# BARRETT MAHONY CONSULTING ENGINEERS CIVIL & STRUCTURAL

























Proposed Strategic Housing Development on the Former Player Wills Site and Undeveloped Land Owned by Dublin City Council at South Circular Road, Dublin 8.

**Structural Assessment Report for Planning** 

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PROJECT: PROPOSED STRATEGIC HOUSING DEVELOPMENT ON THE FORMER PLAYER WILLS

SITE AND UNDEVELOPED LAND OWNED BY DUBLIN CITY COUNCIL AT SOUTH

**CIRCULAR ROAD, DUBLIN 8.** 

**PROJECT NO.** 19.117

DOCUMENT TITLE: STRUCTURAL ASSESSMENT REPORT FOR PLANNING

**DOCUMENT NO:** 19.117 – PWFR – 01

Issue	Date	Description	Orig.	PE	PD	Issue Check
PL1	06/11/2020	ISSUE FOR PLANNING	CV	COR	CK	COR
PL2	11/12/2020	ISSUE FOR PLANNING	CV	COR	CK	COR

STRUCTURAL ASSESSMENT REPORT
FOR
PROPOSED PLAYER WILLS SHD
AT
SOUTH CIRCULAR ROAD,
DUBLIN 08

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#### 1.0 INTRODUCTION

#### 1.1 INTRODUCTION

DBTR-SCR1 Fund, a Sub-Fund of the CWTC Multi Family ICAV intend to apply to An Bord Pleanála for permission for a mixed-use Build to Rent Strategic Housing Development at the former 'Player Wills' site (2.39 hectares) and adjoining lands (0.67 hectares) under the control of Dublin City Council. A public park, public road and works to South Circular Road and to facilitate connections to municipal services at Donore Avenue are proposed on the Dublin City Council land. The former 'Player Wills' site incorporates Eircode's: D08 T6DC, D08 PW25, D08 X7F8 and D08 EK00 and has frontage onto South Circular Road, St. Catherine's Avenue and Donore Avenue, Dublin 8. The Dublin City Council undeveloped land adjoins the former 'Player Wills' site to the west and the former 'Bailey Gibson' site to the east. The total area of the proposed development site is 3.06 hectares.

The design rationale is to create and deliver a high quality, sustainable, residential led mixed use strategic housing development within this inner city brownfield site which respects its setting and maximises the site's natural attributes while achieving maximum efficiency of existing infrastructure. The Proposed Site Layout is illustrated on Drawing No. PL0003 contained within the architectural suite of drawings.

The development will consist of;

- i. the demolition of all buildings (15,454 sq.m GFA), excluding the original fabric of the former Player Wills Factory, to provide for the development of a mixed use(residential, community, arts and culture, creche, food and beverage and retail) scheme comprising predominantly build to rent apartment dwellings (492 no.) together with a significantly lesser quantity of single occupancy shared accommodation private living areas (240 no.), with an average private living floor area of 24.6 sq.m (double the minimum private living space size required for single occupancy shared accommodation) and a arts/culture/community hub within the repurposed ground floor of the former factory building;
- ii. change of use, refurbishment, modifications and alterations to the former Player Wills Factory building (PW1) to include the removal of 1 no. later addition storey (existing 4th storey) and the later addition rear (northern) extension, retention and modification of 3 no. existing storeys and addition of 2 no. storeys set back on the building's south, east and west elevations with an 8-storey projection (max. height 32.53m) on the north eastern corner, with a cumulative gross floor area of 17,630 sq.m including ancillary uses, comprising;
  - at ground floor 852 sq.m of floor space dedicated to community, arts and cultural
    and exhibition space together with artist and photography studios (Class 1 and
    Class 10 Use), 503 sq.m of retail floor space (Class 1 Use), 994 sq.m of
    café/bar/restaurant floor space, 217 sq.m of co-working office floor space (Class
    3 Use) and ancillary floor space for welfare facilities, waste management and
    storage;
  - b. 240 no. single occupancy shared accommodation private living areas, distributed over levels 1-4, including 2 no. rooms of 30 sq.m, 49 no. rooms of 25 sq.m; 14 no. rooms of 23 sq.m, 58 no. rooms of 22.5 sq.m, 8 no. rooms of 20 sq.m, 104 no. rooms of 19 sq.m and 5 no. disabled access (Part M) rooms (3 no. 32 sq.m and 2 no. 26 sq.m); 21 no. kitchen/dining areas, and, 835 sq.m of dedicated shared accommodation services, amenities and facilities distributed across levels 1-4, to accommodate uses including lounge areas, entertainment (games) area, 2 no.

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- external terraces (Level 03 and 04), laundry facilities, welfare facilities and waste storage;
- c. 47 no. build-to rent apartments distributed across levels 1-7 including 12 no. studio apartments; 23 no. 1 bed apartments, 8 no. 2 bed apartments: and, 4 no. 3-bed apartments;
- d. 1,588 sq.m of shared (build to rent and shared accommodation) services, amenities and facilities including at ground floor reception/lobby area, parcel room, 2 no. lounges and administration facilities; at Level 01 entertainment area, TV rooms, entertainment (games room), library, meeting room, business centre; at Level 02 gym and storage and at Level 07, a lounge area.
- e. Provision of communal amenity outdoor space as follows; PW1 450 sq.m in the form of roof terraces dedicated to shared accommodation and 285 sq.m roof terrace for the proposed apartments .
- f. a basement (190 sq.m) underlying the proposed 8-storey projection to the northeast of PW1 to accommodate plant.
- iii. the construction of 445 no. Build to Rent apartment units, with a cumulative gross floor area of 48,455 sq.m including ancillary uses distributed across 3 no. blocks (PW 2, 4 and 5) comprising;
  - a. PW2 (45,556 sq.m gross floor area including ancillary uses) 415 no. apartments in a block ranging in height from 2-19 storeys (max. height 63.05m), incorporating 16 no. studio units; 268 no. 1 bed apartments, 93 no. 2 bed apartments and 38 no. 3-bed apartments. At ground floor, 2 no. retail unts (combined 198 sq.m) (Class 1 use), and a café/restaurant (142 sq.m). Tenant services, amenities and facilities (combined 673 sq.m) distributed across ground floor (lobby, mail room, co-working and lounge area), Level 06 (terrace access) and Level 17 (lounge). Provision of communal amenity open space including a courtyard of 1,123 sq.m and roof terraces of 1,535 sq.m
  - b. Double basement to accommodate car parking, cycle parking, waste storage, general storage and plant.
  - c. PW4 (1,395 sq.m gross floor area including ancillary uses) 9 no. apartments in a part 2-3 storey block (max. height 10.125m) comprising, 2 no. 2-bed duplex apartment units and 7 no. 3-bed triplex apartment units. Provision of communal amenity open space in the form of a courtyard 111 sq.m
  - d. PW5 (1,504 sq.m gross floor area including ancillary uses) 21 no. apartments in a 4 storey block (max. height 13.30m) comprising 12 no. studio apartments, 1 no. 1-bed apartment, 5 no. 2-bed apartments, and 3 no. 3-bed apartments. Provision of communal amenity space in the form of a courtyard 167sq.m. Provision of communal amenity open space in the form of a courtyard 167 sq.m
- iv. the construction of a childcare facility (block PW4) with a gross floor area of 275 sq.m and associated external play area of 146 sq.m;
- v. the provision of public open space with 2 no. permanent parks, 'Players Park' (3,960 sq.m) incorporating active and passive uses to the northwest of the former factory building on lands owned by Dublin City Council; 'St. Catherine's Park' (1,350 sq.m) a playground, to the north east of the Player Wills site adjacent to St. Catherine's National School. A temporary public park (1,158 sq.m) to the northeast of the site set aside for a future school extension. The existing courtyard (690 sq.m) in block PW1 (former factory building) to be retained and enhanced and a public plaza (320 sq.m) between proposed blocks PW and PW4.
- vi. 903 no. long-stay bicycle parking spaces, with 861 no. spaces in the PW2 basement and 42 no. spaces at ground level in secure enclosures within blocks PW4 and PW5. 20 no. spaces reserved for non-residential uses and 110 no. short-stay visitor bicycle spaces provided at ground level.

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- vii. 4 no. dedicated pedestrian access points are proposed to maximise walking and cycling, 2 no. from South Circular Road, 1 no. from St. Catherine's Avenue and 1 no. from Donore Avenue.
- viii. in the basement of PW2, 148 no. car parking spaces to serve the proposed build to rent apartments including 19 no. dedicated disabled parking spaces and 6 no. motorcycle spaces. 20 no. spaces for a car sharing club ('Go Car' or similar). 10% of parking spaces fitted with electric charging points.
- ix. in the basement of PW2, use for 81 no. car parking spaces (1,293 sq.m net floor area) including 5 no. dedicated disabled parking spaces, 3 no. motorcycle spaces and 10% of parking spaces fitted with electric charging points to facilitate residential car parking associated with future development on neighbouring lands. The area will not be used for carparking without a separate grant of permission for that future development. In the alternative, use for additional storage (cage/container) for residents of the proposed development.
- x. 37 no. surface level car parking spaces including 3 no. disabled access and 3 no. creche set down spaces and 10% fitted with electric charging points. 2 no. loading bays and 2 no. taxi set-down areas.
- xi. development of internal street network including a link road (84m long x 4.8m wide) to the south of the proposed 'Players Park' on land owned by Dublin City Council that will provide connectivity between the former 'Bailey Gibson' site and the 'Player Wills' site.
- xii. vehicular access will be provided via Donore Avenue with a one-way exit provided onto South Circular Road to the east of block PW1(the former factory building);
- xiii. replacement and realignment of footpaths to provide for improved pedestrian conditions along sections of Donore Avenue and South Circular Road and realignment of centreline along sections of Donore Avenue with associated changes to road markings;
- xiv. a contra-flow cycle lane is proposed at the one-way vehicular exit to the east of PW1 (former factory building) to allow 2-way cycle movements via this access point;
- xv. decommissioning of existing 2 no. ESB substations and the construction of 2 no. ESB substations and associated switch rooms, 1 no. single ESB substation in PW 1 (43.5 sq.m) and 1 no. double ESB substation in PW2 (68 sq.m);
- xvi. the construction of a waste and water storage building (combined 133 sq.m, height 4.35m) to the west of building PW1;
- xvii. all ancillary site development works; drainage, rooftop solar photovoltaics (20 no. panels total), landscaping, boundary treatment and lighting.

This report focuses on the existing factory building, referenced as block PW1, the majority of which is proposed to be retained and integrated into the new development.

#### **1.2** EXISTING STRUCTURE

The factory building structure consists of a masonry clad steel frame with insitu concrete slabs. The building was constructed in a number of phases dating from 1924-1949. The original building was a two-storey structure, with an additional level constructed in stages between the 1920 and 1930s. The third storey maintains the structural grid of the levels below, with a reduction in the column sizes to that of the lower floors. Also, in the late 1920's the building was extended to the north, with the internalization and removal of a significant portion of the original northern façade. The fourth storey, constructed in 1949, covers only part of the building footprint and does not maintain the same structural grid. This forth level is proposed to be demolished. Refer to Figure 1.1.

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Figure 1.1 – Player Wills Factory – Construction Stages.

At the time of BMCE's appointment, the factory building had been derelict for some time. The building roof drainage outlets were blocked almost throughout and waterproof membranes on the roof had failed, leading to significant water ingress and associated deterioration of both structural and non-structural elements (refer to Photos 1-10 in Appendix A). In addition, the factory contained a high proportion of Asbestos Containing Materials (ACM's). No design or as-built information was available in relation to the building structure.

A large-scale asbestos remediation project was carried out on the building, along with an initial strip out, removal of all non-structural partitions from within the building, to allow better assessment of the original building structure.

Upon completion of those works, a schedule of structural opening-up works and fabric testing was prepared to allow a structural assessment of the building be carried out. The following testing was carried out over a number of months:

- Exposure of existing pad and strip footings at all typical locations.
- Concrete core sampling and compressive testing of suspended slabs at levels 1,2
   & 3.
- Slabs exposures at levels 1,2 & 3 to determine slab depths, reinforcement details, cover.
- Steel sampling from typical columns and beams on all floors for strength tensile testing and metallurgy analysis (some testing ongoing).
- Surveying of the brick and concrete encased steel structure within the external brick facade.
- Cathodic protection trials of encased steel subsequently (ongoing).

Investigation works pertaining to the primary structural elements are discussed in more detail below. At the time of preparation of this report, some of the investigations into the external façade are ongoing. A mark-up of our findings of the primary steel frame is provided in Appendix B.

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#### 2.0 STRUCTURAL INVESTIGATIONS

This section discusses the various structural investigation works which have been carried out to enable an assessment of the existing structure and subsequently design for the proposed new building. Refer to the following appendices for further details of these opening up and testing regime:

- Appendix D United Metals Investigation Works;
- Appendix E McFarland Consulting Façade Steelwork Survey
- Appendix F Load Test Solutions Material Testing.

#### 2.1 STEEL FRAME

#### 2.1.1 Steel Sections and Properties

Due to the age of the structure, the steel sections sizes are not standard section sizes as used today. To establish section properties, dimensional measurements were carried out to compare the steel sections against historical imperial size section tables. At the time of construction of this building, the use of mild steel had started to become commonplace but cast iron and wrought iron steel was still available as a structural building product (refer to Photos 11-15 for images of the steel structure). To establish definite material properties, a number of steel samples were taken from external façade columns, internal columns and beams, over a number of floors, due to the different construction stages. The results of this testing confirmed that the steel used to construct this building was mild steel, generally comparable in its material properties to that commonly in use today, although to a lower design strength than typically adopted in modern construction. The results for the steel testing can be seen in Appendix F.

#### 2.1.2 <u>Ground and First Floor Internal Columns</u>

The ground floor columns are 180mm diameter solid steel sections and the first floor columns are 160mm diameter solid steel sections. Initial testing of the steel concluded that it is mild steel, however tensile testing indicate that the steel grade for these columns is less than the expect S235. Three tests across various columns indicate the steel stress capacity is 215N/mm². Our calculations show that these columns are sufficient for the proposed new building loads above, including the additional levels based on the lightweight form of construction as discussed in Section 3.2 below

#### 2.1.3 Second Floor Internal Columns

The roof over the second floor (third floor) was constructed in two separate phases. The earlier phase consisted of the west wing of the building north of the first three bays back from the South Circular Road. This was built in the late 1920's and here the columns are 100mm diameter solid steel sections. These columns do not have the capacity to support the proposed additional levels due to their slender cross section. These columns will need to be replaced to provide sufficient capacity for support of the proposed additional floors.

The remainder of the roof over the second floor (third floor) was constructed in the 1930's, and here the columns are universal beam sections to historic imperial section tables. Testing confirms the applicable strength grade as S235. Calculations carried out to date show that these columns are also insufficient in strength to cater for the proposed extended building loads, and they will need to be replaced to provide sufficient capacity for support of the proposed additional floors.

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#### 2.1.4 <u>Perimeter Steel Frame</u>

During the investigations, it was discovered that the external brick façade piers encase structural steel columns, and that the concrete lintels are an encasement to structural steel beams (refer to Photos 16-20 in Appendix A). Corrosion of the steelwork was noted in the initial opening up works and the results of this initial opening up can be seen in Appendix E. As a result, specialist cathodic protection testing has been commissioned so as to investigate its effectiveness of protecting the steel within the facade. This is to establish if this method of corrosion protection will be successful in preventing further corrosion of the structural steelwork, which would affect its loadbearing capacity, and also result in expansive corrosion having deleterious effects on the encasing brick façade. This cathodic protection testing has commenced and a report outlining the findings and long term corrosion protection for the encased steel elements will be produced upon completion of the testing.

Upon completion of this testing, an analysis of the perimeter steelwork for the proposed development will be undertaken, and any strengthening works required identified. Where any invasive works are required to strengthen the steelwork within the façade, this work will primarily be carried out from within the building.

#### 2.1.5 First and Second Floor Beams

The first and second floor beams are generally identical in layout and section size. Tensile testing indicates that a strength grade of at least S235 could be used, and up to S275 in place. Calculations show that these beams are sufficient for the proposed new building loads at level 1 and 2, including the higher loaded areas (communal and gym area).

#### 2.1.6 Third (roof) Floor Beams

As noted in Section 2.1.3, the third level was constructed in two phases, after the main building was complete. Both primary and secondary beam sizes (in both phases) at this level are smaller than that of the floor below. Tensile testing indicates that a strength grade of S275. Calculations show that these beams are insufficient for the proposed new building loads.

The primary beams would have to be significantly strengthened to support the transferred columns for the proposed new structure above. These strengthening works would likely be invasive, result in major alterations to the original structure. Additional secondary transfer beams would be required at the lines of support for the new structure above, and to supplement the existing secondary beams so as to reduce the load per beam.

#### 2.2 SLAB ON GRADE

A number of ground floor slab exposures were carried out. To do this, in conjunction with footing exposures, the slab was locally saw-cut and removed to expose typical cross sections of the slab. The existing ground floor slab consists of a 180mm thick slab (thickness varies slightly due to variable subgrade levels) over a crushed rock base (refer to Photo 21-22 in Appendix A). The slab does not have either a radon barrier or damp-proof membrane in place. It also does not have any insulation. All of the above was expected given the age of the structure. To comply with the requirement of current building regulations, along with necessary works to install new drainage and other sub-floor services, it will be necessary to remove the existing ground floor slab and replace this will a new slab with a compliant radon and damp-proof membrane and insulation.

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#### 2.3 SUSPENDED SLABS

Local opening of the existing slabs (approximately 500mm\*500mm) was carried out at each area related to a different construction period. The concrete around the reinforcement was broken away to identify the type, spacing and size of the reinforcement, along with concrete cover for determination of exposure and fire rating capacity (refer to Photos 23-27 in Appendix A). Concrete core samples were taken for compressive testing. Several samples of the reinforcement were also taken for tensile testing.

Non-structural screed containing timber batons at regular spacings have been cast above the structural slabs on levels 1 and 2. Given that the building was exposed to years of wet and damp conditions, these timber batons have rotted. To ensure the new construction is not subject to the potential effects of leaving these screeds in place, the screeds shall be removed and replaced with new non-structural floor screeds.

#### 2.3.1 First and Second Floor Slabs

The first and second floor slabs consist of 114-120mm reinforced concrete structural slabs with 65-75mm thick non-structural screeds. The reinforcement consists of 4.1-4.3mm diameter round wire bars. Tensile testing on several steel samples confirmed the yield strength to be at least 500N/mm². Compressive tests were carried out on concrete core samples which returned results in the range of 28.8-56.2N/mm². Our analysis of these slabs confirms capacity to cater for the proposed new floor loads at these levels, including communal and gym areas. Results of the material testing are included in Appendix F.

The floor slab at both levels can provide the required fire rating without additional work.

#### 2.3.2 Third (roof) Slab

The section of this slab constructed in the later 1920's covering the west wing of the building (approximately 30% of the full floor area) had a similar thickness, strength and reinforcement content to the original levels 1 and 2.

The section of the floor constructed in the 1930's has a slab thickness between 98-107mm. The reinforcing steel used in the slab is a wound wire type steel. The tensile test results for this slab show yield strengths as low as 384N/mm2, with a much lower quantity of tensile steel than provided in the other slabs. The cover to the reinforcement in this slab was found to be as little as 10mm.

