vertical Cracking - (2no ) |  |  |
| E1 | Column | 2 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| F1 | Column | 2 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| G1 | Column | 2 | Interior | Isolated Fine Vertical Cracking - ( ) |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| H1 | Column | 2 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| $J 1$ | Column | 2 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| K1 | Column | 2 | Interior | Isolated Fine Vertical Cracking - ( ) |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| L1 | Column | 2 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| M1 | Column | 2 | Interior | Visually Sound c/w Thickened Pier |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| N1 | Column | 2 | Interior | Visually Sound c/w Chimney Thickening |  |  |
|  |  |  | Exterior | Visually Sound |  |  |


| Element Ref: | Type | Level | Face | Notes | Face-by- Face RAG Rating | $\begin{aligned} & \text { Combined RAG } \\ & \text { Rating } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| N2 | Column | 2 | Interior | Isolated Moderate Vertical Cracking - () |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| N3 | Column | 2 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| N4 | Column | 2 | Interior | Visually Sound c/w Thickened Pier |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| N5 | Column | 2 | Interior | Visually Sound + Saturation |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| N6 | Column | 2 | Interior | Visually Sound c/w Thickened Pier |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| N7 | Column | 2 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| N8 | Column | 2 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| N9 | Column | 2 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| N10 | Column | 2 | Interior | Obscured from view |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| M10 | Column | 2 | Interior | Visually Sound + Saturation |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| L10 | Column | 2 | Interior | Visually Sound + Saturation |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| K10 | Column | 2 | Interior | Isolated Heavy Vertical Cracking - () |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| J10 | Column | 2 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| H10 | Column | 2 | Interior | Visually Sound c/w Thickened Pier |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| G10 | Column | 2 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |


| Element Ref: | Type | Level | Face | Notes | Face-by- Face RAG Rating | $\begin{aligned} & \text { Combined RAG } \\ & \text { Rating } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| F10 | Column | 2 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| E10 | Column | 2 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| D10 | Column | 2 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| D4 | Column | 2 | Interior | Heavy Vertical Cracking - () |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| E4 | Column | 2 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| F4 | Column | 2 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| G4 | Column | 2 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound + Saturated |  |  |
| H4 | Column | 2 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| J4 | Column | 2 | Interior | Isolated Fine Vertical Cracking - ( ) |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| K4 | Column | 2 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| K5 | Column | 2 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| K6 | Column | 2 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| K7 | Column | 2 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| 17 | Column | 2 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| H7 | Column | 2 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Isolated Heavy Vertical Cracking - ( ) |  |  |


| Element Ref: | Type | Level | Face | Notes | Face-by- Face RAG Rating | $\begin{aligned} & \text { Combined RAG } \\ & \text { Rating } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| G7 | Column | 2 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Heavily Saturated |  |  |
| F7 | Column | 2 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| E7 | Column | 2 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| D7 | Column | 2 | Interior | Heavy Vertical Cracking - (Bulging ) |  |  |
|  |  |  | Exterior | Visually Sound |  |  |


| Element Ref: | Type | Level | Face | Notes | Face-by- Face RAG Rating | Combined RAG Rating |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A3/4 | Lintel | 0 | Interior | Fine Vertical Cracking - ( ) |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| A2/3 | Lintel | 0 | Interior | Fine Vertical Cracking - () |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| A1/2 | Lintel | 0 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Isolated Heavy Vertical Cracking - (1no ) |  |  |
| A/B1 | Lintel | 0 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Isolated Moderate Vertical Cracking - (3no ) |  |  |
| B/C1 | Lintel | 0 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Isolated Moderate Vertical Cracking - (2no ) |  |  |
| C/D1 | Lintel | 0 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Isolated Moderate Vertical Cracking - (1no ) |  |  |
| D/E1 | Lintel | 0 | Interior | Fine Vertical Cracking - ( ) |  |  |
|  |  |  | Exterior | Isolated Heavy Vertical Cracking - (4no ) |  |  |
| E/F1 | Lintel | 0 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Isolated Heavy Vertical Cracking - (1no ) |  |  |
| F/G1 | Lintel | 0 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Isolated Heavy Vertical Cracking - (3no ) |  |  |
| G/H1 | Lintel | 0 | Interior | Fine Vertical Cracking - (2no ) |  |  |
|  |  |  | Exterior | Isolated Heavy Vertical Cracking - (2no ) |  |  |
| H/J1 | Lintel | 0 | Interior | Isolated Mechanical Damage |  |  |
|  |  |  | Exterior | Isolated Heavy Vertical Cracking - (2no ) |  |  |
| J/K1 | Lintel | 0 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Isolated Heavy Vertical Cracking - (4no ) |  |  |
| K/L1 | Lintel | 0 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Isolated Heavy Vertical Cracking - (2no ) |  |  |
| L/M1 | Lintel | 0 | Interior | Flaking Paint Obscuring View |  |  |
|  |  |  | Exterior | Isolated Heavy Vertical Cracking - (3no ) |  |  |
| M/N1 | Lintel | 0 | Interior | Heavy Horizontal \& Moderate Vertical Cracking - ( ) |  |  |
|  |  |  | Exterior | Isolated Heavy Vertical Cracking - (4no ) |  |  |


| Element Ref: | Type | Level | Face | Notes | Face-by- Face RAG Rating | Combined RAG Rating |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| N1/2 | Lintel | 0 | Interior | Fine Vertical Cracking - ( ) |  |  |
|  |  |  | Exterior | Isolated Heavy Vertical Cracking - (4no ) |  |  |
| N2/3 | Lintel | 0 | Interior | Moderate Vertical Cracking - () |  |  |
|  |  |  | Exterior | Isolated Moderate Vertical Cracking - (5no ) |  |  |
| N3/4 | Lintel | 0 | Interior | Cracked Render \& Saturation |  |  |
|  |  |  | Exterior | Isolated Moderate Vertical Cracking - (4no ) |  |  |
| N4/5 | Lintel | 0 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Isolated Heavy Vertical Cracking - (4no ) |  |  |
| N5/6 | Lintel | 0 | Interior | Visually Sound + Saturation |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| N6/7 | Lintel | 0 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Isolated Heavy Vertical Cracking - (4no ) |  |  |
| N7/8 | Lintel | 0 | Interior | Fine Vertical Cracking - ( ) |  |  |
|  |  |  | Exterior | Isolated Heavy Vertical Cracking - (4no ) |  |  |
| N8/9 | Lintel | 0 | Interior | Fine Vertical Cracking - ( ) |  |  |
|  |  |  | Exterior | Isolated Heavy Vertical Cracking - (4no ) |  |  |
| N9/10 | Lintel | 0 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Isolated Heavy Vertical Cracking - (2no ) |  |  |
| M/N10 | Lintel | 0 | Interior | Moderate Vertical Cracking - () |  |  |
|  |  |  | Exterior | Isolated Fine Vertical Cracking - (3no ) |  |  |
| L/M10 | Lintel | 0 | Interior | Moderate Vertical Cracking - (4no ) |  |  |
|  |  |  | Exterior | Isolated Heavy Vertical Cracking - (3no ) |  |  |
| K/L10 | Lintel | 0 | Interior | Heavy Vertical Cracking - (3no ) |  |  |
|  |  |  | Exterior | Isolated Heavy Vertical Cracking - (2no ) |  |  |
| J/K10 | Lintel | 0 | Interior | Moderate Vertical \& Horizontal Cracking - ( ) |  |  |
|  |  |  | Exterior | Isolated Heavy Vertical Cracking - (2no ) |  |  |
| H/J10 | Lintel | 0 | Interior | Fine Vertical Cracking - ( ) |  |  |
|  |  |  | Exterior | Isolated Heavy Vertical Cracking - (1no ) |  |  |
| G/H10 | Lintel | 0 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Isolated Moderate Vertical Cracking - (2no ) |  |  |