#### 2.4 FOUNDATIONS

A number of footing exposures were carried out, typically two each at internal atrium columns location, internal columns and at external façade piers (refer to Photos 28-31 in Appendix A). These exposures comprised of locally removing the ground floor slab around each element to establish the footing type, size, depth and founding material. As expected, all foundations were found to be conventional concrete spread footings, with tiered bases which were common at the time of construction. The concrete was found to be in good condition. Compressive tests on core samples were also carried out, giving results of 59.1 and 61.3 N/mm2. The footings are founded on a soft to firm brown boulder clay with relatively low bearing capacity of 80kN/m2.

An assessment of the building loads was carried out to compare the proposed five level residential development to that of the original three level factory building. Due to the reduction in live loading,

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it is possible to found the proposed development on the existing foundations without additional strengthening, once any new concrete elements (floor slabs/screeds) are kept to a minimum, and the new roof constructed from lightweight material.

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#### 3.0 FINDINGS AND RECOMMENDATIONS

#### 3.1 FINDINGS

An extensive amount of testing, opening up and structural assessment has been carried out to determine the capacity of the existing structure of the Player Wills Factory Building, with some testing yet to be complete.

It was found that the foundations have the capacity for the proposed development once the additional building load does not exceed the original building loads.

It was found that the primary steel beams and concrete slabs for the First and Second Floor have the capacity for the proposed development.

Based on the proposed structure for the new levels, the existing internal 160mm diameter columns at First floor level and the 180mm diameter columns at Ground floor level have capacity for the proposed development. Further assessment is being carried out on the cathodic protection trials for the external façade columns to confirm they have capacity for the proposed development.

The third level extension to the original two storey building has been found to be inferior in quality and strength to that of the original building. The existing columns on the top level are small, and only fit for minor building loads. Likewise, the beams are undersized to take even typical floor loads as they were originally designed to support the roof.

The slab at this level is of very poor quality. The slab thickness, at less than 100mm, does not meet the minimum thickness required for 90 minute fire rating. Both the reinforcement quantity and tensile strength are very low resulting in an insufficient flexural strength in the slab, even for residential floor loads.

#### 3.2 RECOMMENDATIONS

Considering the extremely poor quality of the existing roof slab, and low capacity of the supporting steel structure at level 2, it is recommended that the third floor structure, including the columns from Level 2 up, be replaced with a new structural steel and composite metal slab (approximately 110mm thick). This new structure would be designed so as to be suitable to transfer the loads from the new structure above to the existing structure below.

The façade, and the perimeter columns within the façade build up, would be protected and retained. Temporary works would be required during the construction works of the new third floor.

A cross section of the proposed structure for the additional levels for the development, including the replaced Level 3 is provided in Appendix C. This structure will require to be constructed from lightweight materials so as to allow the existing columns up to Level 2 and foundations be re-used.