| Element Ref: | Type | Level | Face | Notes | Face-by- Face RAG Rating | Combined RAG Rating |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| F/G10 | Lintel | 0 | Interior | Fine Vertical Cracking - (2no ) |  |  |
|  |  |  | Exterior | Isolated Fine Vertical Cracking - (1no ) |  |  |
| E/F10 | Lintel | 0 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Isolated Moderate Vertical Cracking - (1no ) |  |  |
| D/E10 | Lintel | 0 | Interior | Fine Vertical Cracking - (1no ) |  |  |
|  |  |  | Exterior | Isolated Moderate Vertical Cracking - (2no ) |  |  |
| D/E4 | Lintel | 0 | Interior | Mechanical Damage |  |  |
|  |  |  | Exterior | Isolated Moderate Vertical Cracking - (1no ) |  |  |
| E/F4 | Lintel | 0 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Isolated Fine Vertical Cracking - (2no ) |  |  |
| F/G4 | Lintel | 0 | Interior | Localised Fine Vertical Cracking - ( ) |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| G/H4 | Lintel | 0 | Interior | Fine Vertical Cracking - ( ) |  |  |
|  |  |  | Exterior | Isolated Fine Vertical Cracking - (1no ) |  |  |
| H/J4 | Lintel | 0 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Isolated Moderate Vertical Cracking - (3no ) |  |  |
| J/K4 | Lintel | 0 | Interior | Fine Vertical Cracking - ( ) |  |  |
|  |  |  | Exterior | Isolated Moderate Vertical Cracking - (1no ) |  |  |
| K4/5 | Lintel | 0 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| K5/6 | Lintel | 0 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| K6/7 | Lintel | 0 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Isolated Moderate Vertical Cracking - (3no ) |  |  |
| J/K7 | Lintel | 0 | Interior | Moderate Vertical Cracking - ( ) |  |  |
|  |  |  | Exterior | Isolated Fine Vertical Cracking - (1no ) |  |  |
| H/J7 | Lintel | 0 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Isolated Fine Vertical Cracking - (1no ) |  |  |
| G/H7 | Lintel | 0 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Isolated Fine Vertical Cracking - (1no ) |  |  |


| Element Ref: | Type | Level | Face | Notes | Face-by- Face <br> RAG Rating | Combined RAG <br> Rating |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| F/G7 | Lintel | 0 | Interior | Mechanical Damage |  |  |
|  |  |  | Exterior | Isolated Moderate Vertical Cracking - (2no ) |  |  |
| E/F7 | Lintel | 0 | Interior | Fine Vertical Cracking - (3no ) |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| D/E7 | Lintel | 0 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |


| Element Ref: | Type | Level | Face | Notes | Face-by- Face RAG Rating | Combined RAG <br> Rating |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A3/4 | Lintel | 1 | Interior | Isolated Heavy Vertical Cracking - () |  |  |
|  |  |  | Exterior | Isolated Moderate Vertical Cracking - (2no ) |  |  |
| A2/3 | Lintel | 1 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Isolated Heavy Vertical Cracking - (5no ) |  |  |
| A1/2 | Lintel | 1 | Interior | Isolated Heavy Vertical Cracking \& Localised Spall - ( ) |  |  |
|  |  |  | Exterior | Isolated Heavy Vertical Cracking - (3no ) |  |  |
| A/B1 | Lintel | 1 | Interior | Heavy Vertical Cracking - (2no ) |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| B/C1 | Lintel | 1 | Interior | Moderate Vertical Cracking - (2no ) |  |  |
|  |  |  | Exterior | Isolated Moderate Vertical Cracking - (1no ) |  |  |
| C/D1 | Lintel | 1 | Interior | Isolated Heavy Vertical Cracking - () |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| D/E1 | Lintel | 1 | Interior | Isolated Heavy Vertical Cracking - () |  |  |
|  |  |  | Exterior | Isolated Heavy Vertical \& Horizontal Cracking - (3no ) |  |  |
| E/F1 | Lintel | 1 | Interior | Isolated Moderate Vertical Cracking - ( ) |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| F/G1 | Lintel | 1 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| G/H1 | Lintel | 1 | Interior | Isolated Moderate Vertical Cracking - ( ) |  |  |
|  |  |  | Exterior | Isolated Fine Vertical Cracking - (3no ) |  |  |
| H/J1 | Lintel | 1 | Interior | Isolated Heavy Vertical Cracking - (3no ) |  |  |
|  |  |  | Exterior | Isolated Moderate Vertical Cracking - (1no ) |  |  |
| J/K1 | Lintel | 1 | Interior | Isolated Moderate Vertical Cracking - () |  |  |
|  |  |  | Exterior | Isolated Moderate Vertical Cracking - (2no ) |  |  |
| K/L1 | Lintel | 1 | Interior | Isolated Heavy Vertical Cracking - () |  |  |
|  |  |  | Exterior | Isolated Moderate Vertical Cracking - (2no ) |  |  |
| L/M1 | Lintel | 1 | Interior | Moderate Vertical Cracking - (1no ) |  |  |
|  |  |  | Exterior | Isolated Moderate Vertical Cracking - (1no ) |  |  |
| M/N1 | Lintel | 1 | Interior | Obscured from view |  |  |
|  |  |  | Exterior | Isolated Heavy \& Moderate Vertical Cracking - (4no ) |  |  |


| Element Ref: | Type | Level | Face | Notes | Face-by- Face RAG Rating | $\begin{array}{l}\text { Combined RAG } \\ \text { Rating }\end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| N1/2 | Lintel | 1 | Interior | Obscured from view |  |  |
|  |  |  | Exterior | Crazing of Render |  |  |
| N2/3 | Lintel | 1 | Interior | Isolated Heavy Vertical \& Horizontal Cracking - ( ) |  |  |
|  |  |  | Exterior | Isolated Heavy Vertical Cracking - (4no ) |  |  |
| N3/4 | Lintel | 1 | Interior | Moderate Vertical Cracking - ( ) |  |  |
|  |  |  | Exterior | Isolated Heavy Vertical Cracking - (3no ) |  |  |
| N4/5 | Lintel | 1 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Isolated Heavy Vertical Cracking - (3no ) |  |  |
| N5/6 | Lintel | 1 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| N6/7 | Lintel | 1 | Interior | Isolated Moderate Vertical Cracking - ( ) |  |  |
|  |  |  | Exterior | Isolated Heavy Vertical Cracking - (4no ) |  |  |
| N7/8 | Lintel | 1 | Interior | Isolated Moderate Vertical Cracking - (1no ) |  |  |
|  |  |  | Exterior | Isolated Heavy Vertical Cracking - (1no ) |  |  |
| N8/9 | Lintel | 1 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Isolated Heavy Vertical Cracking - (3no ) |  |  |
| N9/10 | Lintel | 1 | Interior | Isolated Moderate Vertical Cracking - (2no ) |  |  |
|  |  |  | Exterior | Isolated Heavy Vertical Cracking - (3no ) |  |  |
| M/N10 | Lintel | 1 | Interior | Isolated Moderate Vertical Cracking - (3no ) |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| L/M10 | Lintel | 1 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Isolated Heavy Vertical Cracking - (3no ) |  |  |
| K/L10 | Lintel | 1 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| J/K10 | Lintel | 1 | Interior | Isolated Moderate Vertical Cracking - (1no ) |  |  |
|  |  |  | Exterior | Isolated Fine Vertical Cracking - (1no ) |  |  |
| H/J10 | Lintel | 1 | Interior | Isolated Heavy Vertical Cracking - (1no ) |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| G/H10 | Lintel | 1 | Interior | Isolated Heavy Vertical Cracking - (4no ) |  |  |
|  |  |  | Exterior | Isolated Moderate Vertical Cracking - (1no ) |  |  |


| Element Ref: | Type | Level | Face | Notes | Face-by- Face RAG Rating | $\begin{aligned} & \text { Combined RAG } \\ & \text { Rating } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| F/G10 | Lintel | 1 | Interior | Isolated Heavy Vertical Cracking - (3no ) |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| E/F10 | Lintel | 1 | Interior | Isolated Heavy Vertical Cracking - (3no ) |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| D/E10 | Lintel | 1 | Interior | Isolated Heavy Vertical Cracking - (2no ) |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| D/E4 | Lintel | 1 | Interior | Isolated Moderate Vertical Cracking - (2no ) |  |  |
|  |  |  | Exterior | Isolated Moderate Vertical Cracking - (1no ) |  |  |
| E/F4 | Lintel | 1 | Interior | Isolated Heavy Vertical Cracking - (3no ) |  |  |
|  |  |  | Exterior | Isolated Moderate Vertical Cracking - (3no ) |  |  |
| F/G4 | Lintel | 1 | Interior | Isolated Moderate Vertical Cracking - (3no ) |  |  |
|  |  |  | Exterior | Isolated Moderate Vertical Cracking - (4no ) |  |  |
| G/H4 | Lintel | 1 | Interior | Isolated Moderate Vertical Cracking - (2no ) |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| H/J4 | Lintel | 1 | Interior | Isolated Moderate Vertical Cracking - (4no ) |  |  |
|  |  |  | Exterior | Isolated Fine Vertical Cracking - (1no ) |  |  |
| J/K4 | Lintel | 1 | Interior | Isolated Moderate Vertical Cracking - (2no ) |  |  |
|  |  |  | Exterior | Isolated Moderate Vertical Cracking - (1no ) |  |  |
| K4/5 | Lintel | 1 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| K5/6 | Lintel | 1 | Interior | Isolated Moderate Vertical Cracking - ( ) |  |  |
|  |  |  | Exterior | Isolated Moderate Vertical Cracking - (2no ) |  |  |
| K6/7 | Lintel | 1 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| J/K7 | Lintel | 1 | Interior | Isolated Moderate Vertical Cracking - (2no ) |  |  |
|  |  |  | Exterior | Isolated Fine Vertical Cracking - (2no ) |  |  |
| H/J7 | Lintel | 1 | Interior | Isolated Heavy Vertical Cracking - (3no ) |  |  |
|  |  |  | Exterior | Isolated Heavy Vertical Cracking - (3no ) |  |  |
| G/H7 | Lintel | 1 | Interior | Obscured from view |  |  |
|  |  |  | Exterior | Isolated Heavy Vertical Cracking - (3no ) |  |  |


| Element Ref: | Type | Level | Face | Notes | Face-by- Face RAG Rating | Combined RAG Rating |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| F/G7 | Lintel | 1 | Interior | Obscured from view |  |  |
|  |  |  | Exterior | Isolated Heavy Vertical Cracking - (2no ) |  |  |
| E/F7 | Lintel | 1 | Interior | Isolated Heavy Vertical Cracking - (3no ) |  |  |
|  |  |  | Exterior | Isolated Moderate Vertical Cracking - (3no ) |  |  |
| D/E7 | Lintel | 1 | Interior | Isolated Heavy Vertical Cracking - (1no ) |  |  |
|  |  |  | Exterior | Isolated Moderate Vertical Cracking - (2no ) |  |  |


| Element Ref: | Type | Level | Face | Notes | Face-by- Face <br> RAG Rating | Combined RAG Rating |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A3/4 | Lintel | 2 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| A2/3 | Lintel | 2 | Interior | Isolated Moderate Vertical Cracking - (2no ) |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| A1/2 | Lintel | 2 | Interior | Isolated Heavy Horizontal Cracking - (1no ) |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| A/B1 | Lintel | 2 | Interior | Isolated Moderate Vertical Cracking - (2no ) |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| B/C1 | Lintel | 2 | Interior | Isolated Moderate Vertical Cracking - (2no ) |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| C/D1 | Lintel | 2 | Interior | Isolated Fine Vertical Cracking - (3no ) |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| D/E1 | Lintel | 2 | Interior | Isolated Heavy Vertical Cracking - () |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| E/F1 | Lintel | 2 | Interior | Isolated Moderate Vertical Cracking - ( ) |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| F/G1 | Lintel | 2 | Interior | Isolated Moderate Vertical Cracking - (2no ) |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| G/H1 | Lintel | 2 | Interior | Isolated Moderate Vertical Cracking - (3no ) |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| H/J1 | Lintel | 2 | Interior | Isolated Heavy Vertical Cracking - (2no ) |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| J/K1 | Lintel | 2 | Interior | Isolated Heavy Vertical Cracking - (2no ) |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| K/L1 | Lintel | 2 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| L/M1 | Lintel | 2 | Interior | Isolated Moderate Horizontal Cracking - (1no ) |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| M/N1 | Lintel | 2 | Interior | Isolated Heavy Vertical Cracking - () |  |  |
|  |  |  | Exterior | Visually Sound |  |  |


| Element Ref: | Type | Level | Face | Notes | Face-by- Face RAG Rating | Combined RAG Rating |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| N1/2 | Lintel | 2 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| N2/3 | Lintel | 2 | Interior | Obscured from view |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| N3/4 | Lintel | 2 | Interior | Isolated Heavy Vertical Cracking - (1no ) |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| N4/5 | Lintel | 2 | Interior | Isolated Heavy Vertical Cracking - (2no ) |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| N5/6 | Lintel | 2 | Interior | Isolated Moderate Vertical Cracking - (2no ) |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| N6/7 | Lintel | 2 | Interior | Isolated Heavy Vertical \& Horizontal Cracking - (3no ) |  |  |
|  |  |  | Exterior | Isolated Moderate Vertical Cracking - (1no ) |  |  |
| N7/8 | Lintel | 2 | Interior | Isolated Moderate Vertical Cracking - (1no ) |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| N8/9 | Lintel | 2 | Interior | Isolated Moderate Vertical Cracking - (1no ) |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| N9/10 | Lintel | 2 | Interior | Heavy Horizontal Cracking - ( ) |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| M/N10 | Lintel | 2 | Interior | Heavy Vertical \& Horizontal Cracking - (2no ) |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| L/M10 | Lintel | 2 | Interior | Heavy Vertical Cracking - (2no ) |  |  |
|  |  |  | Exterior | Localised Spalled Concrete - (4no) |  |  |
| K/L10 | Lintel | 2 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| J/K10 | Lintel | 2 | Interior | Isolated Fine Vertical Cracking - (2no ) |  |  |
|  |  |  | Exterior | Localised Spalled Concrete - (1no) |  |  |
| H/J10 | Lintel | 2 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Localised Spalled Concrete - (1no) |  |  |
| G/H10 | Lintel | 2 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |