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# Appendix A

Photographs

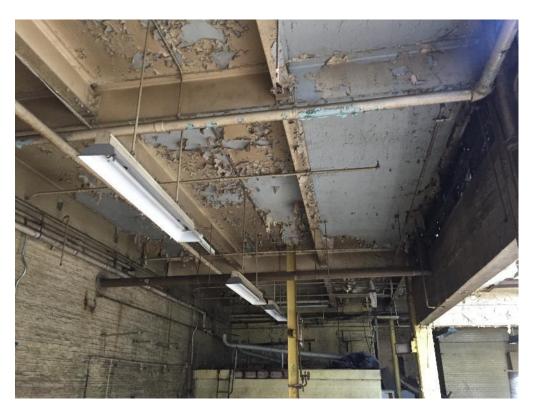


Photo 1: Original Building Condition

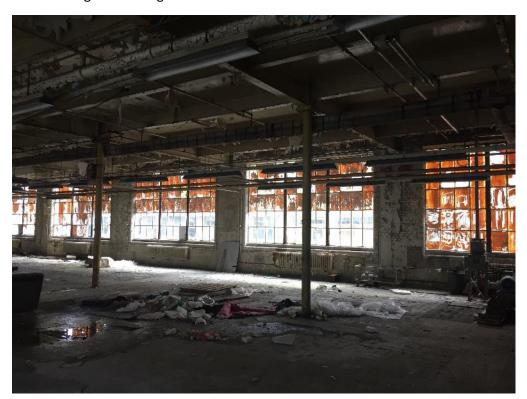


Photo 2: Original Building Condition

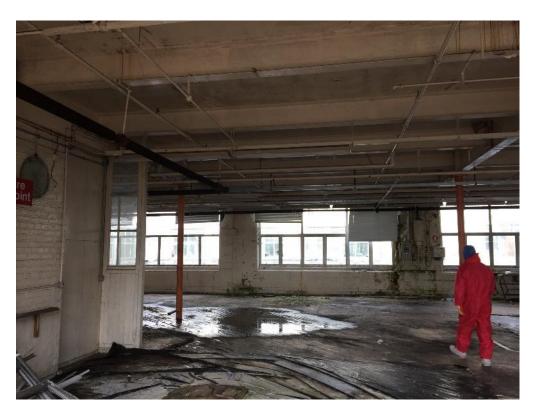


Photo 3: Original Building Condition

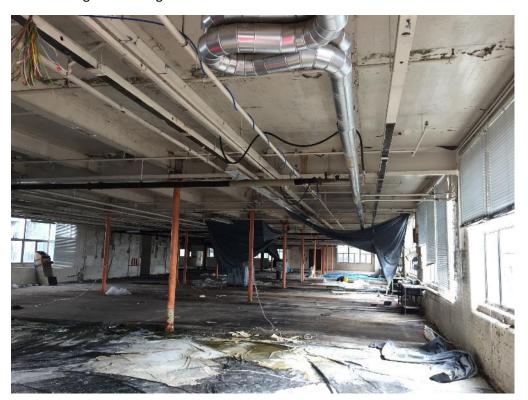


Photo 4: Original Building Condition



Photo 5: Original Building Condition



Photo 6: Original Building Condition



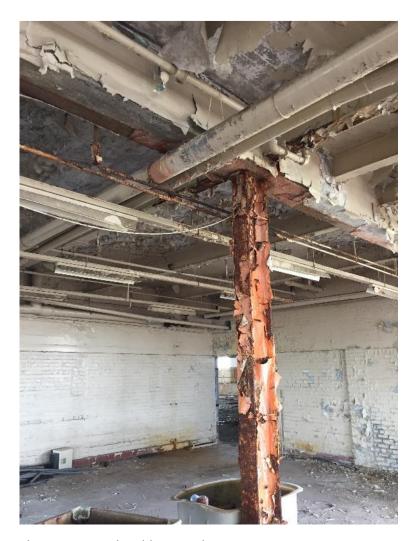


Photo 7: Original Building Condition



Photo 8: Original Building Condition



Photo 9: Original Building Condition





Photo 10: Original Building Condition



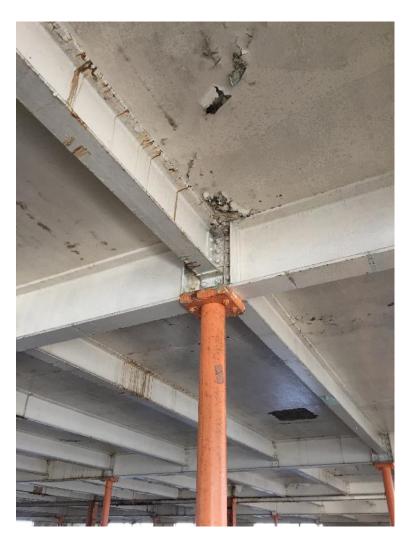


Photo 11: Typical Ground/First Column and beam



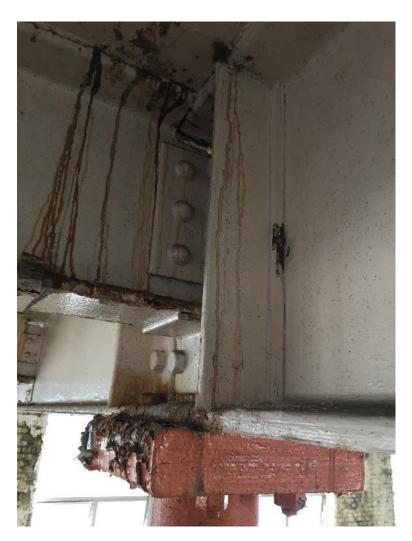


Photo 12: Typical column head connection



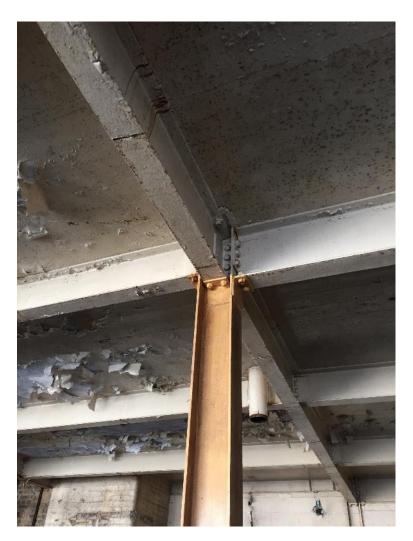


Photo 13: Level 2 column (1930's section) with level 3 beams





Photo 14: Level 2 column for 1920's section





Photo 15: Level 2 in 1930's section



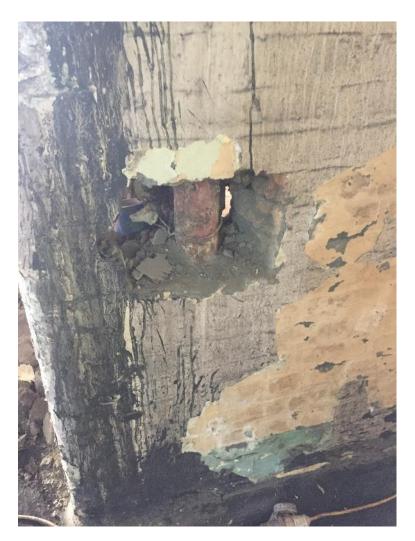


Photo 16: Embedded Steel





Photo 17: Embedded Steel



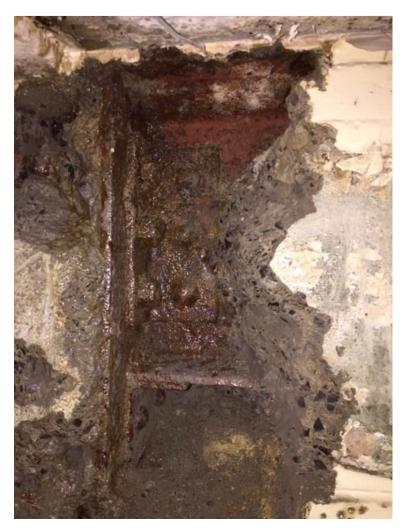


Photo 18: Embedded Steel





Photo 19: Embedded Steel





Photo 20: Embedded Steel



Photo 21: Ground Floor Slab



Photo 22: Ground Floor Slab



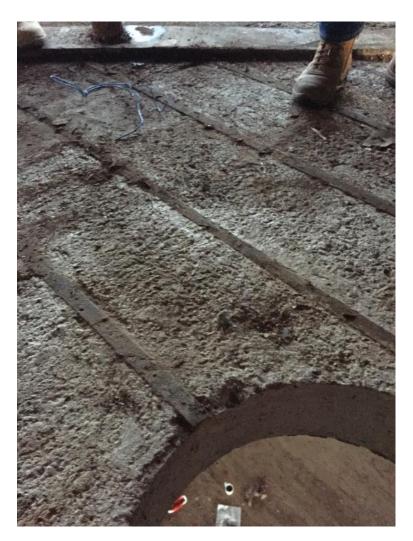


Photo 23: Core sample, with non-structural screed with timber batons



Photo 24: Core Sample



Photo 25: Level 1 Reinforcement



Photo 26: Level 2 reinforcement



Photo 27: Level 3 reinforcement





Photo 28: Tiered spread footing



Photo 29: Tiered spread footing



Photo 30: Tiered spread footing

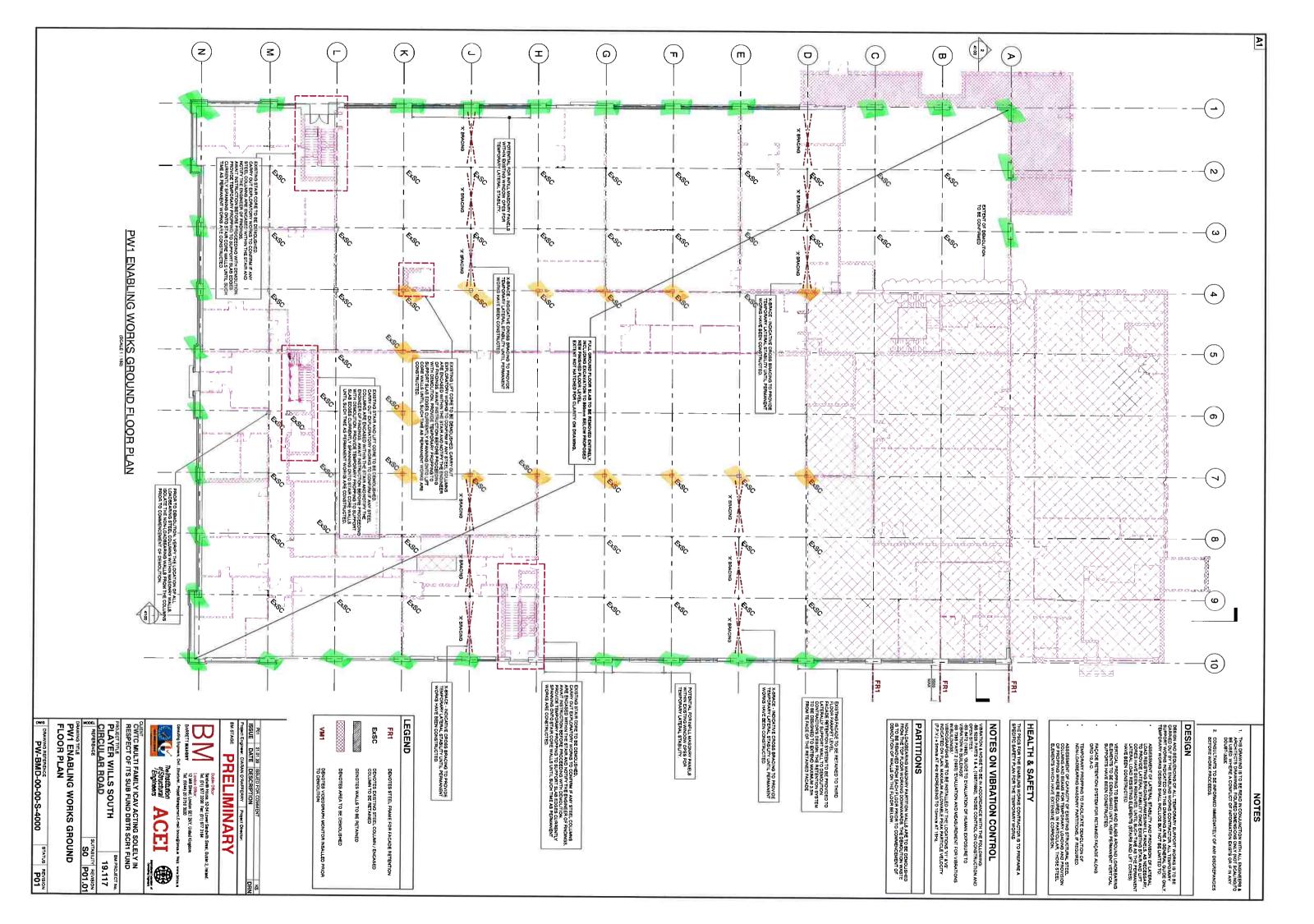


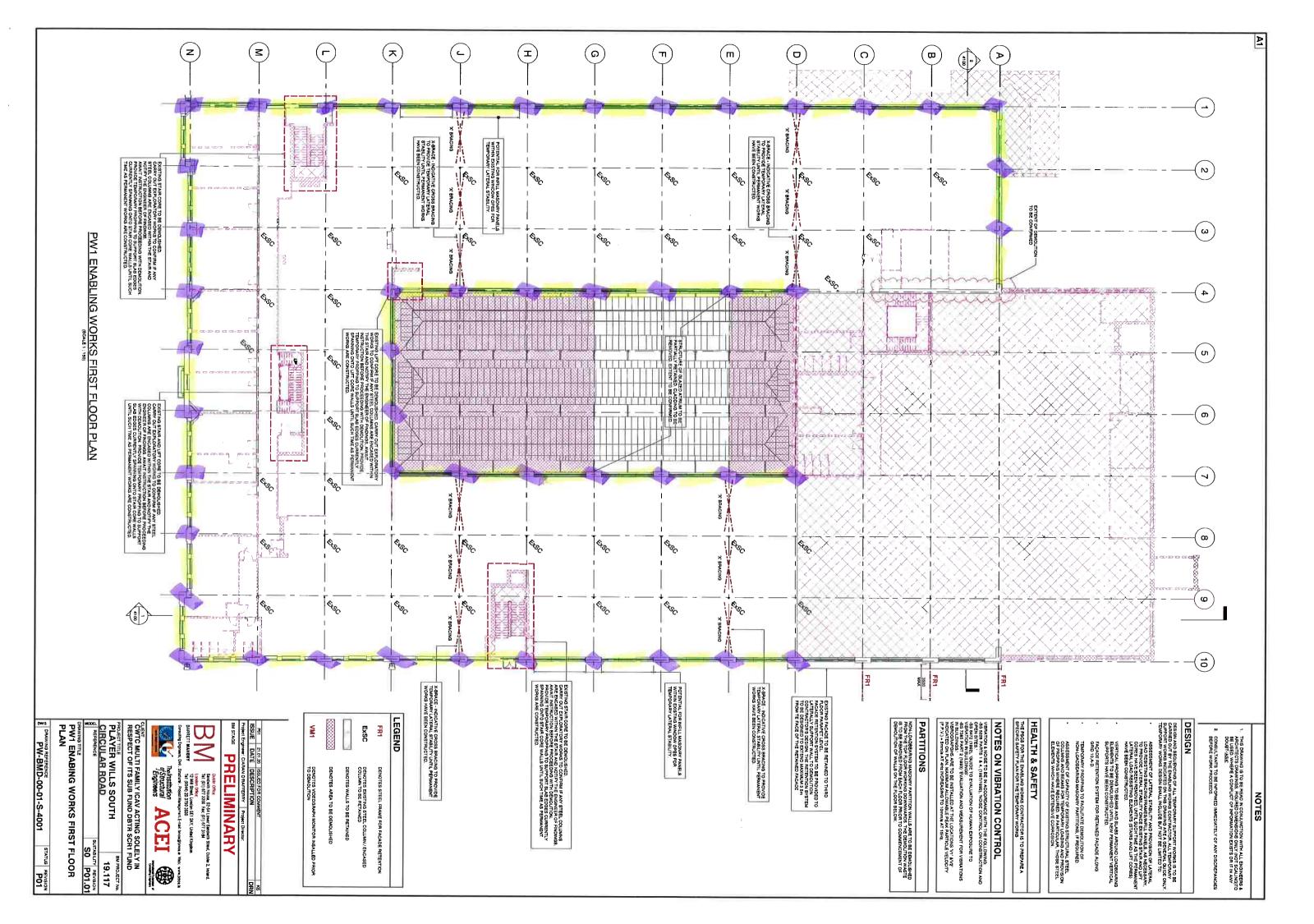


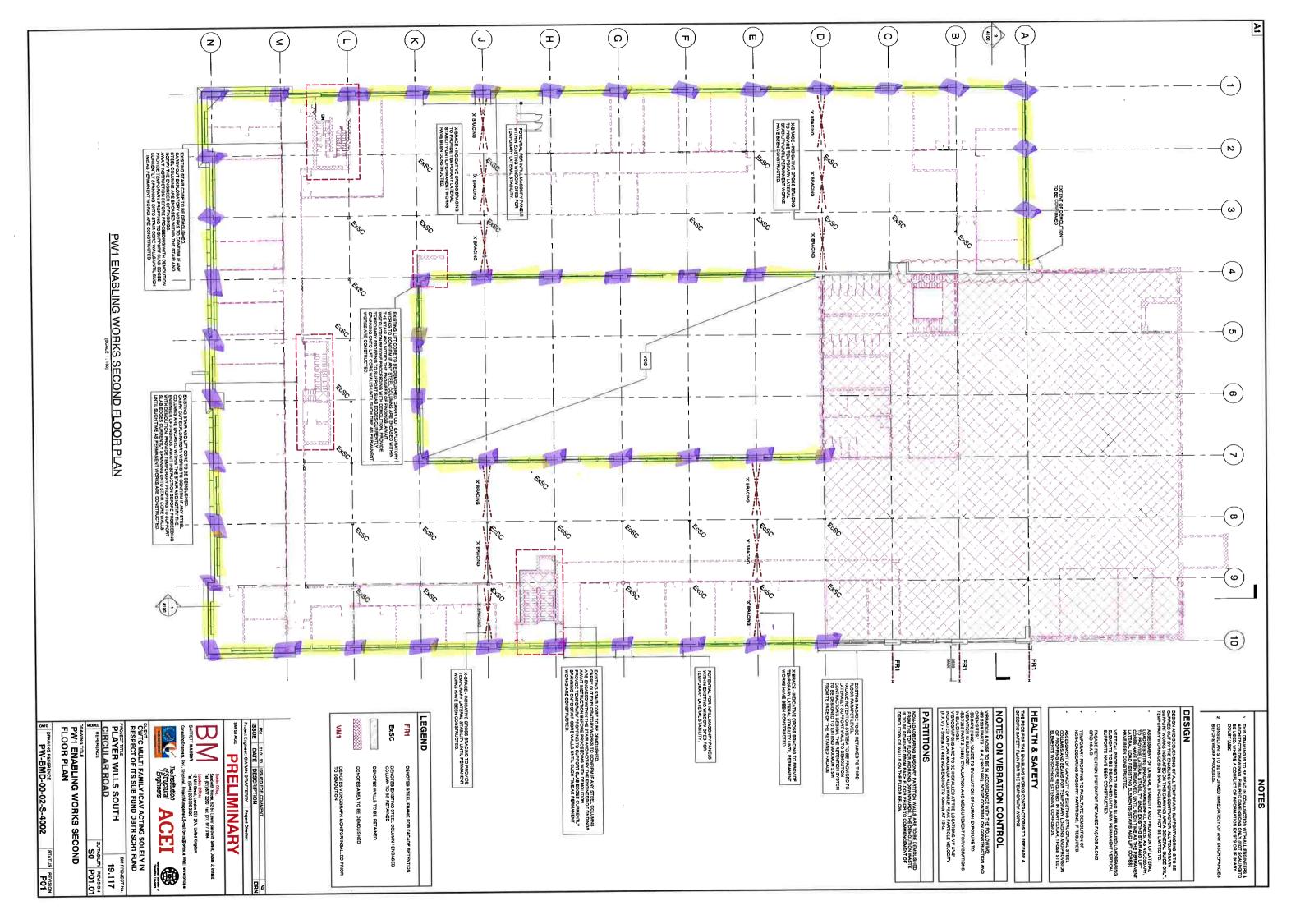
Photo 31: Tiered spread footing

# Appendix B

**Existing Structure Mark-up** 









Project Title: PLAY	ER WILLS	SITE J	ob No: 19.117			
Part of Structure: Ex い	STING EXT	ERNAL + ATR	um coun	RM		
Originator: Date: 25/02/2020 Sheet No:  BARRETT MAHONY						
Calculation Status: Pre	eliminary 🔲 Pla	anning Tender Tender	Construction			
REF. CALCULATION	NS			ОИТРИТ		
GROWD 550	TO FIRST PLA	O'X 6" (REFER	R TO HISTO (ACHED)			
1560	490	HISTO RICA	SECTIONS)  OF 250x 12			

HONY

Project Title:			Job No:				
Part of Structure:					$_{-}$ $HIM$		
Originator:	Checker:	Date:	Sheet No	):	BARRETT MAHONY		
Calculation Status:	Preliminary	Planning	Tender	Construction			
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Typica	TYPICAL 3rd PLOOR PERLIMETER BEAM						
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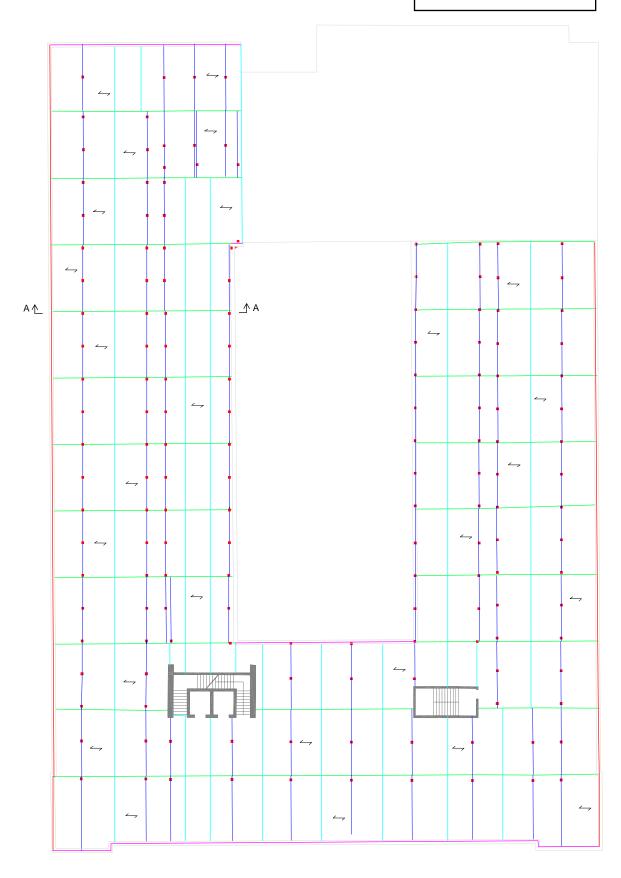
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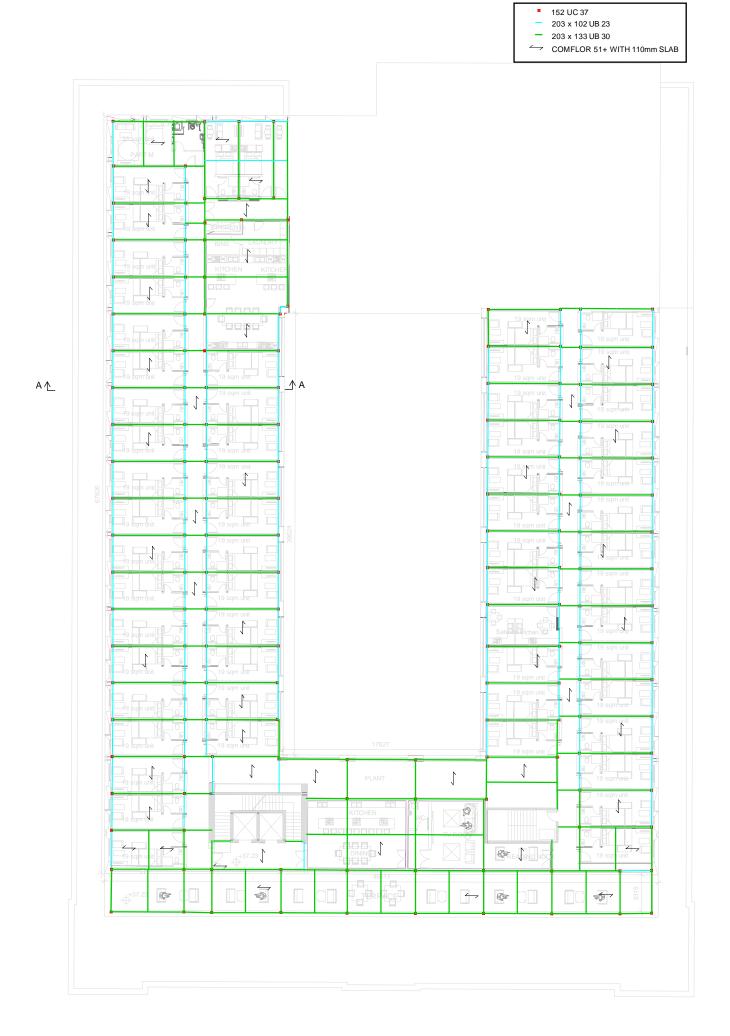
# Appendix C

**Proposed Additional Level Structure** 

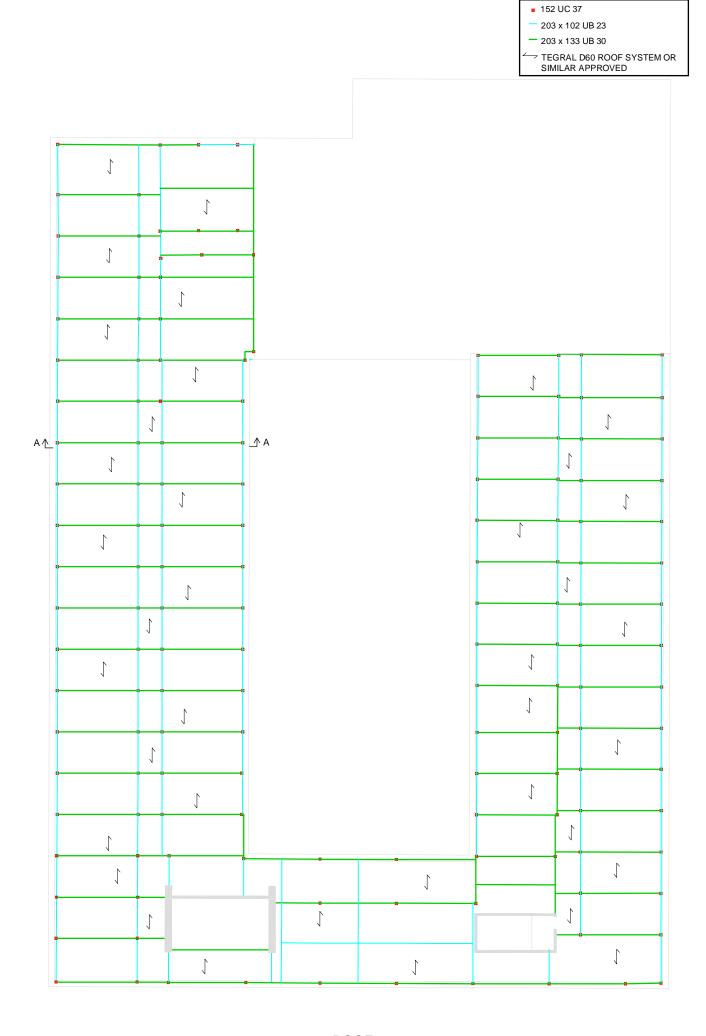
- 1. 2.
- DEMOLISH EXISTING SLAB AND BEAMS
  INSTALL NEW PRIMARY BEAMS ALONG EXISTING COLUMN LINE.
- INSTALL SECONDARY TRANSFER BEAMS TO TRANSFER THE 3.
- LOADS FROM THE COLUMNS ABOVE TO THE PRIMARY BEAMS. INSTALL NEW SECONDARY STEEL AND PERIMETER BEAMS. INSTALL NEW COMFLOR 51+ WITH 110mm SLAB (SIMILAR TO 5. NEW FLOOR ABOVE).
- INSTALL NEW COLUMNS LEVEL 02 LEVEL 03.

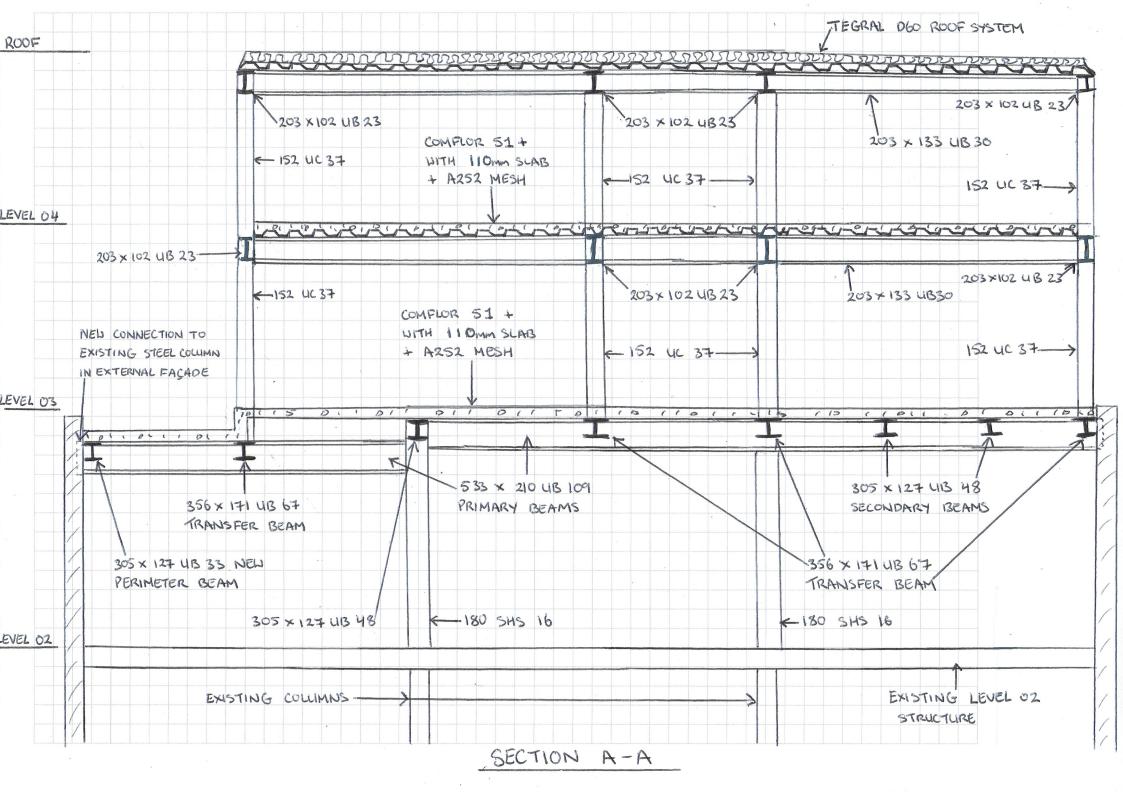
- COLUMNS FROM LEVEL 04 ABOVE
- TRANSFER SECONDARY BEAMS 406 × 178 UB 74
- NEW SECONDARY BEAMS 305 x 127 UB 48
- NEW PRIMARY BEAMS INSTALLED ALDNG EXISTING COLUMN LINE -533 × 210 UB 109
- NEW PRIMARY BEAMS 533  $\times$  165 UB 66
- → COMFLOR 51+ WITH 110mm SLAB
- NEW PERIMETER BEAMS -305 x 127 UB 33





LEVEL 04





# Appendix D

**United Metal Investigation Works** 

### Player Wills

Address:

Generated on - 20/02/2020

Stages - United Metals - Player Wills

Building trades - Investigation Works

Stakeholders - United Metals Recycling (Ireland) Ltd Casey Niall

Drawings - 2019-10-16 (United Metals - Player Wills )

- First floor plan (United Metals - Player Wills )
- Second floor plan (United Metals - Player Wills )
- Third floor plan (United Metals - Player Wills )

- ground floor investigation 1 (United Metals - Player Wills )