| Element Ref: | Type | Level | Face | Notes | Face-by- Face RAG Rating | Combined RAG <br> Rating |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| F/G10 | Lintel | 2 | Interior | Isolated Fine Vertical Cracking - (1no ) |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| E/F10 | Lintel | 2 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| D/E10 | Lintel | 2 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Localised Spalled Concrete - (1no) |  |  |
| D/E4 | Lintel | 2 | Interior | Isolated Fine Vertical Cracking - (1no ) |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| E/F4 | Lintel | 2 | Interior | Isolated Fine Vertical Cracking - (2no ) |  |  |
|  |  |  | Exterior | Isolated Moderate Vertical Cracking - (3no ) |  |  |
| F/G4 | Lintel | 2 | Interior | Isolated Fine Vertical Cracking - (2no ) |  |  |
|  |  |  | Exterior | Isolated Moderate Vertical Cracking - (2no ) |  |  |
| G/H4 | Lintel | 2 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| H/J4 | Lintel | 2 | Interior | Isolated Fine Vertical Cracking - (2no ) |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| J/K4 | Lintel | 2 | Interior | Isolated Heavy \& Moderate Vertical Cracking - (3no ) |  |  |
|  |  |  | Exterior | Visually Sound |  |  |
| K4/5 | Lintel | 2 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Isolated Moderate Vertical Cracking - (2no ) |  |  |
| K5/6 | Lintel | 2 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Isolated Moderate Vertical Cracking - (1no ) |  |  |
| K6/7 | Lintel | 2 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Isolated Moderate Vertical Cracking - (2no ) |  |  |
| J/K7 | Lintel | 2 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Isolated Fine Vertical Cracking - (1no ) |  |  |
| H/37 | Lintel | 2 | Interior | Isolated Moderate Vertical Cracking - (3no ) |  |  |
|  |  |  | Exterior | Isolated Heavy Vertical Cracking - (5no ) |  |  |
| G/H7 | Lintel | 2 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Isolated Moderate Vertical Cracking - (2no ) |  |  |


| Element Ref: | Type | Level | Face | Notes | Face-by- Face RAG Rating | Combined RAG Rating |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| F/G7 | Lintel | 2 | Interior | Isolated Fine Vertical Cracking - (3no ) |  |  |
|  |  |  | Exterior | Isolated Fine Vertical Cracking - (2no ) |  |  |
| E/F7 | Lintel | 2 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Isolated Moderate Vertical Cracking - (2no ) |  |  |
| D/E7 | Lintel | 2 | Interior | Visually Sound |  |  |
|  |  |  | Exterior | Isolated Moderate Vertical Cracking - (3no ) |  |  |

## Appendix B - Condition Rating Plan Drawings

Survey was undertaken in May 2020
Drawing is not to scale
This drawing is for indicative purposes only.


Survey was undertaken in May 2020
Drawing is not to scale
This drawing is for indicative purposes


First Floor

Survey was undertaken in May 2020


Second Floor

## Appendix F

Load Test Solutions Material Testing

# Report 1510-3 

Steel<br>Investigations at former Player Wills Factory

## 22/05/2020

# LOAD TEST SOLUTIONS <br> Structural Testing Specialists 

CONTENTS

1. INTRODUCTION
2. SCOPE OF WORK
3. FINDINGS
4. CONCLUSION

Appendices

APPENDIX A PHOTOGRAPHS

APPENDIX B DRAWINGS
APPENDIX C STEEL HARDNESS TEST REULTS

APPENDIX D TENSILE TEST RESULTS
APPENDIX E CHEMICAL COMOSITION RESULTS

## Steel Investigations - Former Player Wills Factory

## 1. INTRODUCTION

Load Test Solutions was requested by Barrett Mahony Consulting Engineers on behalf of their client to carry out steel investigations and testing at the former Player Wills Factory, South Circular Rd, Dublin 8.

This report presents the findings of the testing and investigation.

## 2. SCOPE OF WORK

The scope of the works is to determine the current condition of steel within the structure through a programme of testing commensurate with testing and inspection techniques used on structures of a similar nature.

The following table shows the testing and examination schedule:
Table 1 Test Quantities

| Test | Beam | Column | Slab reinforcing |
| :--- | :--- | :--- | :--- |
| Tensile strength | 7 | 8 | 17 |
| Steel Hardness | 15 | 6 | N/A |
| Steel diameter | N/A | N/A | 7 |
| Chemical composition | 2 | 3 | 3 |
| Metallographic <br> examination | 0 | 1 | 0 |

### 2.1 THE STRUCTURE

The structure on site consists of a steel and reinforced concrete structure.

## 3. FINDINGS OF STRUCTURAL SURVEYS

The findings of the investigations are detailed below.
A photographic record is provided in Appendix $A$ and drawings of the test areas and locations are included in Appendix B.

Site test results are given in Appendix C
Laboratory testing results are given in Appendix D

### 3.1 STEEL THICKNESS MEASUREMENTS

A measurement of the thickness of reinforcing steel was made at the slab breakout areas. An additional measurement was recorded for reinforcing steel in a window head beam.

## Measurements are noted on the drawings in Appendix B.

### 3.2 STEEL HARDNESS TESTS

Hardness testing was carried out on-site using the Proceq Equitip 3 portable hardness tester.


| Location | Min HV (Vickers) | Max HV (Vickers) | Mean HV (Vickers) |
| :--- | :--- | :--- | :--- |
| First floor main beam | 99 | 183 | 133 |
| First floor main beam | 112 | 174 | 141 |
| First floor main beam | 102 | 162 | 128 |
| First floor sec beam | 84 | 105 | 91 |
| First floor sec beam | 89 | 137 | 118 |
| First floor u column | 97 | 149 | 121 |
| First floor cast column | 116 | 174 | 142 |
| Second floor main beam | 101 | 160 | 129 |
| Second floor main beam | 93 | 108 | 99 |
| Second floor main beam | 128 | 173 | 145 |
| Second floor sec beam | 86 | 159 | 108 |
| Second floor sec beam | 100 | 120 | 109 |
| Second floor u column | 99 | 182 | 143 |
| Second floor rivet column | 93 | 164 | 123 |
| Third floor main beam | 100 | 179 | 125 |
| Third floor main beam | 91 | 182 | 120 |
| Third floor main beam | 99 | 159 | 110 |
| Third floor sec beam | 86 | 145 | 105 |
| Third floor sec beam | 86 | 102 | 94 |
| Third floor u column | 84 | 105 | 91 |
| Third floor u column | 86 | 137 | 108 |
|  |  |  |  |

## Steel Investigations - Former Player Wills Factory

3.3 TENSILE STRENGTH TESTS

Tensile strength tests were carried out by Sandberg LLP in accordance with ISO 6892-1:2016 B
Test results are listed in Appendix D

### 3.4 CHEMICAL COMPOSITION TESTS

Chemical composition tests were carried out by Sandberg LLP and compared to the relevant steel standards for assessment.

Test results are listed in Appendix E

## Appendix A

Photographs


Beam Sample


Column Sample

Steel Investigations - Former Player Wills Factory


Slab Reinforcing Steel

Steel Investigations - Former Player Wills Factory


Roof Slab Reinforcing


Beam above windows reinforcing steel

Appendix B
Drawings






Appendix C

Steel Hardness Test Results

Steel Hardness Test Results

| Location | Min HV (Vickers) | Max HV (Vickers) | Mean HV (Vickers) |
| :---: | :---: | :---: | :---: |
| First floor main beam | 99 | 183 | 133 |
| First floor main beam | 112 | 174 | 141 |
| First floor main beam | 102 | 162 | 128 |
| First floor sec beam | 84 | 105 | 91 |
| First floor sec beam | 89 | 137 | 118 |
| First floor u column | 97 | 149 | 121 |
| First floor cast column | 116 | 174 | 142 |
| Second floor main beam | 101 | 160 | 129 |
| Second floor main beam | 93 | 108 | 99 |
| Second floor main beam | 128 | 173 | 145 |
| Second floor sec beam | 86 | 159 | 108 |
| Second floor sec beam | 100 | 120 | 109 |
| Second floor u column | 99 | 182 | 143 |
| Second floor rivet column | 93 | 164 | 123 |
| Third floor main beam | 100 | 179 | 125 |
| Third floor main beam | 91 | 182 | 120 |
| Third floor main beam | 99 | 159 | 110 |
| Third floor sec beam | 86 | 145 | 105 |
| Third floor sec beam | 86 | 102 | 94 |
| Third floor u column | 84 | 105 | 91 |
| Third floor u column | 86 | 137 | 108 |



INVESTIGATION INSPECTION
MATERIALS TESTING

TENSILE TEST CERTIFICATE BS EN ISO 6892-1:2016 B

Sandberg LLP 40 Grosvenor Gardens London SW1W 0EB

Tel: 02075657000 Fax: 02075657100 email: ho@sandberg.co.uk web: www.sandberg.co.uk

| Certificate: | $66370 / \mathrm{M} / 6$ | Order Ref: | Proforma No. 2 |
| :--- | :---: | :--- | :---: |
| Samples Received: | 13 March 2020 | Tested By: | AT |
| Test Date: | 29 April 2020 | Test Procedure: | M10/3/3 |
| Client Details: | Load Test Solutions Ltd, Unit <br> W2RW, Co Laois, Ireland. |  |  |



Materials, samples and test specimens are retained for a period of 2 months from the issue of the final report.
Opinions and interpretations expressed herein are outside the scope of UKAS accreditation.

INVESTIGATION INSPECTION
MATERIALS TESTING

TENSILE TEST CERTIFICATE BS EN ISO 6892-1:2016 B

Sandberg LLP 40 Grosvenor Gardens London SW1W 0EB

Tel: 02075657000 Fax: 02075657100 email: ho@sandberg.co.uk web: www.sandberg.co.uk

| Certificate: | $66370 / \mathrm{M} / 7$ | Order Ref: | Proforma No. 2 |
| :--- | :---: | :--- | :---: |
| Samples Received: | 13 March 2020 | Tested By: | AT |
| Test Date: | 29 April 2020 | Test Procedure: | M10/3/3 |
| Client Details: | Load Test Solutions Ltd, Unit <br> W2RW, Co Laois, Ireland. |  |  |


| Specimen Reference |  | Area $\mathrm{mm}^{2}$ | Upper Yield |  | Ultimate Tensile |  | Elongation \% |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Met lab Ref | Sample Ref |  | Load kN | Stress $\mathrm{N} / \mathrm{mm}^{2}$ | Load kN | $\begin{aligned} & \text { Stress } \\ & \mathrm{N} / \mathrm{mm}^{2} \end{aligned}$ |  |
| MA 333 | $\begin{gathered} \text { SFSB2 - Beam Web. } \\ 2^{\text {nc }} \text { Floor } \end{gathered}$ | 28.94 | 9.19 | 318 | 13.78 | 476 | 31.5 |
| MA 334 | $\begin{gathered} \text { SFSB3 - Beam Web. } \\ 2^{\text {nc }} \text { Floor } \end{gathered}$ | 28.94 | 8.12 | 281 | 12.28 | 425 | 37.5 |
| MA 335 | SFC1 - Col Web. $2^{\text {nd }}$ Floor | 29.22 | 9.80 | 336 | 12.78 | 437 | 34.0 |
| MA 336 | SFC2 - Col Web. $2^{\text {nd }}$ Floor | 29.42 | 9.96 | 339 | 11.76 | 400 | 37.5 |
| Specification: |  |  |  |  |  |  |  |
|  | BS EN 10025-2:2019 |  |  |  |  |  |  |
|  | Grade S235 |  |  | 235 min |  | 360-510 | 26 min |
|  | Grade S275 |  |  | 275 min |  | 410-560 | 23 min |
|  | Grade S355 |  |  | 355 min |  | 470-630 | 22 min |

Comments: The tensile properties of samples MA 333, MA 334, MA 335 and MA 336 would comply with the requirements for a grade S275 structural steel with the exception of the UTS value for sample MA 336.

Date: 4 May 2020

Neale Fetter - Assistant Manager Metallurgy Department
Materials, samples and test specimens are retained for a period of 2 months from the issue of the final report.
Opinions and interpretations expressed herein are outside the scope of UKAS accreditation.


INVESTIGATION INSPECTION
MATERIALS TESTING

TENSILE TEST CERTIFICATE BS EN ISO 6892-1:2016 B

Sandberg LLP 40 Grosvenor Gardens London SW1W 0EB

Tel: 02075657000 Fax: 02075657100 email: ho@sandberg.co.uk web: www.sandberg.co.uk

| Certificate: | $66370 / \mathrm{M} / 8$ | Order Ref: | Proforma No. 2 |
| :--- | :---: | :--- | :---: |
| Samples Received: | 13 March 2020 | Tested By: | NAF |
| Test Date: | 27-28 April 2020 | Test Procedure: | M10/3/3 |
| Client Details: | Load Test Solutions Ltd, Unit <br> W2RW, Co Laois, Ireland. |  |  |