• 16/10/2019







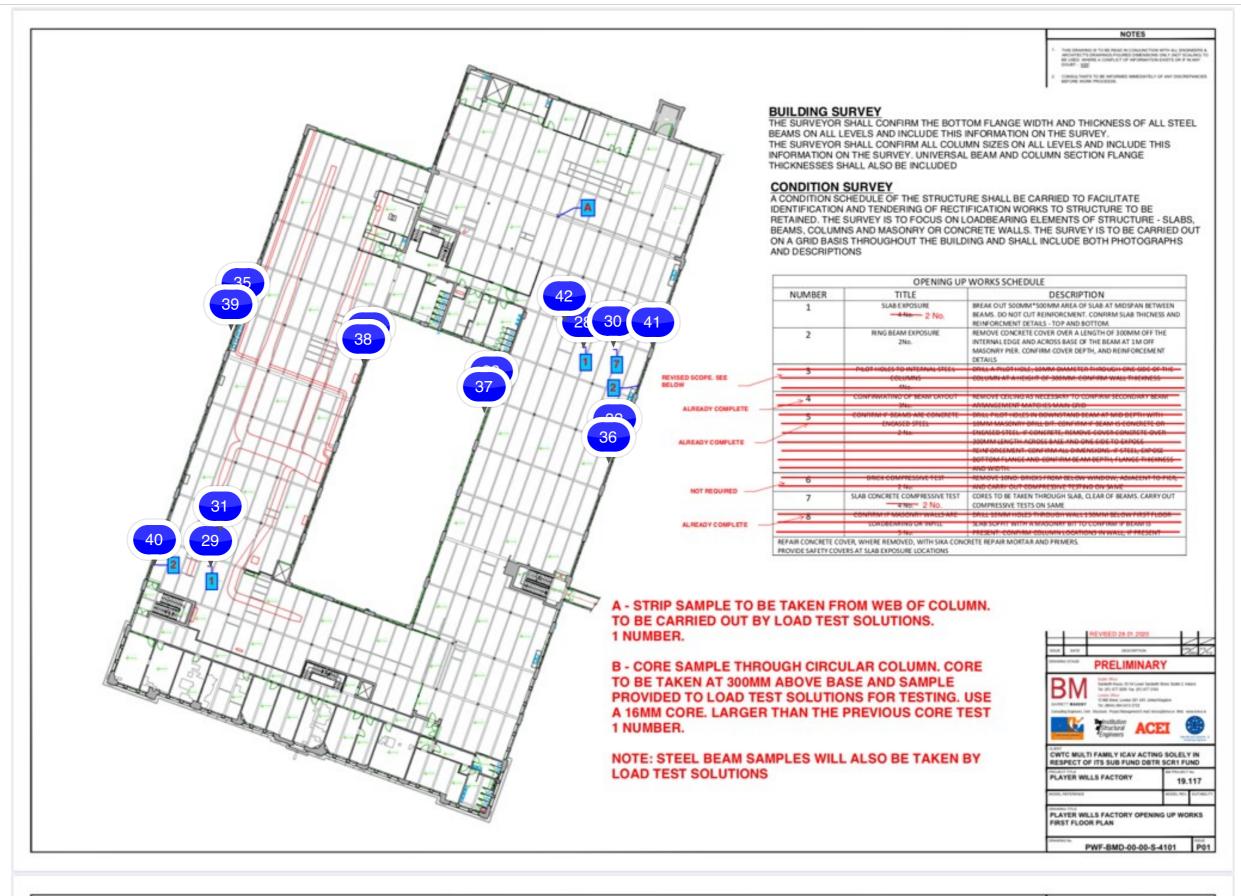
• 16/10/2019















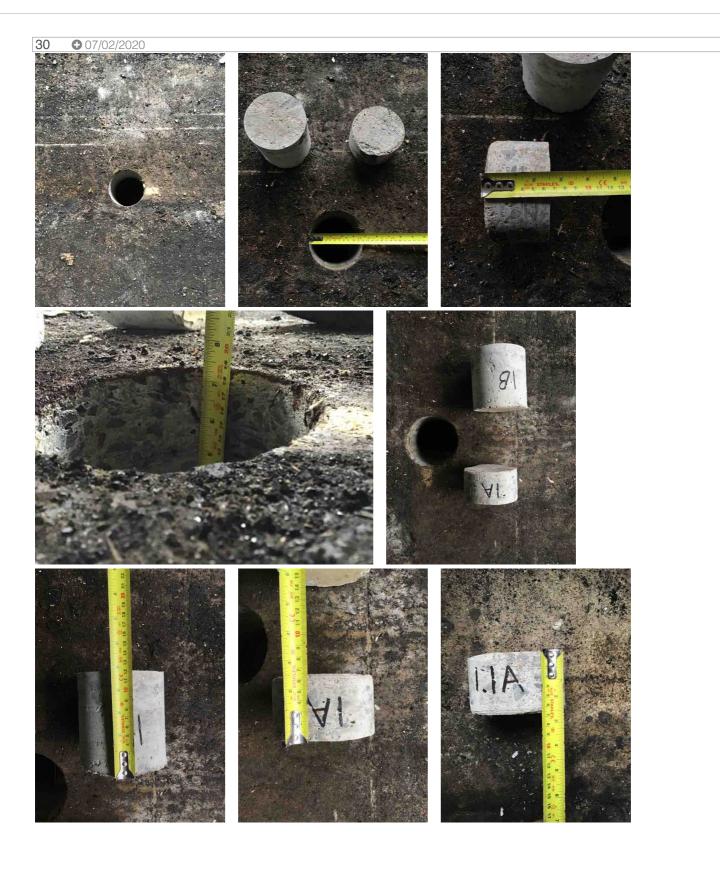




















### • 07/02/2020









#### **⊕** 07/02/2020







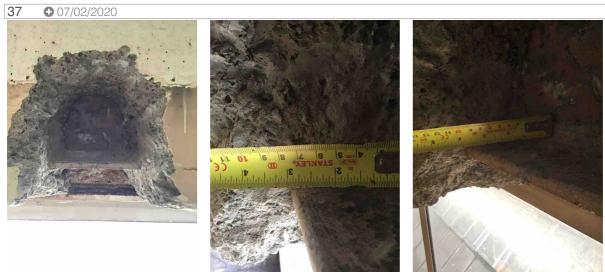


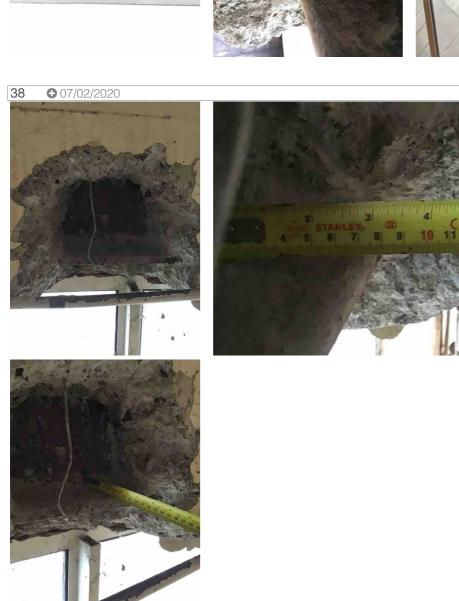
















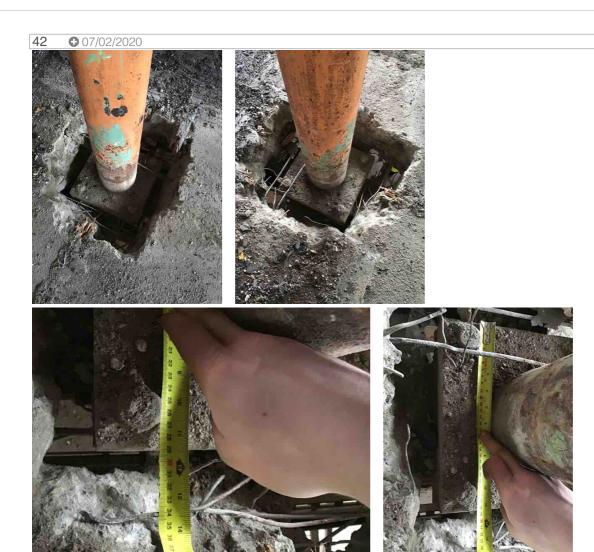


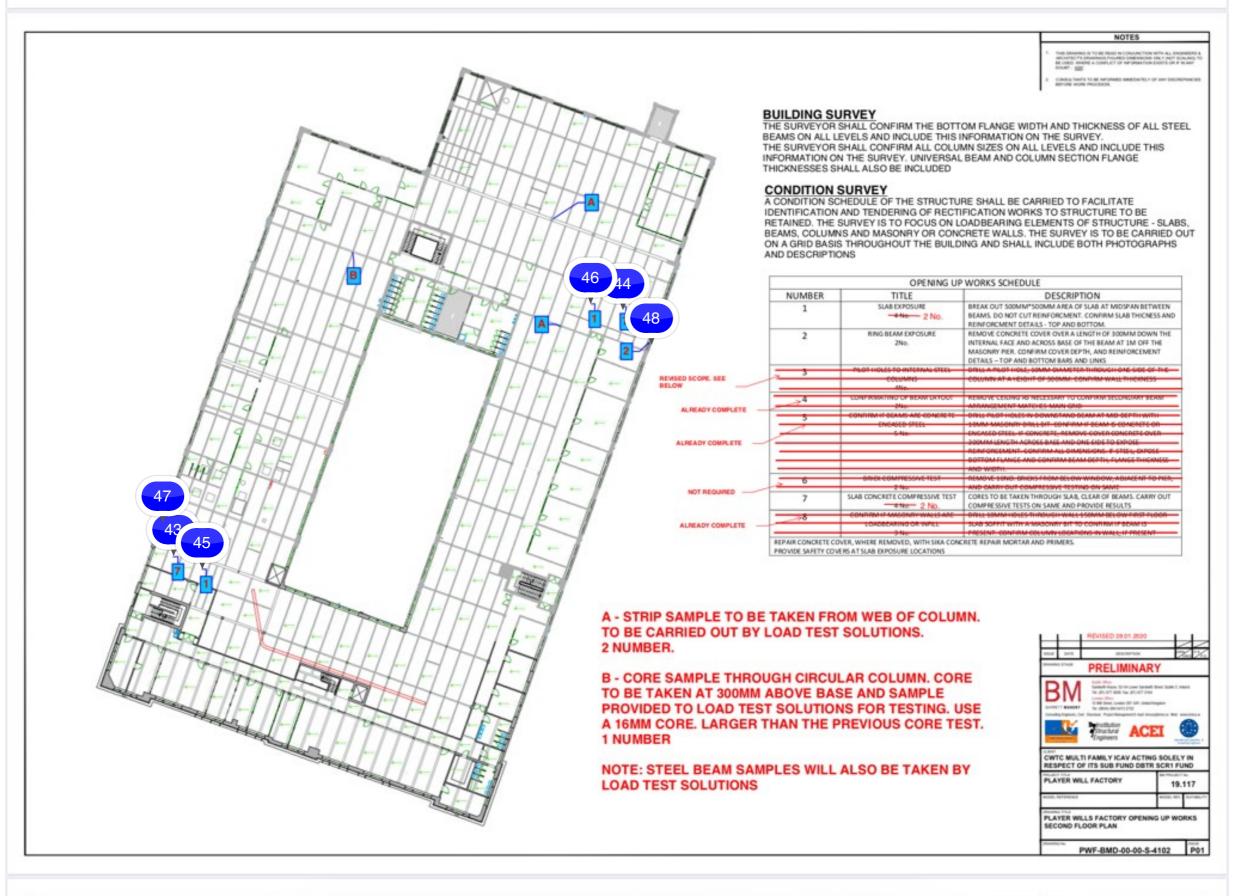
### • 07/02/2020



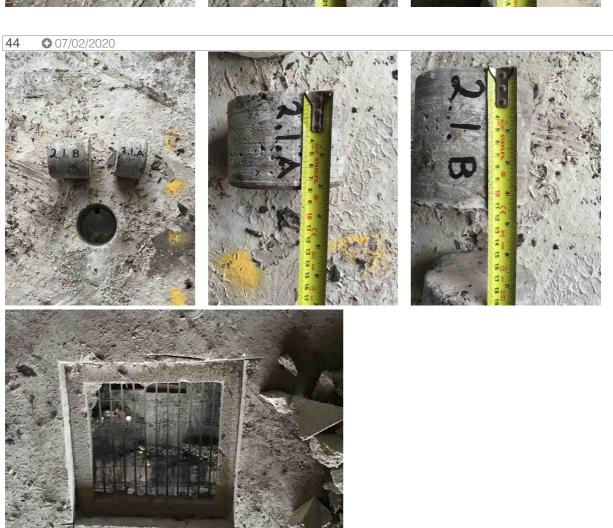




























• 07/02/2020





















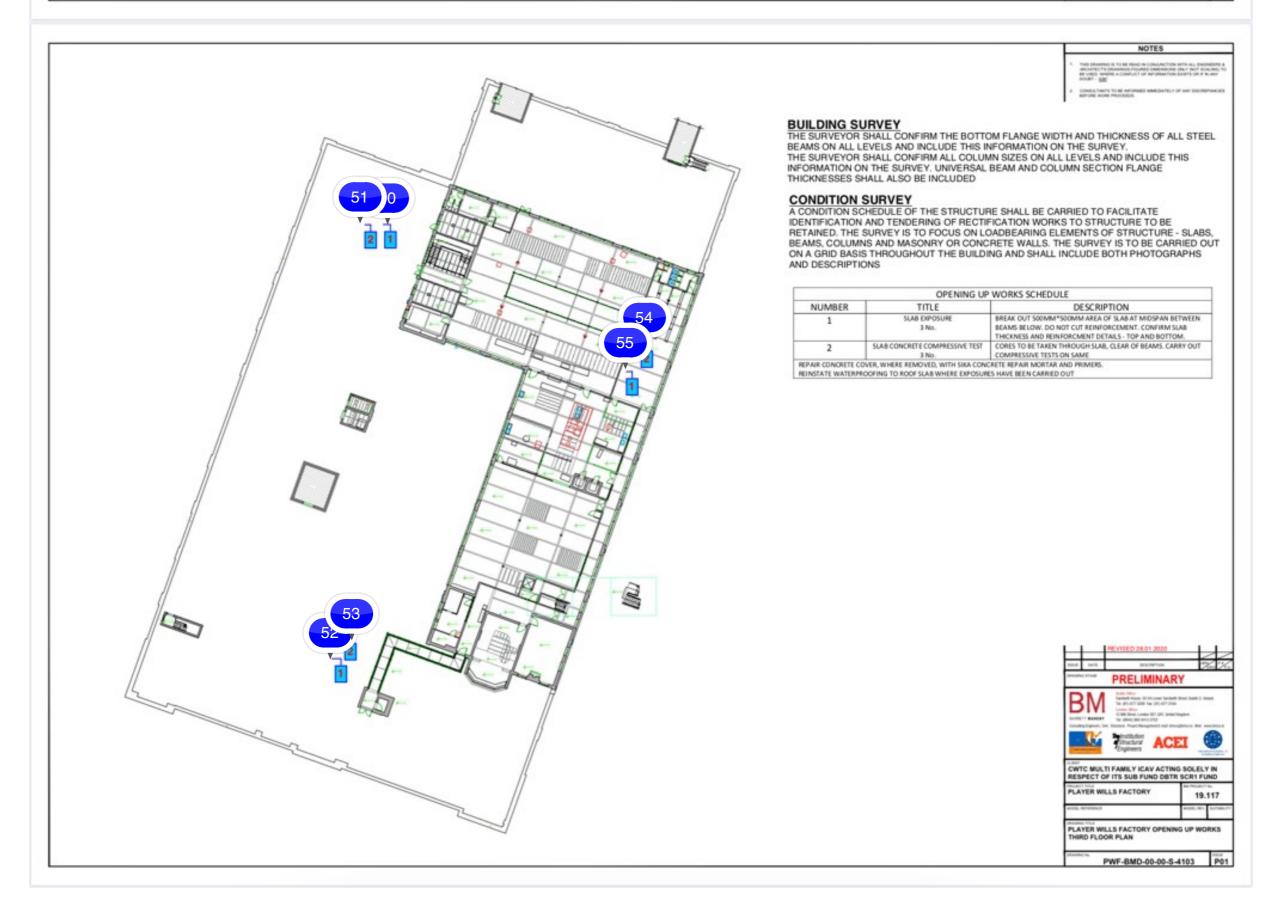


**•** 07/02/2020

48

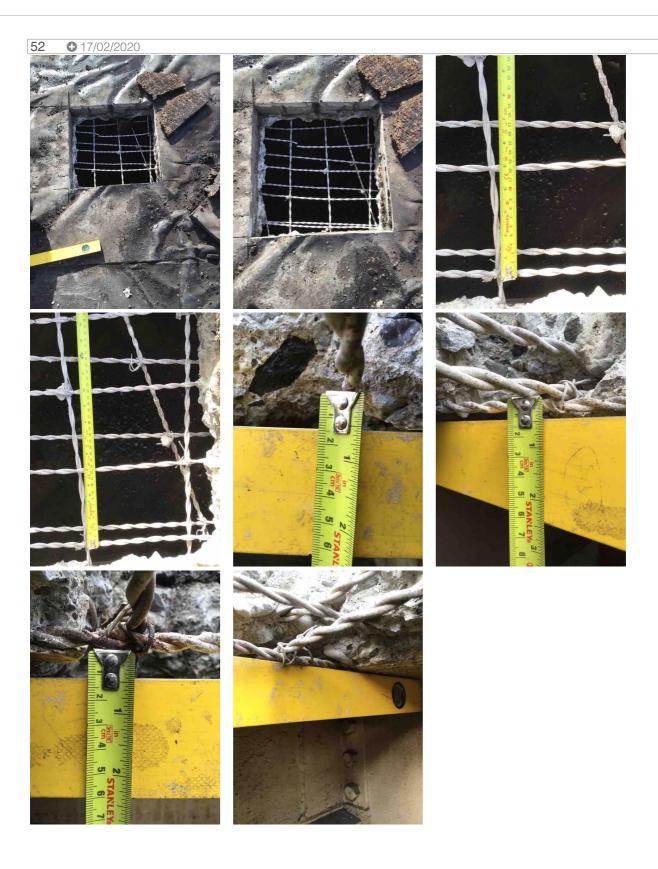


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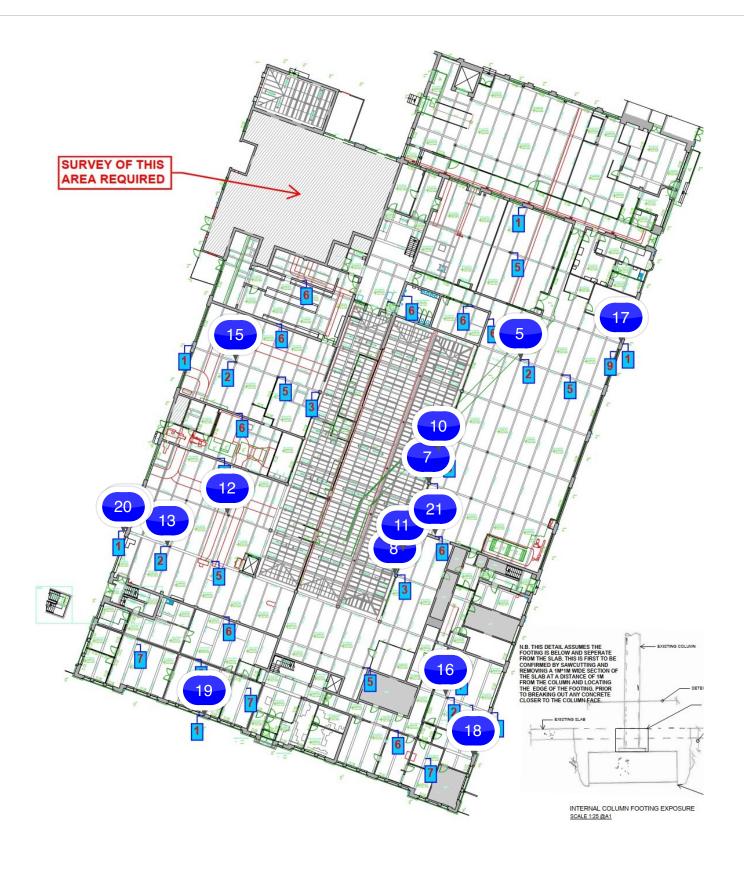