| Specimen Reference |  | Area $\mathrm{mm}^{2}$ | 0.2\% Proof Stress |  | Ultimate Tensile |  | Elongation \% |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Met lab Ref | Sample Ref |  | Load kN | Stress $\mathrm{N} / \mathrm{mm}^{2}$ | Load kN | $\begin{aligned} & \text { Stress } \\ & \mathrm{N} / \mathrm{mm}^{2} \end{aligned}$ |  |
| $\begin{gathered} \text { MA } 328-1 \\ 1 \end{gathered}$ | SFS1-RC Slab. $1^{\text {st }}$ Floor | 12.88 | 7.62 | 592 | 7.76 | 603 | 17.5 |
| $\begin{gathered} \text { MA } 328- \\ 2 \end{gathered}$ | SFS1 - RC Slab. $1^{\text {st }}$ Floor | 13.07 | 7.84 | 600 | 8.17 | 625 | 17.5 |
| $\begin{gathered} \text { MA } 328- \\ 3 \end{gathered}$ | SFS1 - RC Slab. $1^{\text {st }}$ Floor | 13.07 | 8.35 | 639 | 8.70 | 665 | N/D* |
| $\begin{gathered} \text { MA } 329-1 \\ 1 \end{gathered}$ | $\text { SFS1 - RC Slab. } 2^{\text {nd }}$ <br> Floor | 13.07 | 8.08 | 618 | 8.12 | 621 | 15.0 |
| $\begin{gathered} \text { MA } 329- \\ 2 \end{gathered}$ | SFS1 - RC Slab. $2^{\text {nd }}$ Floor | 12.82 | 8.18 | 638 | 8.26 | 644 | 15.0 |
| $\begin{gathered} \text { MA 329- } \\ 3 \end{gathered}$ | $\text { SFS1 - RC Slab. } 2^{\text {nd }}$ Floor | 12.88 | 7.84 | 609 | 8.13 | 631 | 17.5 |
|  |  |  |  |  |  |  |  |

Comments: * Elongation not determined - final fracture occurred outside gauge length.
Results for the above samples of steel reinforcing wire strand were not assessed for strength grade. This was because no specific client specification was supplied or identified for assessment purposes.

Date: 4 May 2020

## Neale Fetter - Assistant Manager Metallurgy Department

Materials, samples and test specimens are retained for a period of 2 months from the issue of the final report.
Opinions and interpretations expressed herein are outside the scope of UKAS accreditation.


INVESTIGATION INSPECTION
MATERIALS TESTING

TENSILE TEST CERTIFICATE BS EN ISO 6892-1:2016 B

Sandberg LLP 40 Grosvenor Gardens London SW1W 0EB

Tel: 02075657000 Fax: 02075657100 email: ho@sandberg.co.uk web: www.sandberg.co.uk

| Certificate: | $66370 /$ M/9 | Order Ref: | Proforma No. 2 |
| :--- | :---: | :--- | :---: |
| Samples Received: | 13 March 2020 | Tested By: | NAF |
| Test Date: | $27-28$ April 2020 | Test Procedure: | M10/3/3 |
| Client Details: | Load Test Solutions Ltd, Unit <br> W2RW, Co Laois, Ireland. |  |  |


| Specimen Reference |  | Area $\mathrm{mm}^{2}$ | 0.2\% Proof Stress |  | Ultimate Tensile |  | Elongation \% |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Met lab Ref | Sample Ref |  | Load kN | Stress $\mathrm{N} / \mathrm{mm}^{2}$ | Load kN | $\begin{aligned} & \text { Stress } \\ & \mathrm{N} / \mathrm{mm}^{2} \end{aligned}$ |  |
| $\begin{gathered} \text { MA } 330- \\ 1 \end{gathered}$ | SFS2 - RC Slab. $2^{\text {nd }}$ Floor | 12.95 | 8.16 | 630 | 8.32 | 643 | 15.0 |
| $\begin{gathered} \text { MA } 330- \\ 2 \end{gathered}$ | SFS2 - RC Slab. $2^{\text {nd }}$ Floor | 12.82 | 8.14 | 635 | 8.33 | 650 | 17.5 |
| $\begin{gathered} \text { MA } 330- \\ 3 \end{gathered}$ | SFS2 - RC Slab. $2^{\text {nd }}$ Floor | 12.38 | 7.91 | 639 | 8.04 | 650 | 15.0 |
| $\begin{gathered} \text { MA } 337- \\ 1 \end{gathered}$ | $\begin{gathered} \text { R1-RC Slab. } 3^{\text {rc }} \\ \text { Floor } \end{gathered}$ | 13.27 | 7.12 | 537 | 8.76 | 660 | 15.0 |
| $\begin{gathered} \text { MA } 337- \\ 2 \end{gathered}$ | $\begin{gathered} \text { R1 - RC Slab. } 3^{\text {rc }} \\ \text { Floor } \end{gathered}$ | 13.33 | 7.12 | 534 | 8.82 | 662 | 14.0 |
| $\begin{gathered} \text { MA } 337- \\ 3 \end{gathered}$ | $\begin{gathered} \text { R1 - RC Slab. } 3^{\text {rc }} \\ \text { Floor } \end{gathered}$ | 13.14 | 7.53 | 573 | 8.58 | 653 | 17.5 |
|  |  |  |  |  |  |  |  |

Comments: Results for the above samples of steel reinforcing wire strand were not assessed for strength grade. This was because no specific client specification was supplied or identified for assessment purposes.

Date: 4 May 2020

## Neale Fetter - Assistant Manager Metallurgy Department

Materials, samples and test specimens are retained for a period of 2 months from the issue of the final report. Opinions and interpretations expressed herein are outside the scope of UKAS accreditation.

INVESTIGATION INSPECTION
MATERIALS TESTING

TENSILE TEST CERTIFICATE BS EN ISO 6892-1:2016 B

Sandberg LLP 40 Grosvenor Gardens London SW1W 0EB

Tel: 02075657000 Fax: 02075657100 email: ho@sandberg.co.uk web: www.sandberg.co.uk

| Certificate: | $66370 / \mathrm{M} / 10$ | Order Ref: | Proforma No. 2 |
| :--- | :---: | :--- | :---: |
| Samples Received: | 13 March 2020 | Tested By: | NAF |
| Test Date: | 27-28 April 2020 | Test Procedure: | M10/3/3 |
| Client Details: | Load Test Solutions Ltd, Unit <br> W2RW, Co Laois, Ireland. |  |  |



Comments: * Elongation not determined - final fractured occurred within the test machines grips. Results for the above samples of steel reinforcing wire strand were not assessed for strength grade. This was because no specific client specification was supplied or identified for assessment purposes.


Date: 4 May 2020

Neale Fetter - Assistant Manager Metallurgy Department
Materials, samples and test specimens are retained for a period of 2 months from the issue of the final report. Opinions and interpretations expressed herein are outside the scope of UKAS accreditation.

INVESTIGATION INSPECTION
MATERIALS TESTING

TENSILE TEST CERTIFICATE BS EN ISO 6892-1:2016 B

Sandberg LLP 40 Grosvenor Gardens London SW1W 0EB

Tel: 02075657000 Fax: 02075657100 email: ho@sandberg.co.uk web: www.sandbery.co.uk

| Certificate: | $66370 / \mathrm{M} / 3$ | Order Ref: | Email dated 26/09/2019 |
| :--- | :---: | :--- | :---: |
| Samples Received: | 28 October 2019 | Tested By: | AT |
| Test Date: | 01 November 2019 | Test Procedure: | M10/3/3 |
| Client Details: | Load Test Solutions Ltd, Unit <br> W2RW, Co Laos, Ireland. |  |  |



Comments: The tensile properties for samples MZ 1012, MZ 1013, MZ 1014 and MZ 1015 all conformed to the structural steel grade S235.