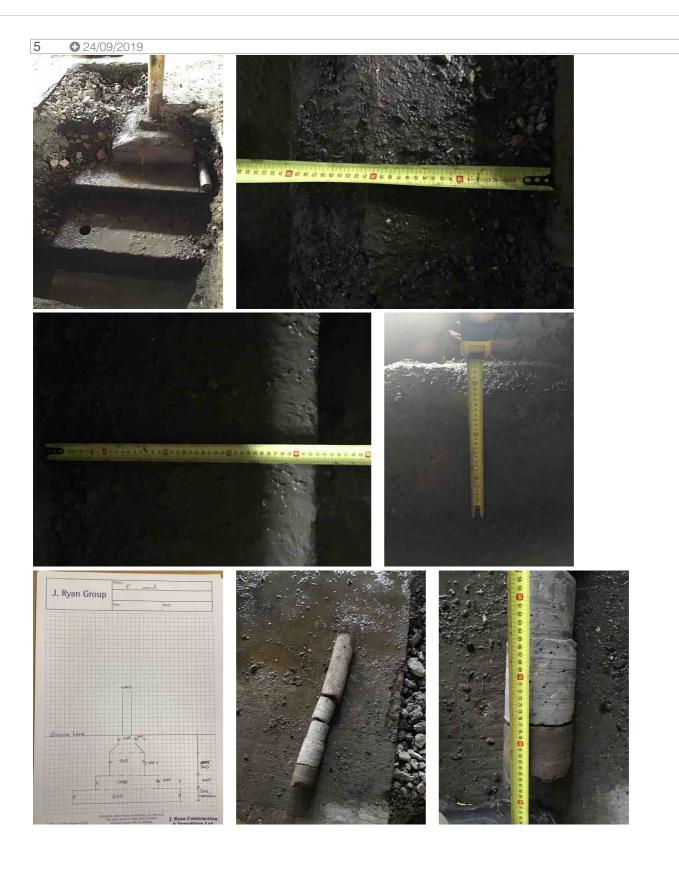














7 • 24/09/2019 Steel Investigation











# 10 • 24/09/2019 Steel Investigation









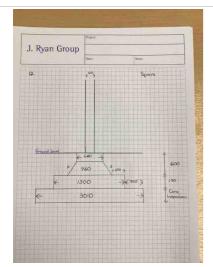






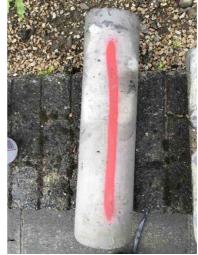


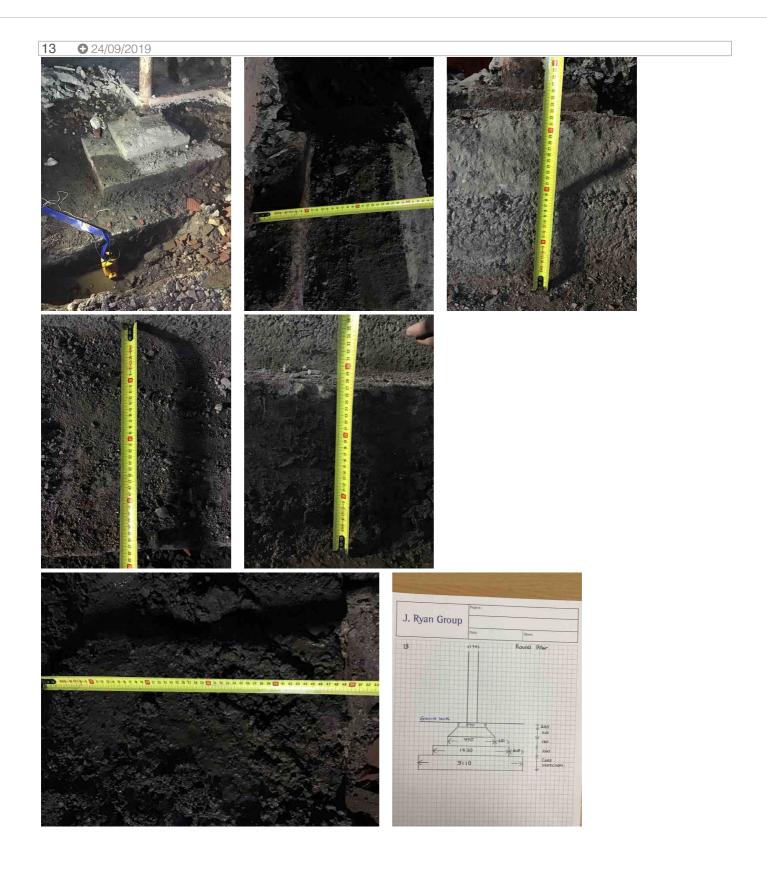


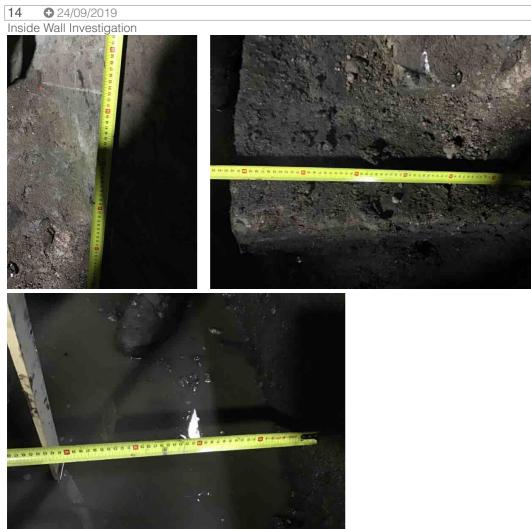


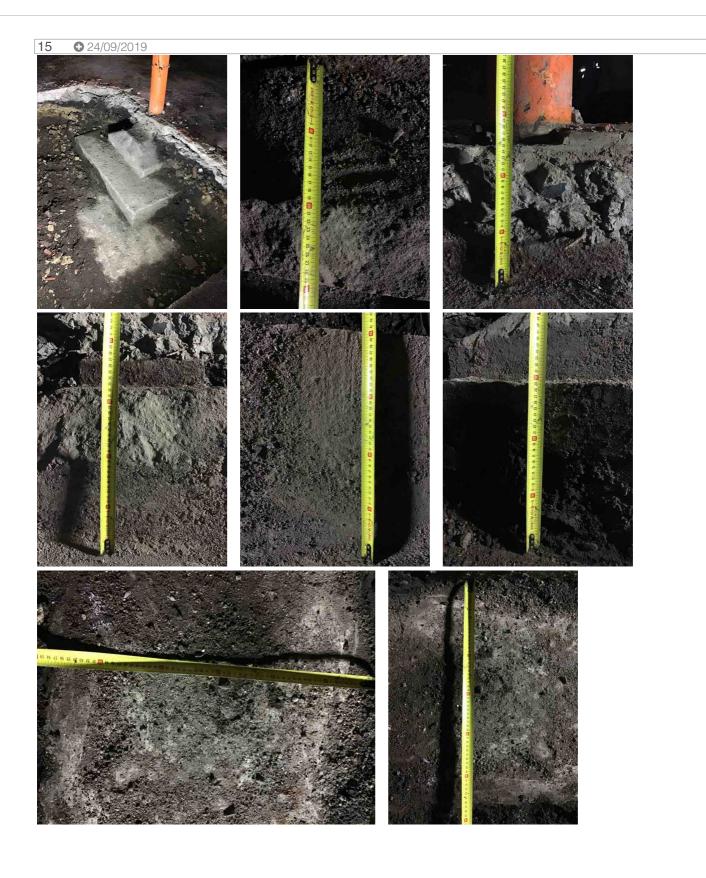


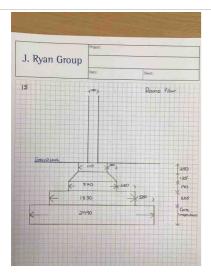






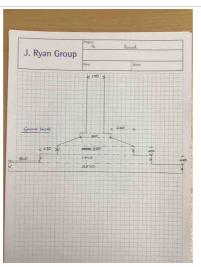












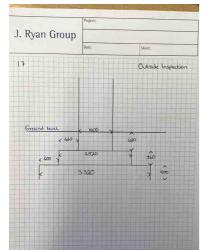
### 17 • 25/09/2019 OutSide Investigation 17



















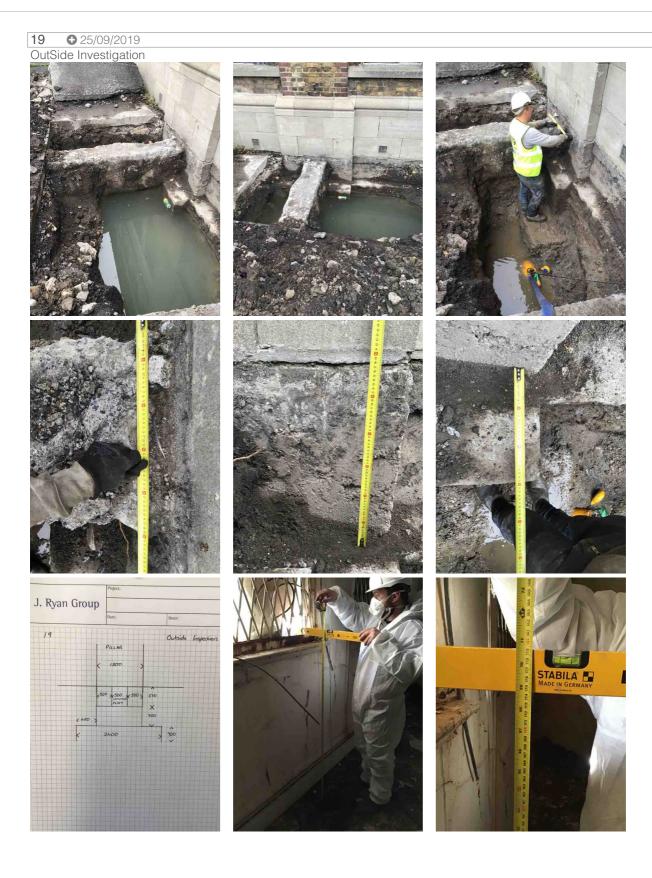






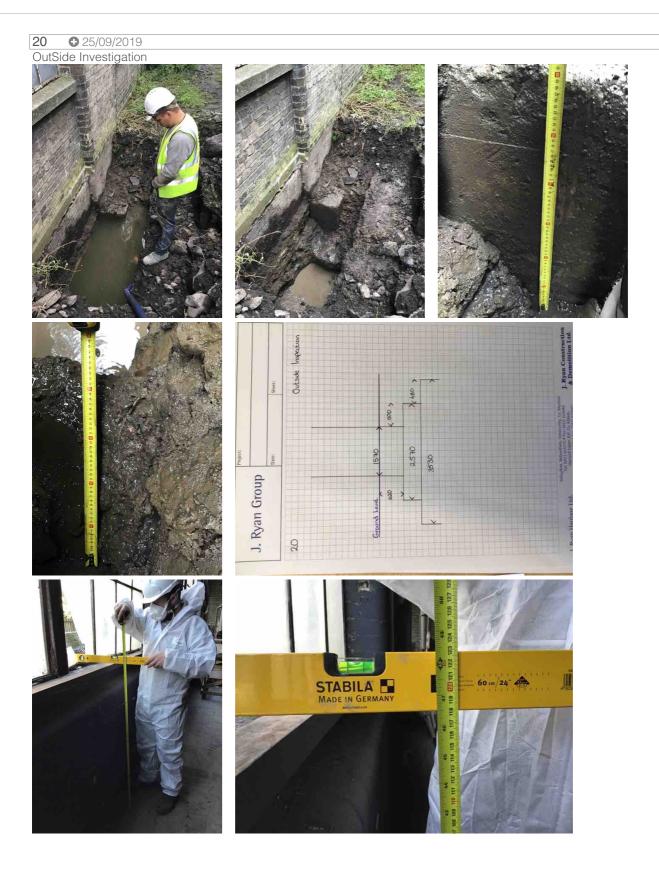
















## • 27/09/2019











### Contact details

United Metals Recycling (Ireland) Ltd Casey Niall Address: Eastway Business Park, Ballysimmon Limerick

0877827946 Phone:

niall.casey@unitedmetals.ie email:

## Appendix E

McFarland Consulting Façade Steelwork Survey



Unit A3, Harbour Court, 5 Heron Road, Belfast BT3 9HB Tel: +44 (0) 28 9073 8100 Email: info@mcfarlandconsulting.co.uk www.mcfarlandconsulting.co.uk

# Player Wills Factory – Column Condition Survey 19575-MCL-XX-RP-J-0001-P01

To:	Ciaran O'Rafferty	From:	Jason Kearney
Re:	Player Wills Factory, Column Condition Survey	Date:	22/06/2020

#### 1.0 INTRODUCTION

On the 10th March 2020, McFarland Consulting Limited (MCL) were instructed by Arran Timms, of Virtus, to commence investigative works concerning the remediation of cracked brickwork piers at the Player Wills Factory, Dublin. This report relates to the first phase of investigative works; a condition survey of affected columns and lintels by means of visual inspection. The survey was undertaken between the 27th and 28th May 2020 by 2no. MCL Corrosion Engineers.

#### 2.0 SCOPE OF WORKS

The scope of works included undertaking a visual inspection of encased columns and lintels within the existing factory building and subsequently assigning a condition rating to each. The condition rating considers:

- Whether the columns/lintels are presently exhibiting cracking, spalling or delamination;
- Whether the columns/lintels are visibly saturated or stained; and
- The proximity of rainwater goods to the encased elements (as a likely source of water ingress to date).

Only those columns and lintels to be retained as part of the refurbishment works were surveyed. The findings of this condition survey will inform the selection of localised investigations, including non-destructive testing and cathodic protection trials, that are to be undertaken in subsequent phases of works.

#### 3.0 CAVEATS AND EXCLUSIONS

Any information made available to us in the course of the investigation whether verbal or in the form of drawings, documents, reports etc. has been assumed to be bona fide and of reliable content.

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 QF 14 Issue 1

 19575-MCL-XX-RP-J-0001-P01
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#### 4.0 DESCRIPTION OF THE STRUCTURE

This derelict factory building, constructed in 1923, is a masonry clad steel frame structure that is to be refurbished for residential use. The steel frame is exposed within the building interior, however, across the exterior elevations the steel columns have been encased within brick piers. The columns located along the perimeter of the central atrium are also encased; the ground floor columns are encased in concrete whilst the columns on the upper floors are encased in brick. It is evident from opening up works undertaken by others that no cavity space exists between the steel columns and the surrounding brick encasement at the majority of locations. There was evidence of a small cavity space having been incorporated within 1no. second floor encased column located adjacent to the internal atrium space.

Additionally, a combination of steel sections encased in concrete and reinforced concrete has been used in the construction of window lintels throughout the building. The encased steel lintels are present over ground, first and second floor windows. Reinforced concrete lintels are present over a selection of second floor windows.

#### 5.0 FINDINGS AND OBSERVATIONS

The visual inspection of the encased columns and lintels was undertaken from ground level around the exterior of the building and from the respective floor levels within the building interior such that the exposed faces of each element could be inspected. The exterior faces of the atrium columns (those facing into the atrium void space) were visually inspected from the surrounding roof level.

The exterior and interior faces of each element were inspected and subsequently assigned a condition rating and corresponding colour indicator, in accordance with the convention outlined in Figure 1 below. Where the assigned condition rating for the interior and exterior faces of the same element differed, the more severe condition is considered to apply to the element overall.

An observation register for each element can be found in Appendix A. Plan drawings indicating the assigned condition rating for each element on a floor by floor basis can be found in Appendix B.

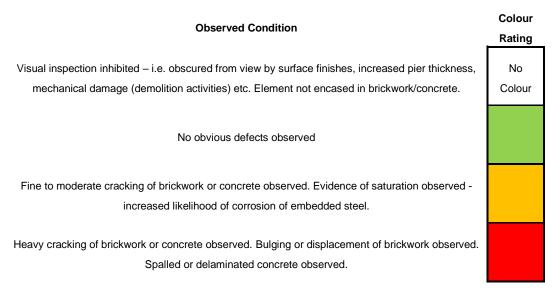


Figure 1: RAG Condition Rating

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A summary of observations is outlined below:

Numerous instances of cracking were observed on the brickwork encasement at column locations. The severity of cracking ranged from hairline cracking to heavy cracking. The orientation of the observed cracking tended to be vertical, following the alignment of the embedded steel column (Plates 1 to 3). In the most severe of cases, 2no. parallel vertical cracks, coinciding with alignment of the column flanges, were present over the full height (storey height) of the affected columns (Plates 4 to 6).







Plate 3



Plate 5



Plate 2

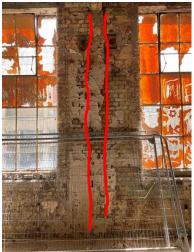


Plate 4



Plate 6



Bulging and displacement of the brickwork encasement was identified at 1no. location (Plate 7).

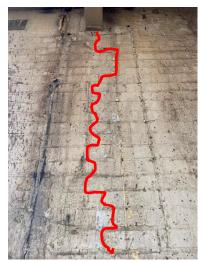


Plate 7

 Evidence of saturation was identified at a number of encased column and lintel locations (Plates 8 and 9). Saturation was particularly prevalent across the south elevation internally (Plates 10 and 11). Whilst the areas where saturation was evident often also exhibited cracking, there were instances where saturation was not accompanied by observable defects. Nonetheless, there is an increased likelihood of corrosion occurring at these locations given the availability of moisture to support the corrosion process.







Plate 9







Plate 10 Plate 11

• Numerous instances of cracking were observed on concrete encased lintels. The cracking was predominantly vertical in orientation, likely coinciding with the position of supplementary stirrups (Plates 12 and 13) – this type of bar reinforcement was observed surrounding the steel lintel sections at locations where opening up works had been undertaken (by others). At a limited number of locations, horizontal cracking was also observed, likely coinciding with the bottom flange of the encased lintel (Plates 14 to 16). Localised cracking of the concrete encasement was also observed at the point of connection between encased lintels and secondary beams (Plate 17).



Plate 12





Plate 13



Plate 15









Plate 17

Numerous instances of cracking were also observed on reinforced concrete lintels, likely
coinciding with the position of shear links (Plate 18). At a selection of reinforced concrete
lintels, spalled concrete and exposed corroded reinforcement was identified (Plate 19).
Reinforced concrete lintels are believed only to be present over a selection of second floor
window locations.



Plate 18

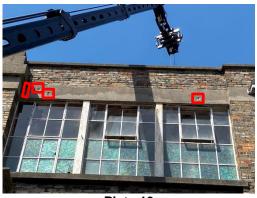


Plate 19

• Within the interior of the building, surface finishes (paint coatings, tiling, plasterwork, panelling etc.) may have inhibited the identification of defects (plate 20). Additionally, along the southern building elevation (gridline N) the existence of inbuilt chimney flues, thickened brick piers and exterior stone cladding may have concealed defects (Plates 21 to 23).



Plate 20



Plate 21







Plate 22 Plate 23

Localised areas of brick/concrete encasement have been removed (by others) to expose the
embedded steel sections or steel reinforcement. The condition of the steel present at these
locations varied, from exhibiting little or no corrosion (Plates 24 and 25) to exhibiting moderate
surface corrosion (Plates 26 and 27). From the limited number of elements exposed, it
appears that the embedded columns located along the eastern elevation are worst affected.







Plate 26



Plate 25



Plate 27



## 6.0 CONCLUSIONS

Cracking of the encasement surrounding columns and lintels was observed at numerous locations throughout the building, both on external and internal faces. The survey also indicates a significant concentration of defects to the eastern aspect of the building on the first floor. In addition to the observed cracking, spalled and delaminated concrete was also identified on a selection of reinforced concrete lintels located on the second floor.

The nature of the observed cracking, in conjunction with the condition of the embedded steel exposed in localised areas, would suggest that steel corrosion is a likely cause of the observed defects. The lack of cavity space provided between the embedded steel columns and the surrounding brick encasement is likely contributing to the cracking observed at these locations. In the absence of a cavity space, the build-up of expansive corrosion products on the surface of the steel columns imposes increased stress directly onto the surrounding brickwork, subsequently causing it to crack. However, cracking arising from structural deficiencies or structural movement cannot be ruled out; these considerations should be checked by a suitably qualified structural engineer.

Nonetheless, it is recommended that further investigations are undertaken to determine whether the embedded steel is likely to be actively corroding, and the extent over which this may be occurring. It is also recommended that investigations are undertaken to determine the presence of deleterious contaminants or the action of deterioration processes which may be contributing to the corrosion of the embedded steel.



**Appendix A – Observation Register** 



Element Ref:	Туре	Level	Face	Notes	Face-by- Face RAG Rating	Combined RAG Rating							
42	Calina		Interior	Not Encased									
А3	Column	0	Exterior	Heavy Vertical Cracking - (2no Parallel)									
42	Caluman	0	Interior	Heavy Vertical Cracking - (1no )									
A2	Column	0	Exterior	Heavy Vertical Cracking - (2no Parallel)									
A1	Column	0	Interior	Moderate Vertical Cracking - ( )									
AI	Column	0	Exterior	Visually Sound									
D1	Caliman	0	Interior	Moderate Vertical Cracking - ( )									
B1	Column	0	Exterior	Visually Sound									
C1	Column	-	Interior	Visually Sound									
CI	Column	0	Exterior	Visually Sound									
D1	Caluman	0	Interior	Isolated Fine Vertical Cracking - (1no )									
D1	1 Column	0	Exterior	Visually Sound									
E1	Column	0	Interior	Encasement Partially Removed									
£1	Column		Exterior	Visually Sound									
F1	Caluman	0	Interior	Isolated Moderate Vertical Cracking - ( )									
F1	Column	0	Exterior	Visually Sound									
G1	Column	0	Interior	Encasement Partially Removed									
GI		Column	Column	Column	Column	Column	Column	Column	Column	0	Exterior	Heavy Vertical Cracking - ( )	
H1	Column	0	Interior	Visually Sound									
п	Column	0	Exterior	Visually Sound									
J1	Column	0	Interior	Visually Sound									
JI	Column	0	Exterior	Visually Sound									
K1	Column	0	Interior	Obscured from View									
KI	Column	0	Exterior	Isolated Heavy Vertical Cracking - (1no )									
L1	Column	0	Interior	Visually Sound									
	Column 0		Exterior	Visually Sound									
M1	Column 0	0	Interior	Visually Sound									
INIT		<u> </u>	Exterior	Visually Sound									
N1	Column		Interior	Obscured from View									
INT	Coluillii		Exterior	Visually Sound									



Element Ref:	Туре	Level	Face	Notes	Face-by- Face RAG Rating	Combined RAG Rating
			Interior	Visually Sound		
N2	Column	0	Exterior	Heavy Vertical Cracking - ( )		
			Interior	Cracked Render and Saturation		
N3	Column	0	Exterior	Visually Sound		
N/A	Caliman	0	Interior	Heavy Vertical Cracking - ( )		
N4	Column	0	Exterior	Visually Sound		
N5	Column	0	Interior	Heavy Vertical Cracking - ( )		
N5	Column	J	Exterior	Visually Sound		
NE	Column	0	Interior	Isolated Moderate Vertical Cracking - ( )		
N6	Column	0	Exterior	Visually Sound		
N7	Column	0	Interior	Cracked Render		
N7	Column	N7 Column	Exterior	Visually Sound		
N8	Column	0	Interior	Visually Sound		
INO	Column	Ů	Exterior	Visually Sound		
N9	Column	0	Interior	Cracked Render		
N9	Column	Column	Exterior	Visually Sound		
N10	Column	0	Interior	Visually Sound		
NIO	Column	U	Exterior	Heavy Vertical Cracking - ( )		
M10	Column	0	Interior	Isolated Moderate Vertical Cracking - ( )		
IVIIO	Column	O O	Exterior	Visually Sound		
L10	Column	0	Interior	Heavy Vertical Cracking - ( )		
LIO	Column	o o	Exterior	Isolated Heavy Vertical Cracking - (2no Parallel)		
K10	Column	0	Interior	Encasement Partially Removed		
KIO	Column	0	Exterior	Visually Sound		
J10	Column	0	Interior	Visually Sound		
310	Column	Ŭ	Exterior	Visually Sound		
H10	Column	0	Interior	Visually Sound		
1120	551611111	Ĭ	Exterior	Visually Sound		
G10	Column	0	Interior	Heavy Vertical Cracking - (2no Parallel)		
010	Coluilli		Exterior	Visually Sound		



Element Ref:	Туре	Level	Face	Notes	Face-by- Face RAG Rating	Combined RAG Rating
-10			Interior	Isolated Moderate Vertical Cracking - ( )		
F10	Column	0	Exterior	Visually Sound		
540			Interior	Moderate Vertical Cracking - ( )		
E10	Column	0	Exterior	Visually Sound		
D10	Caluman	0	Interior	Moderate Vertical Cracking - (2no Parallel)		
D10	Column	0	Exterior	Visually Sound		
D4	Column	nn O	Interior	Mechanical Damage		
D4	Column		Exterior	n/a		
E4	Column	0	Interior	Visually Sound		
E4	Column	0	Exterior	n/a		
F4	Column	0	Interior	Visually Sound		
F4	r4 Column	olullii 0	Exterior	n/a		
G4		umn 0	Interior	Moderate Vertical Cracking - ( )		
04	Column	O	Exterior	n/a		
H4	Column	0	Interior	Visually Sound		
114	Column	o l	Exterior	n/a		
J4	Column	0	Interior	Visually Sound		
J4	Column		Exterior	n/a		
K4	Column	0	Interior	Visually Sound		
K4	Column	J	Exterior	n/a		
K5	Column	0	Interior	Visually Sound		
K5	Column		Exterior	n/a		
К6	Column	0	Interior	Moderate Horizontal Cracking - ( )		
	001411111		Exterior	n/a		
K7	Column	0	Interior	Visually Sound		
	Column		Exterior	n/a		
J7	Column	0	Interior	Visually Sound		
		Column 0	Exterior	n/a		
Н7	Column	0	Interior	Visually Sound		
117	Column		Exterior	n/a		



Element Ref:	Туре	Level	Face	Notes	Face-by- Face RAG Rating	Combined RAG Rating
<b>G</b> 7	Column	0	Interior	Visually Sound		
d7	Column		Exterior	n/a		
F7 Column	0	Interior	Mechanical Damage			
Г	Column	0	Exterior	n/a		
E7	Column	Column 0	Interior	Fine Horizontal Cracking - ( )		
L7	Column		Exterior	n/a		
D7 Colum	Caliman	0	Interior	Visually Sound		
	Column	0	Exterior	n/a		



Element Ref:	Туре	Level	Face	Notes	Face-by- Face RAG Rating	Combined RAG Rating
4.2			Interior	Visually Sound		
A3	Column	1	Exterior	Visually Sound		
4.2		_	Interior	Isolated Moderate Vertical Cracking - ( )		
A2	Column	1	Exterior	Visually Sound		
A.1	Caluman	1	Interior	Visually Sound		
A1	Column	1	Exterior	Visually Sound		
D4	Caliman	4	Interior	Isolated Heavy Vertical Cracking - ( )		
B1	Column	1	Exterior	Visually Sound		
C1	Caluman	1	Interior	Heavy Vertical Cracking - (2no Parallel)		
C1	Column	1	Exterior	Visually Sound		
D1	Caluman	1	Interior	Isolated Moderate Vertical Cracking - ( )		
DI	D1 Column	1	Exterior	Visually Sound		
E1	Column	1	Interior	Visually Sound		
E1	E1 Column	1	Exterior	Visually Sound		
F1	Column	1	Interior	Heavy Vertical Cracking - ( )		
FI	Column	1	Exterior	Isolated Fine Vertical Cracking - (1no )		
G1	Column	1	Interior	Isolated Moderate Vertical Cracking - (2no Parallel)		
GI	Column	1	Exterior	Visually Sound		
H1	Column	1	Interior	Visually Sound		
п	Column	1	Exterior	Visually Sound		
J1	Column	1	Interior	Heavy Vertical Cracking - ( )		
J1	Column	1	Exterior	Visually Sound		
K1	Column	1	Interior	Visually Sound		
KI	Column	1	Exterior	Visually Sound		
L1	Column	1	Interior	Heavy Vertical Cracking - (2no. Parallel)		
	Column	1	Exterior	Visually Sound		
M1	Column	1	Interior	Visually Sound		
IAIT	Column	1	Exterior	Visually Sound		
N1	Column	1	Interior	Visually Sound c/w Chimney Thickening		
141	Column		Exterior	Heavy Vertical Cracking - ( )		



Element Ref:	Туре	Level	Face	Notes	Face-by- Face RAG Rating	Combined RAG Rating		
NO	Colon	4	Interior	Visually Sound c/w Chimney Thickening				
N2	Column	1	Exterior	Isolated Heavy Vertical Cracking - ( )				
N2	Caliman	4	Interior	Visually Sound c/w Thickened Pier				
N3	Column	1	Exterior	Visually Sound				
N/4	Caluman	1	Interior	Visually Sound c/w Chimney Thickening				
N4	Column	1	Exterior	Visually Sound				
N5	Column	1	Interior	Visually Sound c/w Thickened Pier				
IN5	Column	1	Exterior	Visually Sound				
NC	Column	1	Interior	Visually Sound c/w Chimney Thickening				
N6	Column	1	Exterior	Isolated Moderate Vertical Cracking - ( )				
N7	Column		Interior	Visually Sound				
N7	Column	Column	Column	1	Exterior	Visually Sound		
NO	Caluman	1	Interior	Visually Sound				
N8	Column	1	Exterior	Visually Sound				
N9	Column	1	Interior	Visually Sound c/w Thickened Pier				
N9	Column		Exterior	Visually Sound				
N10	Column	1	Interior	Visually Sound				
NIO	Column	1	Exterior	Heavy Vertical Cracking - ( )				
M10	Column	1	Interior	Heavy Vertical Cracking - ( )				
IVIIO	Column	1	Exterior	Isolated Heavy Vertical Cracking - ( )				
L10	Column	1	Interior	Heavy Vertical Cracking - (2no Parallel)				
LIO	Column	1	Exterior	Heavy Vertical Cracking - ( )				
K10	Column	1	Interior	Heavy Vertical Cracking - (2no Parallel)				
KIU	Coluillii		Exterior	Isolated Heavy Vertical Cracking - (2no )				
J10	Column	1	Interior	Heavy Vertical Cracking - (2no Parallel)				
710	Column	1	Exterior	Isolated Moderate Vertical Cracking - (1no )				
H10	Column	1	Interior	Visually Sound c/w Thickened Pier				
1110	Column	1 -	Exterior	Heavy Vertical Cracking - ( )				
G10	Column	1	Interior	Heavy Vertical Cracking - (2no Parallel)				
G10	Column		Exterior	Heavy Vertical Cracking - ( )				



Element Ref:	Туре	Level	Face	Notes	Face-by- Face RAG Rating	Combined RAG Rating			
F10	Column	1	Interior	Heavy Vertical Cracking - (2no Parallel)					
F10	Column	1	Exterior	Heavy Vertical Cracking - ( )					
F10	Caluman	1	Interior	Heavy Vertical Cracking - ( )					
E10	Column	1	Exterior	Heavy Vertical Cracking - ( )					
D10	Column	1	Interior	Heavy Vertical Cracking - (2no Parallel)					
D10	Column	1	Exterior	Heavy Vertical Cracking - ( )					
D4	Column	1	Interior	Moderate Vertical Cracking - ( )					
D4	Column		Exterior	Visually Sound					
F.4	Caluman	1	Interior	Isolated Moderate Vertical Cracking - ( )					
E4	Column 1	Exterior	Visually Sound						
F4	Caluman	1	Interior	Isolated Moderate Vertical Cracking - ( )					
F4	Column	Column	Column	Column	1	Exterior	Visually Sound		
C4	Caluman	n 1	Interior	Heavy Vertical Cracking - (2no Parallel)					
G4	Column	1	Exterior	Visually Sound & Saturated					
H4	Column	1	Interior	Isolated Moderate Vertical Cracking - ( )					
П4	Column	1	Exterior	Visually Sound					
J4	Column	n 1	Interior	Isolated Heavy Vertical Cracking - (2no Parallel)					
J4	Column	1	Exterior	Visually Sound					
K4	Column	Column 1	Interior	Visually Sound					
K4	Column	1	Exterior	Visually Sound		]			
K5	Column	1	Interior	Moderate Vertical Cracking - ( )					
KS	Column	1	Exterior	Visually Sound					
K6	Column	1	Interior	Visually Sound					
KU	Column	1	Exterior	Visually Sound		]			
K7	Column	1	Interior	Visually Sound					
N/	Column		Exterior	Visually Sound					
J7	Column	1	Interior	Heavy Vertical Cracking - ( )					
J/	Column		Exterior	Heavy Vertical Cracking - ( )					
U7	Column	1	Interior	Isolated Heavy Vertical Cracking - (1no )					
H7	Column	1	Exterior	Heavy Vertical Cracking - ( )					



Element Ref:	Туре	Level	Face	Notes	Face-by- Face RAG Rating	Combined RAG Rating	
<b>G</b> 7	Column	1	Interior	Heavy Vertical Cracking - (2no Parallel)			
G/ Column	1	Exterior	Saturation Evident				
F7 Column	Column	1	Interior	Heavy Vertical Cracking - (2no Parallel)			
Г	Column	Column	1	Exterior	Heavy Vertical Cracking - ( )		
E7	Column	1	Interior	Heavy Vertical Cracking - (2no Parallel)			
L7	Column		Exterior	Isolated Heavy Vertical Cracking - ( )			
D7	Column	1	Interior	Heavy Vertical Cracking - (2no Parallel)			
		.Olulliii I I	Exterior	Visually Sound			



Element Ref:	Туре	Level	Face	Notes	Face-by- Face RAG Rating	Combined RAG Rating
4.2	6.1		Interior	Visually Sound		
A3	Column	2	Exterior	Visually Sound		
4.2	6.1	2	Interior	Visually Sound		
A2	Column	2	Exterior	Visually Sound		
A 1	Calumn	2	Interior	Visually Sound		
A1	Column	2	Exterior	Visually Sound		
D4	Calvara	2	Interior	Isolated Moderate Vertical Cracking - ( )		
B1	Column	2	Exterior	Visually Sound		
C1	Calumn	2	Interior	Visually Sound		
C1	Column	2	Exterior	Visually Sound		
D1	Calvara	2	Interior	Isolated Moderate Vertical Cracking - ( )		
D1	1 Column		Exterior	Isolated Heavy Vertical Cracking - (2no )		
F1	Calumn	mn 2	Interior	Visually Sound		
E1	Column		Exterior	Visually Sound		
F1	Column	2	Interior	Visually Sound		
FI	Column	Column 2	Exterior	Visually Sound		
G1	Column	olumn 2	Interior	Isolated Fine Vertical Cracking - ( )		
GI	Column	2	Exterior	Visually Sound		
H1	Column	2	Interior	Visually Sound		
п	Column	2	Exterior	Visually Sound		
J1	Column	2	Interior	Visually Sound		
31	Column	2	Exterior	Visually Sound		
K1	Column	2	Interior	Isolated Fine Vertical Cracking - ( )		
KI	Column	2	Exterior	Visually Sound		
L1	Column	2	Interior	Visually Sound		
	Column		Exterior	Visually Sound		
M1	Column 2	2	Interior	Visually Sound c/w Thickened Pier		
IVII		Column 2	Exterior	Visually Sound		
N1	Column	2	Interior	Visually Sound c/w Chimney Thickening		
INT	Coluilli		Exterior	Visually Sound		



Element Ref:	Туре	Level	Face	Notes	Face-by- Face RAG Rating	Combined RAG Rating		
NO	0.51	2	Interior	Isolated Moderate Vertical Cracking - ( )				
N2	Column	2	Exterior	Visually Sound				
N2	Caliman	2	Interior	Visually Sound				
N3	Column	2	Exterior	Visually Sound				
N4	Caluman	2	Interior	Visually Sound c/w Thickened Pier				
N4	Column	2	Exterior	Visually Sound				
N5	Column	2	Interior	Visually Sound + Saturation				
IN5	Column	2	Exterior	Visually Sound				
NC	Caluman	2	Interior	Visually Sound c/w Thickened Pier				
N6	Column	2	Exterior	Visually Sound				
N7	Column	2	Interior	Visually Sound				
N7	Colulliii Z	Column	Column	2	Exterior	Visually Sound		
NO	Calvana	2	Interior	Visually Sound				
N8	Column	2	Exterior	Visually Sound				
N9	Column	2	Interior	Visually Sound				
N9	Column		Exterior	Visually Sound				
N10	Column	Column 2	Interior	Obscured from view				
NIO	Column	2	Exterior	Visually Sound				
M10	Column	2	Interior	Visually Sound + Saturation				
IVIIO	Column	2	Exterior	Visually Sound				
L10	Column	2	Interior	Visually Sound + Saturation				
LIO	Column	2	Exterior	Visually Sound				
K10	Column	2	Interior	Isolated Heavy Vertical Cracking - ( )				
KIU	Coluillii		Exterior	Visually Sound				
J10	Column	2	Interior	Visually Sound				
310	Column		Exterior	Visually Sound				
H10	Column	2	Interior	Visually Sound c/w Thickened Pier				
1110	Column		Exterior	Visually Sound				
G10	Column	2	Interior	Visually Sound				
G10	Column		Exterior	Visually Sound				



Element Ref:	Туре	Level	Face	Notes	Face-by- Face RAG Rating	Combined RAG Rating
540		2	Interior	Visually Sound		
F10	Column	2	Exterior	Visually Sound		
		_	Interior	Visually Sound		
E10	Column	2	Exterior	Visually Sound		
242			Interior	Visually Sound		
D10	Column	2	Exterior	Visually Sound		
			Interior	Heavy Vertical Cracking - ( )		
D4	Column	2	Exterior	Visually Sound		
			Interior	Visually Sound		
E4	Column	2	Exterior	Visually Sound		
		2	Interior	Visually Sound		
F4	Column	2	Exterior	Visually Sound		
64	G4 Column	2	Interior	Visually Sound		
G4		2	Exterior	Visually Sound + Saturated		
	Caliman	2	Interior	Visually Sound		
H4	Column	Column 2	Exterior	Visually Sound		
14	Caliman	2	Interior	Isolated Fine Vertical Cracking - ( )		
J4	Column	2	Exterior	Visually Sound		1
V.4	Caluman	2	Interior	Visually Sound		
К4	Column	2	Exterior	Visually Sound		
V.F.	Caliman	2	Interior	Visually Sound		
K5	Column	2	Exterior	Visually Sound		
W.C	Column	2	Interior	Visually Sound		
К6	Column	2	Exterior	Visually Sound		1
1/7	Column	2	Interior	Visually Sound		
К7	Column	2	Exterior	Visually Sound		
J7	Column	2	Interior	Visually Sound		
J/	Column		Exterior	Visually Sound		
H7	Column	2	Interior	Visually Sound		
п/	Column		Exterior	Isolated Heavy Vertical Cracking - ( )		



Element Ref:	Туре	Level	Face	Notes	Face-by- Face RAG Rating	Combined RAG Rating
<b>G</b> 7	Column	2	Interior	Visually Sound		
G/	Column	2	Exterior	Heavily Saturated		
F7	F7 Column	2	Interior	Visually Sound		
Г7	Column		Exterior	Visually Sound		
E7	Column	2	Interior	Visually Sound		
L7	Column	2	Exterior	Visually Sound		
D7	Caliman	2	Interior	Heavy Vertical Cracking - (Bulging )		
	Column	Column 2	Exterior	Visually Sound		