For Sandberg LLP
Date: 5 November 2019

INVESTIGATION INSPECTION
MATERIALS TESTING

TENSILE TEST CERTIFICATE BS EN ISO 6892-1:2016 B

Sandberg LLP 40 Grosvenor Gardens London SW1W 0EB

Tel: 02075657000 Fax: 02075657100 email: ho@sandberg.co.uk web: www.sandberg.co.uk

| Certificate: | 66370/M/4 | Order Ref: | Email dated 6/12/2019 |
| :--- | :---: | :--- | :---: |
| Samples Received: | 20 December 2019 | Tested By: | NAF |
| Test Date: | 02 January 2020 | Test Procedure: | M10/3/3 |
| Client Details: | Load Test Solutions Ltd, Unit <br> W2RW, Co Laois, Ireland. | Zone 5, Clonminam Business Park, Portlaoise, R32 |  |


| Specimen Reference |  | Area $\mathrm{mm}^{2}$ | 0.2\% Proof |  | Ultimate Tensile |  | Elongation \% |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Met lab Ref | Sample Ref |  | Load kN | Stress $\mathrm{N} / \mathrm{mm}^{2}$ | Load kN | Stress $\mathrm{N} / \mathrm{mm}^{2}$ |  |
| MZ 1251 | Column Sample 7 mm Dia. 75 mm long | 19.09 | 4.280 | 225 | 7.60 | 398 | 18.0 |
| Specification: |  |  |  |  |  |  |  |
|  | EN 10025-2:2019 |  |  |  |  |  |  |
|  | Grade S185 |  |  | 185 min |  | 290-510 | 18 min |
|  | Grade S235 |  |  | 235 min |  | 360-510 | 26 min |
|  | Grade S275 |  |  | 275 min |  | 410-560 | 23 min |
|  | Grade S355 |  |  | 355 min |  | 470-630 | 22 min |

Comments: The tensile properties for samples MZ 1251 conformed to the structural steel grade S185.

Date: 9 January 2020

## Neale Fetter - Assistant Manager - Metallurgy Department

Materials, samples and test specimens are retained for a period of 2 months from the issue of the final report. Opinions and interpretations expressed herein are outside the scope of UKAS accreditation.

Appendix E

Chemical Composition Results

## SANDBURG <br> CONSULTING ENGINEERS

INVESTIGATION INSPECTION MATERIALS TESTING

## TEST CERTIFICATE <br> METALLOGRAPHIC EXAMINATION TO BS EN ISO 643 : 2012

Sand berg LLP 40 Grosvenor Gardens London SW1W 0EB

Tel: 02075657000
Fax: 02075657100
email: ho@sandberg.co.uk web: www.sandberg.co.uk



Comments: Metallographic examination revealed a microstructure comprising of pearlite within a ferritic matrix, with a coarse grain structure. This would be typical of that expected of a low alloy carbon steel material.

For Sandberg LLP


Date: 9 January 2020

## Neale Fetter - Assistant Manager- Metallurgy Department

Materials, samples and test specimens are retained for a period of 2 months from the issue of the final report. Opinions and interpretations expressed herein are outside the scope of UKAS accreditation.


Sandberg IIP
40 Grosvenor Gardens
London SW1W 0EB
Tel: 02075657000
Fax: 02075657100
email: ho@sandberg WW.sand

| Certificate: | 66370/M/2 |  | Samples Received: |  |  | 28 October 2019 |  |  |  | Test Date: |  |  | 31 October 2019 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Reference: | Email dated 26/09/2019 |  | Tested By: |  |  | Metaltech Services Limited |  |  |  | Test Procedure: |  |  | OES |  |  |
| Client Details: | Load Test Solutions Ltd, Unit 2 Zone 5, Clonminam Business Park, Portlaoise, R32 W2RW, Co Laois, Ireland. |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| CHEMICAL COMPOSITION \% |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Met Lab Ref | Client Description |  | C | Si | Mn | S | P | Ni | Cr | Mo | Cu | V | Nb | AI | CEV |
| MZ 1015 |  | Col B/P | 0.23 | 0.01 | 0.54 | 0.024 | 0.052 | 0.02 | <0.01 | $<0.01$ | 0.02 | <0.01 | 0.002 | <0.01 | 0.329 |
| Specification: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | BS EN 10025-2:2019 |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | Grade 5235 (max) | 0.19 | - | 1.5 | 0.045 | 0.045 |  |  |  | 0.60 |  |  |  | 0.35 |
|  |  | Grade S 275 (max) | 0.24 | - | 1.6 | 0.045 | 0.045 |  |  |  | 0.60 |  |  |  | 0.40 |
|  |  | Grade 5355 (max) | 0.27 | 0.6 | 1.7 | 0.045 | 0.045 |  |  |  | 0.60 |  |  |  | 0.45 |
| Comments : |  | Results contained in this certificate are outside the UKAS accreditation for this laboratory but have been performed on our behalf by another laborat Metaltech Services Limited Report No. MSL 4945-1. <br> The above sample MZ 1015 gave high phosphorus content, exceeding the maximum allowable limit for modern structural steels. The CEV value for maximum allowable limits, therefore material of this quality would be considered weldable using standard welding techniques and consumables as sper : Part 2 : 2001, which supersedes withdrawn standard BS $5135: 1984$, however consideration for the high phosphorus content should be made. |  |  |  |  |  |  |  |  |  |  |  |  |  | Neale Fetter - Assistant Manager Metallurgy Department

Materials, samples and test specimens are retained for a period of 2 months from the issue of the final report. Opinions and interpretations expressed herein are outside the scope of UKAS accreditation.
INVESTIGATION INSPECTION

## TEST CERTIFICATE

Sandberg LLP
suaprey douansodo $0 \ddagger$ London SW1W 0EB
Tel: 02075657000
Fax: 02075657100 Fax: 020 75657100
web: www.sandberg.co.uk


[^0]Neale Fetter - Assistant Manager Metallurgy Department
Materials, samples and test specimens are retained for a period of 2 months from the issue of the final report.
Opinions and interpretations expressed herein are outside the scope of UKAS accreditation.
INVESTIGATION INSPECTION

## TEST CERTIFICATE

Sandberg LLP
suaprey douansodo 0t London SW1W 0EB
Tel: 02075657000
Fax: 02075657100 Fax: 02075657100
web: www.sandberg.co.uk


| Comments $:$ | Results contained in this certificate are outside the UKAS accreditation for this laboratory but have been performed on our behalf by another laboratory that is so accredited. <br> Metaltech Services Limited Report No. MSL 5402 <br> Carbon Equivalent Value (CEV) for the above sample was found to be acceptable, and as the material would be considered readily weldable using standard welding techniques <br> and consumables as specified in BS EN 1011: Part $2: 2001$, which supersedes withdrawn standard BS $5135: 1984$. |
| :--- | :--- |

Date: 4 May 2020

## For the attention of Tom Fox

Dear Tom

## Re: Tensile \& Metallographic Testing

Please find attached Certificates 1 to 3 including revised certificate 3 for your records.

Yours sincerely

Amy Tolladay
Senior Technician - Metallurgy Department

Enc.

Materials, samples and test specimens are retained for a period of 2 months from the issue of the final report.
Your attention is drawn to the enclosed sample retention form and we would be grateful if you could complete the form and return it within one month from the date of the report.