Element Ref:	Туре	Level	Face	Notes	Face-by- Face RAG Rating	Combined RAG Rating			
42/4	15		Interior	Fine Vertical Cracking - ( )					
A3/4	Lintel	0	Exterior	Visually Sound					
42/2	1:		Interior	Fine Vertical Cracking - ( )					
A2/3	Lintel	0	Exterior	Visually Sound					
11/2			Interior	Visually Sound					
A1/2	Lintel	0	Exterior	Isolated Heavy Vertical Cracking - (1no )					
A /D4	Lintal	0	Interior	Visually Sound					
A/B1	Lintel	0	Exterior	Isolated Moderate Vertical Cracking - (3no )					
D/C1	Lintel (	Linkol	Linkel	0	Interior	Visually Sound			
B/C1	Lintei	0	Exterior	Isolated Moderate Vertical Cracking - (2no )					
C/D1	Lintel 0	Lintol	Lintal	Lintal	0	Interior	Visually Sound		
C/D1		0	Exterior	Isolated Moderate Vertical Cracking - (1no )					
D/E1	Lintel	0	Interior	Fine Vertical Cracking - ( )					
D/EI	Linter		Exterior	Isolated Heavy Vertical Cracking - (4no )					
E /E1	Lintel	0	Interior	Visually Sound					
E/F1	Lintei		Exterior	Isolated Heavy Vertical Cracking - (1no )					
F/G1	Lintel	0	Interior	Visually Sound					
F/G1	Linter		Exterior	Isolated Heavy Vertical Cracking - (3no )					
G/H1	Lintel	0	Interior	Fine Vertical Cracking - (2no )					
G/H1	Linter		Exterior	Isolated Heavy Vertical Cracking - (2no )					
Н/Ј1	Lintel	0	Interior	Isolated Mechanical Damage					
11/31	Linter		Exterior	Isolated Heavy Vertical Cracking - (2no )					
J/K1	Lintel	0	Interior	Visually Sound					
3/1/1	Lillei		Exterior	Isolated Heavy Vertical Cracking - (4no )					
K/L1	Lintel	0	Interior	Visually Sound					
N/ LI	Lillei		Exterior	Isolated Heavy Vertical Cracking - (2no )					
L/M1	Lintel	0	Interior	Flaking Paint Obscuring View					
<i>L</i> / WII	Lillei		Exterior	Isolated Heavy Vertical Cracking - (3no )					
M/N1	Lintel	0	Interior	Heavy Horizontal & Moderate Vertical Cracking - ( )					
171/141	Linter		Exterior	Isolated Heavy Vertical Cracking - (4no )					



Element Ref:	Туре	Level	Face	Notes	Face-by- Face RAG Rating	Combined RAG Rating	
N/4 /2	Linkal		Interior	Fine Vertical Cracking - ( )			
N1/2	Lintel	0	Exterior	Isolated Heavy Vertical Cracking - (4no )			
N2/2	line al	0	Interior	Moderate Vertical Cracking - ( )			
N2/3	Lintel		Exterior	Isolated Moderate Vertical Cracking - (5no )		]	
N12 /4	Lintel	0	Interior	Cracked Render & Saturation			
N3/4	Lintei		Exterior	Isolated Moderate Vertical Cracking - (4no )		]	
NIA/E	Lintel	0	Interior	Visually Sound			
N4/5	Lintei		Exterior	Isolated Heavy Vertical Cracking - (4no )			
NE /C	Lintal	0	Interior	Visually Sound + Saturation			
N5/6	Lintel	0	Exterior	Visually Sound			
NC/7	Lintal	0	Interior	Visually Sound			
N6/7	Lintel		Exterior	Isolated Heavy Vertical Cracking - (4no )			
N7/0	Lintal	0	Interior	Fine Vertical Cracking - ( )			
N7/8	Lintel	0	Exterior	Isolated Heavy Vertical Cracking - (4no )			
N8/9	Lintal	Lintel 0	Interior	Fine Vertical Cracking - ( )			
140/3	Lintel	201		Exterior	Isolated Heavy Vertical Cracking - (4no )		
N9/10	Linkal	Lintel	0	Interior	Visually Sound		
N9/10	Linter		Exterior	Isolated Heavy Vertical Cracking - (2no )			
M/N10	Lintel	0	Interior	Moderate Vertical Cracking - ( )			
IVI/IVIO	Linter		Exterior	Isolated Fine Vertical Cracking - (3no )			
L/M10	Lintel	0	Interior	Moderate Vertical Cracking - (4no )			
L/WIIO	Linter	U	Exterior	Isolated Heavy Vertical Cracking - (3no )			
K/L10	Lintel	0	Interior	Heavy Vertical Cracking - (3no )			
NYLIO	Linter		Exterior	Isolated Heavy Vertical Cracking - (2no )			
J/K10	Lintel	0	Interior	Moderate Vertical & Horizontal Cracking - ( )			
3/110	Liillei		Exterior	Isolated Heavy Vertical Cracking - (2no )			
H/J10	Lintel	0	Interior	Fine Vertical Cracking - ( )			
11/310	Lillei		Exterior	Isolated Heavy Vertical Cracking - (1no )			
G/H10	Lintel	0	Interior	Visually Sound			
3/1110	Linter		Exterior	Isolated Moderate Vertical Cracking - (2no )			



Element Ref:	Туре	Level	Face	Notes	Face-by- Face RAG Rating	Combined RAG Rating	
F/C10	Linkal		Interior	Fine Vertical Cracking - (2no )			
F/G10	Lintel	0	Exterior	Isolated Fine Vertical Cracking - (1no )			
F/F10	Lintal	0	Interior	Visually Sound			
E/F10	Lintel	0	Exterior	Isolated Moderate Vertical Cracking - (1no )		]	
D/F10	Lintal	0	Interior	Fine Vertical Cracking - (1no )			
D/E10	Lintel	0	Exterior	Isolated Moderate Vertical Cracking - (2no )		]	
D/F4	Link I	0	Interior	Mechanical Damage			
D/E4	Lintel	0	Exterior	Isolated Moderate Vertical Cracking - (1no )		]	
F /F4		Interior	Visually Sound				
E/F4	Lintel	0	Exterior	Isolated Fine Vertical Cracking - (2no )			
E/CA	Lintal	0	Interior	Localised Fine Vertical Cracking - ( )			
F/G4	Lintel 0	F/G4 Lintel	Exterior	Visually Sound			
C/UA	Lintal	0	Interior	Fine Vertical Cracking - ( )			
G/H4	H4 Lintel	0	Exterior	Isolated Fine Vertical Cracking - (1no )		]	
Н/Ј4	Lintal	Lintel 0	Interior	Visually Sound			
11/34	Linter		Exterior	Isolated Moderate Vertical Cracking - (3no )			
J/K4	linkal.	Lintel	0	Interior	Fine Vertical Cracking - ( )		
J/ K4	Linter		Exterior	Isolated Moderate Vertical Cracking - (1no )			
K4/5	Lintel	0	Interior	Visually Sound			
K4/3	Linter		Exterior	Visually Sound			
K5/6	Lintel	0	Interior	Visually Sound			
K5/6	Linter		Exterior	Visually Sound			
K6/7	Lintel	0	Interior	Visually Sound			
KO/7	Linter		Exterior	Isolated Moderate Vertical Cracking - (3no )			
J/K7	Lintal	0	Interior	Moderate Vertical Cracking - ( )			
J/K/	Lintel		Exterior	Isolated Fine Vertical Cracking - (1no )			
Н/Ј7	Lintal	0	Interior	Visually Sound			
U/1/	Lintel	Lintel 0	Exterior	Isolated Fine Vertical Cracking - (1no )			
G/UZ	Lintal	0	Interior	Visually Sound			
G/H7	Lintel		Exterior	Isolated Fine Vertical Cracking - (1no )			



Element Ref:	Туре	Level	Face	Notes	,	Combined RAG Rating
E/G7	F/G7 Lintel	0	Interior	Mechanical Damage		
1707			Exterior	Isolated Moderate Vertical Cracking - (2no )		
E/F7	Linkal	ntel 0	Interior	Fine Vertical Cracking - (3no )		
2/17	Linter		Exterior	Visually Sound		
D/E7	Lintel	0	Interior	Visually Sound		
D/E/		J	Exterior	Visually Sound		



Element Ref:	Туре	Level	Face	Notes	Face-by- Face RAG Rating	Combined RAG Rating
			Interior	Isolated Heavy Vertical Cracking - ( )		
A3/4	Lintel	1	Exterior	Isolated Moderate Vertical Cracking - (2no )		
/ .			Interior	Visually Sound		
A2/3	Lintel	Lintel 1	Exterior	Isolated Heavy Vertical Cracking - (5no )		
44/2			Interior	Isolated Heavy Vertical Cracking & Localised Spall - ( )		
A1/2	Lintel	1	Exterior	Isolated Heavy Vertical Cracking - (3no )		
. /	Lintol		Interior	Heavy Vertical Cracking - (2no )		
A/B1	Lintel	1	Exterior	Visually Sound		
D/04	Lintel 1		Interior	Moderate Vertical Cracking - (2no )		
B/C1	Lintei	1	Exterior	Isolated Moderate Vertical Cracking - (1no )		
C/D4			Interior	Isolated Heavy Vertical Cracking - ( )		
C/D1	Lintel	1	Exterior	Visually Sound		
D/54	D/E1 Lintel		Interior	Isolated Heavy Vertical Cracking - ( )		
D/E1		1	Exterior	Isolated Heavy Vertical & Horizontal Cracking - (3no )		
5/54		1	Interior	Isolated Moderate Vertical Cracking - ( )		
E/F1	Lintel	1	Exterior	Visually Sound		
F/C4	Lintal	Lintel 1	Interior	Visually Sound		
F/G1	Lintei	1	Exterior	Visually Sound		
C/U1	Lintal	1	Interior	Isolated Moderate Vertical Cracking - ( )		
G/H1	Lintel	1	Exterior	Isolated Fine Vertical Cracking - (3no )		
H/J1	Lintel		Interior	Isolated Heavy Vertical Cracking - (3no )		
П/ЛІ	Linter	1	Exterior	Isolated Moderate Vertical Cracking - (1no )		
1/1/1	Lintel	1	Interior	Isolated Moderate Vertical Cracking - ( )		
J/K1	Linter	1	Exterior	Isolated Moderate Vertical Cracking - (2no )		
K/L1	Lintel	1	Interior	Isolated Heavy Vertical Cracking - ( )		
N/LI	Linter		Exterior	Isolated Moderate Vertical Cracking - (2no )		
L/M1	Lintel	1	Interior	Moderate Vertical Cracking - (1no )		
L/ IVII	Linter	1	Exterior	Isolated Moderate Vertical Cracking - (1no )		
M/N1	Lintel	1	Interior	Obscured from view		
141/141	Linter		Exterior	Isolated Heavy & Moderate Vertical Cracking - (4no )		



Element Ref:	Туре	Level	Face	Notes	Face-by- Face RAG Rating	Combined RAG Rating	
N/4 /2	Linkal		Interior	Obscured from view			
N1/2	Lintel	1	Exterior	Crazing of Render			
N/2 /2			Interior	Isolated Heavy Vertical & Horizontal Cracking - ( )			
N2/3	Lintel	1	Exterior	Isolated Heavy Vertical Cracking - (4no )			
NI2/4	Linkal		Interior	Moderate Vertical Cracking - ( )			
N3/4	Lintel	1	Exterior	Isolated Heavy Vertical Cracking - (3no )			
NA/E	Lintel	1	Interior	Visually Sound			
N4/5	Lintei	1	Exterior	Isolated Heavy Vertical Cracking - (3no )			
NE/C	Lintal	1	Interior	Visually Sound			
N5/6	Lintel	1	Exterior	Visually Sound			
N6/7		1	Interior	Isolated Moderate Vertical Cracking - ( )			
N6/7	Lintel	1	Exterior	Isolated Heavy Vertical Cracking - (4no )			
N17/0	Lintal	1	Interior	Isolated Moderate Vertical Cracking - (1no )			
N7/8	Lintel 1	1	Exterior	Isolated Heavy Vertical Cracking - (1no )			
N8/9	Lintal	Lintel 1	Interior	Visually Sound			
140/3	Lintel	1	Exterior	Isolated Heavy Vertical Cracking - (3no )			
N9/10	Linkal	Lintel	1	Interior	Isolated Moderate Vertical Cracking - (2no )		
N9/10	Linter	1	Exterior	Isolated Heavy Vertical Cracking - (3no )			
M/N10	Lintel	1	Interior	Isolated Moderate Vertical Cracking - (3no )			
WIJIVIO	Linter	1	Exterior	Visually Sound			
L/M10	Lintel	1	Interior	Visually Sound			
L/WIIO	Linter	1	Exterior	Isolated Heavy Vertical Cracking - (3no )			
K/L10	Lintel	1	Interior	Visually Sound			
NYLIO	Linter	1	Exterior	Visually Sound			
J/K10	Lintel	1	Interior	Isolated Moderate Vertical Cracking - (1no )			
3/1110	Lintel		Exterior	Isolated Fine Vertical Cracking - (1no )			
H/J10	Lintel	1	Interior	Isolated Heavy Vertical Cracking - (1no )			
.,,,20	2		Exterior	Visually Sound			
G/H10	Lintel	1	Interior	Isolated Heavy Vertical Cracking - (4no )			
5/1110	LIIICI		Exterior	Isolated Moderate Vertical Cracking - (1no )			



Element Ref:	Туре	Level	Face	Notes	Face-by- Face RAG Rating	Combined RAG Rating			
E/C12	المسار	1	Interior	Isolated Heavy Vertical Cracking - (3no )					
F/G10	Lintel	1	Exterior	Visually Sound					
5/540		1	Interior	Isolated Heavy Vertical Cracking - (3no )					
E/F10	Lintel		Exterior	Visually Sound					
D/F10	Lintal	1	Interior	Isolated Heavy Vertical Cracking - (2no )					
D/E10	Lintel	1	Exterior	Visually Sound					
D/E4	Lintel	1	Interior	Isolated Moderate Vertical Cracking - (2no )					
D/E4	Linter	1	Exterior	Isolated Moderate Vertical Cracking - (1no )					
E /E /	Line 1	Lintel 1	Interior	Isolated Heavy Vertical Cracking - (3no )					
E/F4	Linter	1	Exterior	Isolated Moderate Vertical Cracking - (3no )					
F/G4	Lintal	1	Interior	Isolated Moderate Vertical Cracking - (3no )					
r/U4	Lintel 1	Linter	Linter	1	Exterior	Isolated Moderate Vertical Cracking - (4no )			
G/H4	Lintal	Lintel 1	Interior	Isolated Moderate Vertical Cracking - (2no )					
G/H4	Linter		Exterior	Visually Sound					
Н/Ј4	Lintel	1	Interior	Isolated Moderate Vertical Cracking - (4no )					
11/34	Lintel	1	Exterior	Isolated Fine Vertical Cracking - (1no )					
J/K4	Lintel	Lintel	Lintel	Lintel	1	Interior	Isolated Moderate Vertical Cracking - (2no )		
3/14				1	Exterior	Isolated Moderate Vertical Cracking - (1no )			
K4/5	Lintel	1	Interior	Visually Sound					
14/3	Linter	1	Exterior	Visually Sound					
K5/6	Lintel	1	Interior	Isolated Moderate Vertical Cracking - ( )					
K5/0	Linter	1	Exterior	Isolated Moderate Vertical Cracking - (2no )					
K6/7	Lintel	1	Interior	Visually Sound					
KO/7	Linter	1	Exterior	Visually Sound					
J/K7	Lintel	1	Interior	Isolated Moderate Vertical Cracking - (2no )					
3/10/	Lillei	1	Exterior	Isolated Fine Vertical Cracking - (2no )					
Н/J7	Lintel	1	Interior	Isolated Heavy Vertical Cracking - (3no )					
11/37	Lilitei	1	Exterior	Isolated Heavy Vertical Cracking - (3no )					
G/H7	Lintel	1	Interior	Obscured from view					
G/H7 Lir	Liitei	1	Exterior	Isolated Heavy Vertical Cracking - (3no )					



Element Ref:	Туре	Level	Face	Notes	Face-by- Face RAG Rating	Combined RAG Rating
F/G7	Lintel	1	Interior	Obscured from view		
F/G/	Linter		Exterior	Isolated Heavy Vertical Cracking - (2no )		
E/F7	Lintel	rel 1	Interior	Isolated Heavy Vertical Cracking - (3no )		
L/17	Lintei		Exterior	Isolated Moderate Vertical Cracking - (3no )		
D/E7 Lintel	Lintel	intel 1	Interior	Isolated Heavy Vertical Cracking - (1no )		
		Exterior	Isolated Moderate Vertical Cracking - (2no )			



Element Ref:	Туре	Level	Face	Notes	Face-by- Face RAG Rating	Combined RAG Rating
42/4	linkal.	2	Interior	Visually Sound		
A3/4	Lintel	2	Exterior	Visually Sound		
42/2	linkal.	2	Interior	Isolated Moderate Vertical Cracking - (2no )		
A2/3	Lintel	2	Exterior	Visually Sound		
A1/2	Lintel	2	Interior	Isolated Heavy Horizontal Cracking - (1no )		
A1/2	Linter	2	Exterior	Visually Sound		
A /D1	Linkal		Interior	Isolated Moderate Vertical Cracking - (2no )		
A/B1	Lintel	2	Exterior	Visually Sound		
B/C1	Lintol	Lintel 2	Interior	Isolated Moderate Vertical Cracking - (2no )		
B/CI	Linter	2	Exterior	Visually Sound		
C/D1	Linkal	2	Interior	Isolated Fine Vertical Cracking - (3no )		
C/D1	D1 Lintel	2	Exterior	Visually Sound		
D/E1	Lintel	2	Interior	Isolated Heavy Vertical Cracking - ( )		
D/EI	Linter	2	Exterior	Visually Sound		
F /F1	Linkal	2	Interior	Isolated Moderate Vertical Cracking - ( )		
E/F1	Lintel	2	Exterior	Visually Sound		
F/G1	Lintel	2	Interior	Isolated Moderate Vertical Cracking - (2no )		
r/G1	Linter	2	Exterior	Visually Sound		
G/H1	Lintel	2	Interior	Isolated Moderate Vertical Cracking - (3no )		
G/HI	Linter	2	Exterior	Visually Sound		
Н/Ј1	Lintel	2	Interior	Isolated Heavy Vertical Cracking - (2no )		
11/31	Linter	2	Exterior	Visually Sound		
J/K1	Lintel	2	Interior	Isolated Heavy Vertical Cracking - (2no )		
J/KI	Lilitei		Exterior	Visually Sound		
K/L1	Lintel	2	Interior	Visually Sound		
N/LI	Lilitei		Exterior	Visually Sound		
L/M1		2	Interior	Isolated Moderate Horizontal Cracking - (1no )		
L/ IVII	Lintel		Exterior	Visually Sound		
M/N1	Lintel	2	Interior	Isolated Heavy Vertical Cracking - ( )		
141/141	Lilitei		Exterior	Visually Sound		