Tests reported on sheets not bearing the UKAS mark in this report/certificate are not included in the UKAS accreditation schedule for this laboratory.

Opinions and interpretations expressed herein are outside the scope of UKAS accreditation.

This report is personal to the client, confidential, non-assignable and written with no admission of liability to any third party.

This report shall not be reproduced, except in full, without the written approval of Sandberg LLP.

Where our involvement consists exclusively of testing samples, the results and our conclusions relate only to the samples tested.


INVESTIGATION INSPECTION
MATERIALS TESTING

TEST CERTIFICATE METALLOGRAPHIC EXAMINATION TO BS EN ISO 643:2020

Sandberg LLP
40 Grosvenor Gardens
London SW1W 0EB

Tel: $\quad 02075657000$
Fax: 02075657100 email: ho@sandberg.co.uk web: www.sandberg.co.uk

| Certificate: | $68141 / \mathrm{M} / 1$ | Order Ref: | Proforma Paid 02.09.20 |
| :--- | :---: | :--- | :---: |
| Samples Received: | 26 August 2020 | Tested By: | MC |
| Test Date: | 11 September 2020 | Test Procedure: | M5/3/2 \& M13/3/0 |
| Client Details: | Load Test Solutions Ltd, Unit 2 Zone | 5, Clonminam Business Park, Portlaoise, R32 W2RW. |  |



| Met Lab Ref: | MA 784 | Client Ref: | Col 1 |  |
| :--- | :--- | :--- | :--- | :--- |
| Examined By: | SET | Mag: $\times 84$ | Etchant: $\quad 2 \%$ Nital | Grain Size Index: 6.5 |
| Comments: | Metallographic examination revealed a microstructure comprising of a small amount of pearlite <br> within a ferritic matrix. This would be typical of that expected of a low carbon, low alloy steel <br> material. |  |  |  |
|  |  |  |  |  |

For Sandberg LLP


Date: September 16, 2020

## Simon R P Morris - Senior Associate

Materials, samples and test specimens are retained for a period of 2 months from the issue of the final report. Opinions and interpretations expressed herein are outside the scope of UKAS accreditation.


TEST CERTIFICATE METALLOGRAPHIC EXAMINATION TO BS EN ISO 643:2020

Sandberg LLP
40 Grosvenor Gardens
London SW1W 0EB

Tel: 02075657000
Fax: 02075657100 email: ho@sandberg.co.uk web: www.sandberg.co.uk


| Met Lab Ref: | MA 785 | Client Ref: | Col 2 |  |
| :--- | :--- | :--- | :--- | :--- |
| Examined By: | SET | Mag: $\times 84$ | Etchant: $\quad 2 \%$ Nital | Grain Size Index: 6.5 |
| Comments: | Metallographic examination revealed a microstructure comprising of a small amount of pearlite <br> within a ferritic matrix. This would be typical of that expected of a low carbon, low alloy steel <br> material. |  |  |  |
|  |  |  |  |  |

For Sandberg LLP


Date: September 16, 2020

## Simon R P Morris - Senior Associate

Materials, samples and test specimens are retained for a period of 2 months from the issue of the final report. Opinions and interpretations expressed herein are outside the scope of UKAS accreditation.


INVESTIGATION INSPECTION
MATERIALS TESTING

TENSILE TEST CERTIFICATE BS EN ISO 6892-1:2019 B

Sandberg LLP
40 Grosvenor Gardens London SW1W 0EB

Tel: 02075657000
Fax: 02075657100 email: ho@sandberg.co.uk web: www.sandberg.co.uk

| Certificate: | 68141/M/3/Rev01 | Order Ref: | Proforma Paid 02.09.20 |
| :--- | :---: | :--- | :---: |
| Samples Received: | 26 August 2020 | Tested By: | AT |
| Test Date: | 16 September 2020 | Test Procedure: | M10/3/3 |
| Client Details: | Load Test Solutions Ltd, Unit 2 Zone | 5, Clonminam Business Park, Portlaoise, R32 W2RW. |  |



| Comments: | The tensile properties of samples MA 784 and MA 785 would conform to the requirements for a <br> grade S275 material ( 150 to 200 mm thick). |
| :--- | :--- |

For Sandberg LLP
Date: September 24, 2020


Simon R P Morris - Senior Associate
Materials, samples and test specimens are retained for a period of 2 months from the issue of the final report. Opinions and interpretations expressed herein are outside the scope of UKAS accreditation.

## AUTHORISATION FOR THE RETENTION OF MATERIALS, SAMPLES AND TEST SPECIMENS

Sandberg LLP 40 Grosvenor Gardens
London SW1W 0EB
Tel: 02075657000 Fax: 02075657100 email: ho@sandberg.co.uk web: www.sandberg.co.uk

| CLIENT: | Load Test Solutions |  |  |
| :--- | :--- | :--- | :---: |
| DATE REPORT ISSUED: | 24 September 2020 | JOB NO: |  |

Materials, samples and test specimens are retained for a period of 2 months from the issue of the final report. Thereafter we will either dispose of them or retain them for a further period, whichever you require. However, we cannot accept requests for indefinite retention and the maximum period of retention without review by yourselves is 6 months.

A charge is made for storage at $£ 50$ per $0.025 \mathrm{~m}^{3}$ (approximately one cubic foot) or part thereof per quarter commencing at the end of our standard 2 month retention period. You will be invoiced for the storage charges at the start of each quarterly period.

If you wish to retain them for a specified period, or if you intend to collect any of these items, please complete the form below and return it to the Grosvenor Gardens address with 1 month.

## PLEASE KEEP UPPER HALF FOR REFERENCE

PLEASE COMPLETE 'A’ OR 'B’ AND RETURN IF APPROPRIATE
A. Please RETAIN/PREPARE FOR COLLECTION* all materials.

* Delete as appropriate

If materials are to be retained please give retention period


If materials are to be collected please give intended date of collection

B. If you require only certain materials, samples or test specimens to be retained or collected please describe them below and give retention period or intended collection date.
(Any material not listed will be disposed)

| TO BE RETAINED/COLLECTED (delete as appropriate) |  |  | JOB NO: |
| :--- | :--- | :--- | :--- |
| Contact Name |  | Signature |  |
|  |  |  |  |
| Company |  | Date |  |

## Barrett Mahony Consulting Engineers

## Dublin:

Sandwith House,
52-54 Lower Sandwith Street,
Dublin 2,
D02 WR26, Ireland.
Tel: +353 16773200

## London:

12 Mill Street,
London, SE1 2AY,
United Kingdom
Tel: +44 2037503530.
Sofia:
19 Yakubitsa Street,
Lozenets,
Sofia 1164,
Bulgaria
Tel: +359 24949772


[^0]:    Results contained in this certificate are outside the UKAS accreditation for this laboratory but have been performed on our behalf by another laboratory that is so accredited. RoTech Laboratories Report No. 20-05033. RoTech Laboratories Report No. 20-05033.

    Materials are a Carbon-Manganese steel with no intentional alloying, the Sulphur and Phosphorous levels are high for steel. If the materials are to be welded consideration on the low CEV, High Sulphur and Phosphorus levels must be taken. The material is not considered readily weldable according to BS EN 1011, thus it would be prudent to seek advice of a welding engineer prior to welding the material.