Element Ref:	Туре	Level	Face	Notes	Face-by- Face RAG Rating	Combined RAG Rating
N/4 /0	line I	2	Interior	Visually Sound		
N1/2	Lintel	2	Exterior	Visually Sound		
N2/2	Lintal	2	Interior	Obscured from view		
N2/3	Lintel	2	Exterior	Visually Sound		
N2/4	Lintal	2	Interior	Isolated Heavy Vertical Cracking - (1no )		
N3/4	Lintel	2	Exterior	Visually Sound		
N4/5	Lintel	2	Interior	Isolated Heavy Vertical Cracking - (2no )		
114/5	Linter	2	Exterior	Visually Sound		
N5/6	Lintel	2	Interior	Isolated Moderate Vertical Cracking - (2no )		
เพร/ช	Lintei	2	Exterior	Visually Sound		
N6/7	7 Lintel 2	2	Interior	Isolated Heavy Vertical & Horizontal Cracking - (3no )		
140/7		2	Exterior	Isolated Moderate Vertical Cracking - (1no )		
N7/8	Lintel	2	Interior	Isolated Moderate Vertical Cracking - (1no )		
117/8	Linter		Exterior	Visually Sound		
N8/9	Lintel	2	Interior	Isolated Moderate Vertical Cracking - (1no )		
140/3	Linter	2	Exterior	Visually Sound		
N9/10	Lintel	el 2	Interior	Heavy Horizontal Cracking - ( )		
113/10	Linter	2	Exterior	Visually Sound		
M/N10	Lintel	2	Interior	Heavy Vertical & Horizontal Cracking - (2no )		
101/1010	Linter		Exterior	Visually Sound		
L/M10	Lintel	2	Interior	Heavy Vertical Cracking - (2no )		
L/ W110	Linter		Exterior	Localised Spalled Concrete - (4no)		
K/L10	Lintel	2	Interior	Visually Sound		
1,7220	2	_	Exterior	Visually Sound		
J/K10	Lintel	2	Interior	Isolated Fine Vertical Cracking - (2no )		
-,20		_	Exterior	Localised Spalled Concrete - (1no)		
Н/Ј10	Lintel	2	Interior	Visually Sound		
.,,,20		_	Exterior	Localised Spalled Concrete - (1no)		
G/H10	Lintel	2	Interior	Visually Sound		
5,.110	21661		Exterior	Visually Sound		



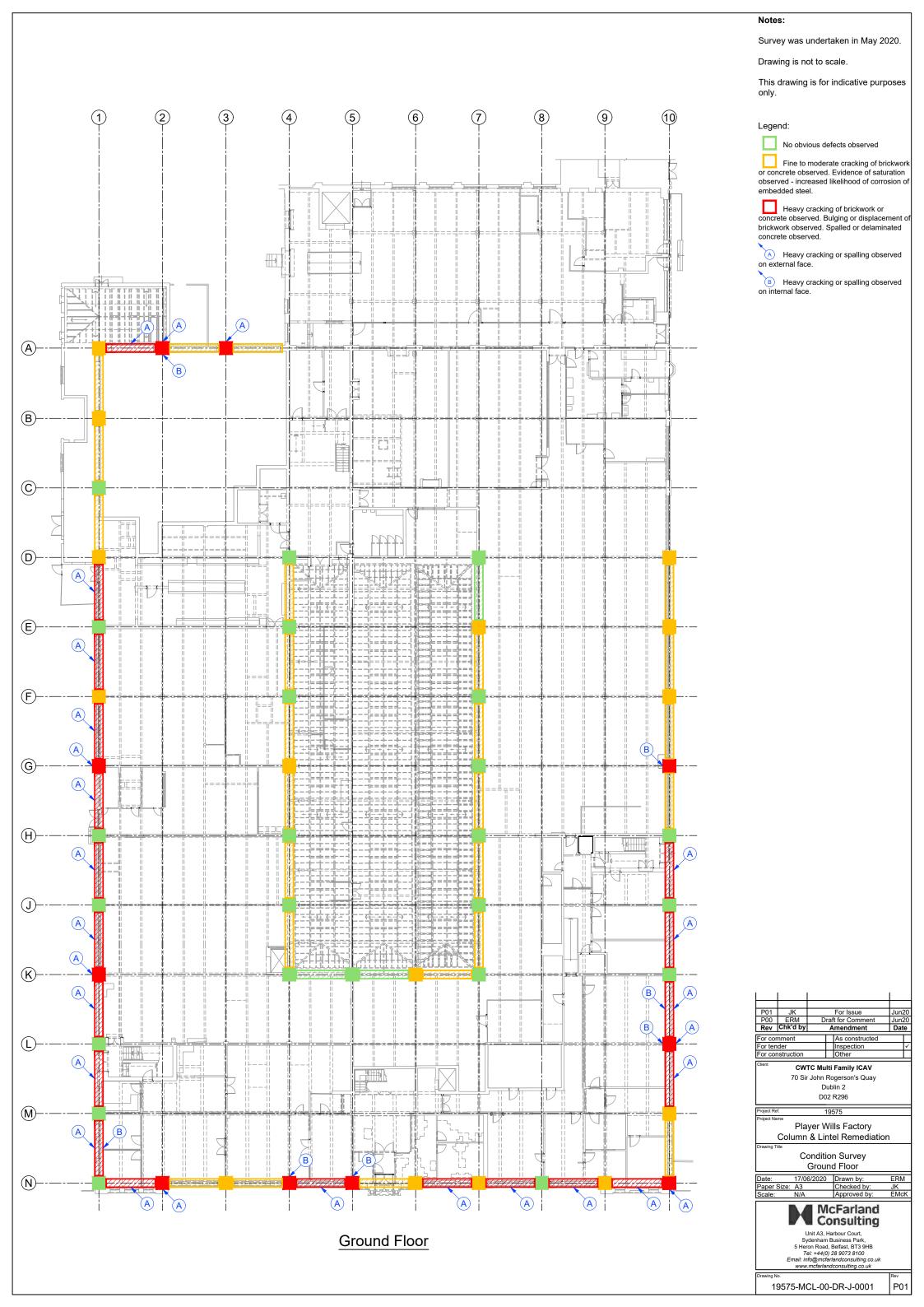
Element Ref:	Туре	Level	Face	Notes	Face-by- Face RAG Rating	Combined RAG Rating	
5/040			Interior	Isolated Fine Vertical Cracking - (1no )			
F/G10	Lintel	2	Exterior	Visually Sound			
5/540		2	Interior	Visually Sound			
E/F10	Lintel	2	Exterior	Visually Sound			
D/540		2	Interior	Visually Sound			
D/E10	Lintel	2	Exterior	Localised Spalled Concrete - (1no)			
D/54	linkal.	2	Interior	Isolated Fine Vertical Cracking - (1no )			
D/E4	Lintel	2	Exterior	Visually Sound			
E /E 4	Lintel 2	-/	2	Interior	Isolated Fine Vertical Cracking - (2no )		
E/F4	Lintei	Lintel 2	Exterior	Isolated Moderate Vertical Cracking - (3no )			
F/CA	Lintel	Lintol	2	Interior	Isolated Fine Vertical Cracking - (2no )		
F/G4		2	Exterior	Isolated Moderate Vertical Cracking - (2no )			
C/114	Linkal	2	Interior	Visually Sound			
G/H4	Lintel		Exterior	Visually Sound			
Н/Ј4	Lintol	2	Interior	Isolated Fine Vertical Cracking - (2no )			
П/Ј4	Lintel	LIIILEI	2	Exterior	Visually Sound		
J/K4	Lintel	2	Interior	Isolated Heavy & Moderate Vertical Cracking - (3no )			
J/ K4	Linter	2	Exterior	Visually Sound			
K4/5	Lintel		Interior	Visually Sound			
K4/ 3	Linter	2	Exterior	Isolated Moderate Vertical Cracking - (2no )			
K5/6	Lintel	2	Interior	Visually Sound			
K3/0	Linter	2	Exterior	Isolated Moderate Vertical Cracking - (1no )			
K6/7	Lintel	2	Interior	Visually Sound			
KO/ /	Linter	2	Exterior	Isolated Moderate Vertical Cracking - (2no )			
J/K7	Lintel	2	Interior	Visually Sound			
J/ K/	Lilitei		Exterior	Isolated Fine Vertical Cracking - (1no )			
H/J7	Lintel	2	Interior	Isolated Moderate Vertical Cracking - (3no )			
11/37	Lilitei		Exterior	Isolated Heavy Vertical Cracking - (5no )			
G/H7	Lintel	2	Interior	Visually Sound			
3/11/	LIIILEI		Exterior	Isolated Moderate Vertical Cracking - (2no )			

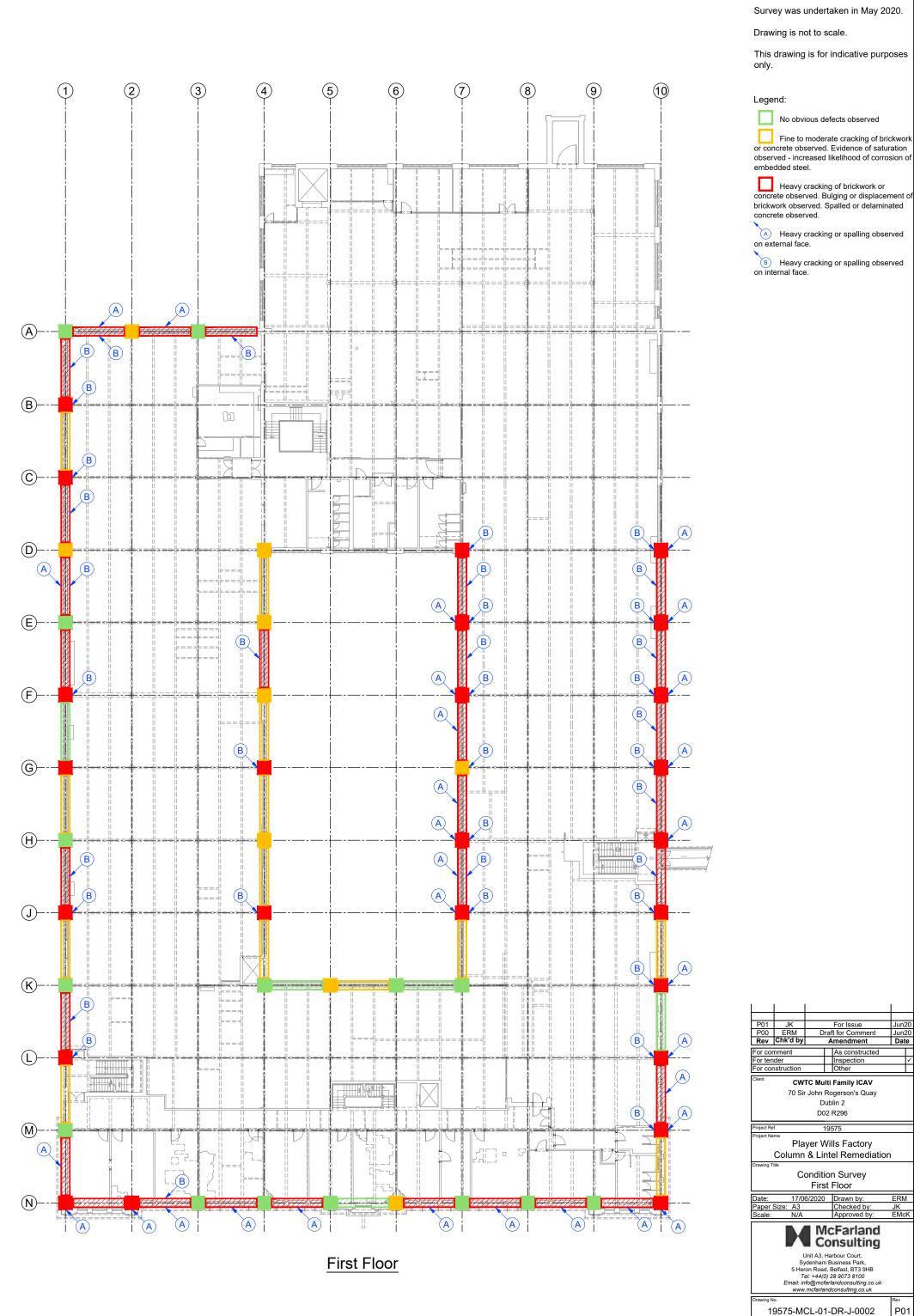


Element Ref:	Туре	Level	Face	Notes	Face-by- Face RAG Rating	Combined RAG Rating
F/G7	Lintel	2	Interior	Isolated Fine Vertical Cracking - (3no )		
			Exterior	Isolated Fine Vertical Cracking - (2no )		
E/F7	Lintel	2	Interior	Visually Sound		
			Exterior	Isolated Moderate Vertical Cracking - (2no )		
D/E7	Lintel	2	Interior	Visually Sound		
			Exterior	Isolated Moderate Vertical Cracking - (3no )		



**Appendix B – Condition Rating Plan Drawings** 



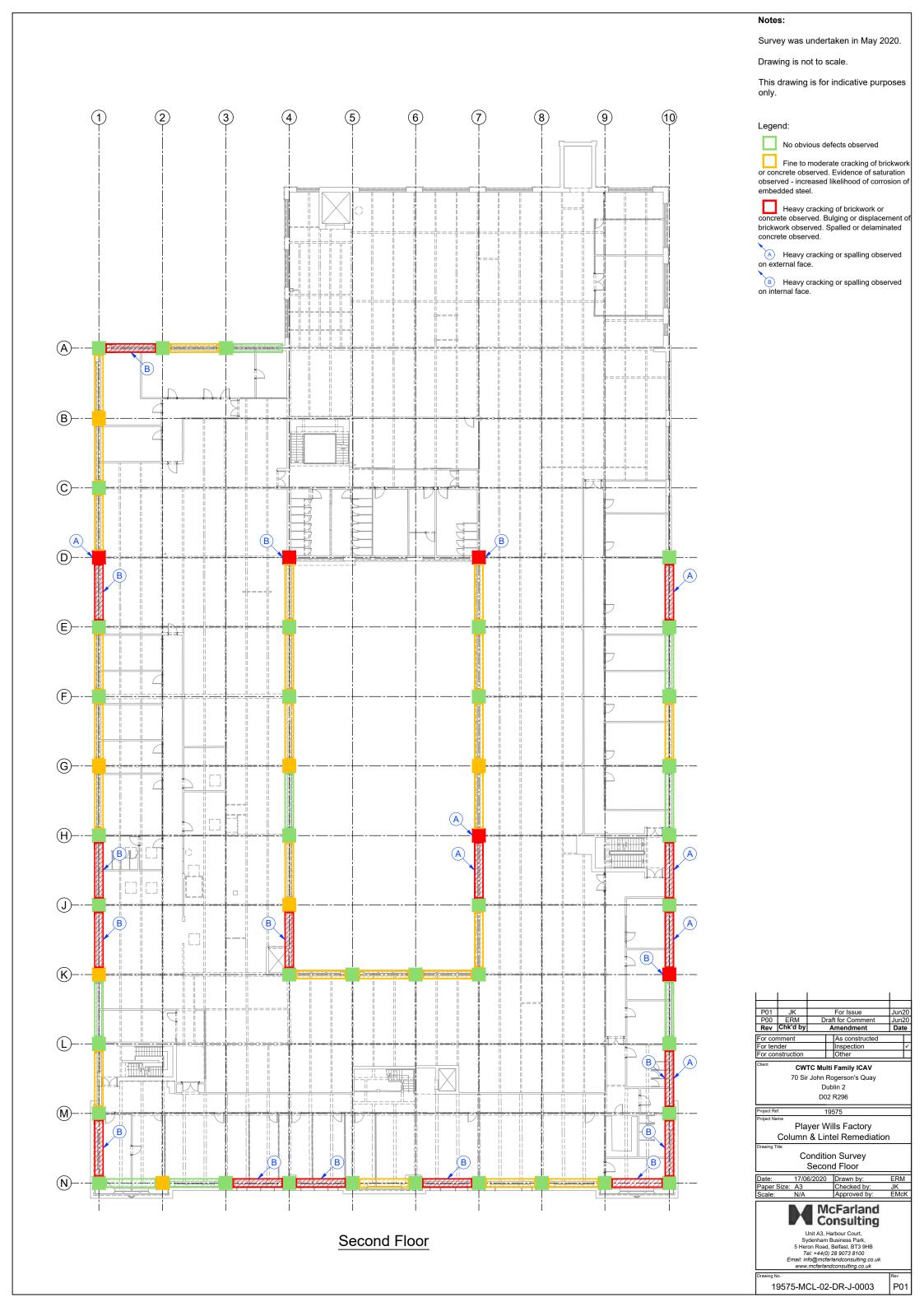


Notes:

observed - increased likelihood of corrosion of

Jun20 Date

19575-MCL-01-DR-J-0002



## Appendix F

**Load Test Solutions Material Testing** 

# Report 1510-3

Steel Investigations at former Player Wills Factory

22/05/2020



Load Test Solutions Ltd, Unit 2 Zone 5, Clonminam Business Park, Portlaoise

Ph: 057-8670629 Mobile: 087-3620086

#### CONTENTS

- 1. INTRODUCTION
- 2. SCOPE OF WORK
- 3. FINDINGS
- 4. CONCLUSION

#### **Appendices**

APPENDIX A PHOTOGRAPHS

APPENDIX B DRAWINGS

APPENDIX C STEEL HARDNESS TEST REULTS

APPENDIX D TENSILE TEST RESULTS

APPENDIX E CHEMICAL COMOSITION RESULTS



#### 1. INTRODUCTION

Load Test Solutions was requested by Barrett Mahony Consulting Engineers on behalf of their client to carry out steel investigations and testing at the former Player Wills Factory, South Circular Rd, Dublin 8.

This report presents the findings of the testing and investigation.

#### 2. SCOPE OF WORK

The scope of the works is to determine the current condition of steel within the structure through a programme of testing commensurate with testing and inspection techniques used on structures of a similar nature.

The following table shows the testing and examination schedule:

**Table 1 Test Quantities** 

Test	Beam	Column	Slab reinforcing
Tensile strength	7	8	17
Steel Hardness	15	6	N/A
Steel diameter	N/A	N/A	7
Chemical composition	2	3	3
Metallographic examination	0	1	0

#### 2.1 THE STRUCTURE

The structure on site consists of a steel and reinforced concrete structure.

#### 3. FINDINGS OF STRUCTURAL SURVEYS

The findings of the investigations are detailed below.

A photographic record is provided in Appendix A and drawings of the test areas and locations are included in Appendix B.

Site test results are given in Appendix C

Laboratory testing results are given in Appendix D



#### 3.1 STEEL THICKNESS MEASUREMENTS

A measurement of the thickness of reinforcing steel was made at the slab breakout areas. An additional measurement was recorded for reinforcing steel in a window head beam.

Measurements are noted on the drawings in Appendix B.

#### 3.2 STEEL HARDNESS TESTS

Hardness testing was carried out on-site using the Proceq Equitip 3 portable hardness tester.



Location	Min HV (Vickers)	Max HV (Vickers)	Mean HV (Vickers)
First floor main beam	99	183	133
First floor main beam	112	174	141
First floor main beam	102	162	128
First floor sec beam	84	105	91
First floor sec beam	89	137	118
First floor u column	97	149	121
First floor cast column	116	174	142
Second floor main beam	101	160	129
Second floor main beam	93	108	99
Second floor main beam	128	173	145
Second floor sec beam	86	159	108
Second floor sec beam	100	120	109
Second floor u column	99	182	143
Second floor rivet column	93	164	123
Third floor main beam	100	179	125
Third floor main beam	91	182	120
Third floor main beam	99	159	110
Third floor sec beam	86	145	105
Third floor sec beam	86	102	94
Third floor u column	84	105	91
Third floor u column	86	137	108



#### 3.3 TENSILE STRENGTH TESTS

Tensile strength tests were carried out by Sandberg LLP in accordance with ISO 6892-1:2016 B

Test results are listed in Appendix D

#### 3.4 CHEMICAL COMPOSITION TESTS

Chemical composition tests were carried out by Sandberg LLP and compared to the relevant steel standards for assessment.

Test results are listed in Appendix E



## Steel Investigations – Former Player Wills Factory

Appendix A

**Photographs** 





Beam Sample



Column Sample





**Slab Reinforcing Steel** 





**Roof Slab Reinforcing** 



Beam above windows reinforcing steel

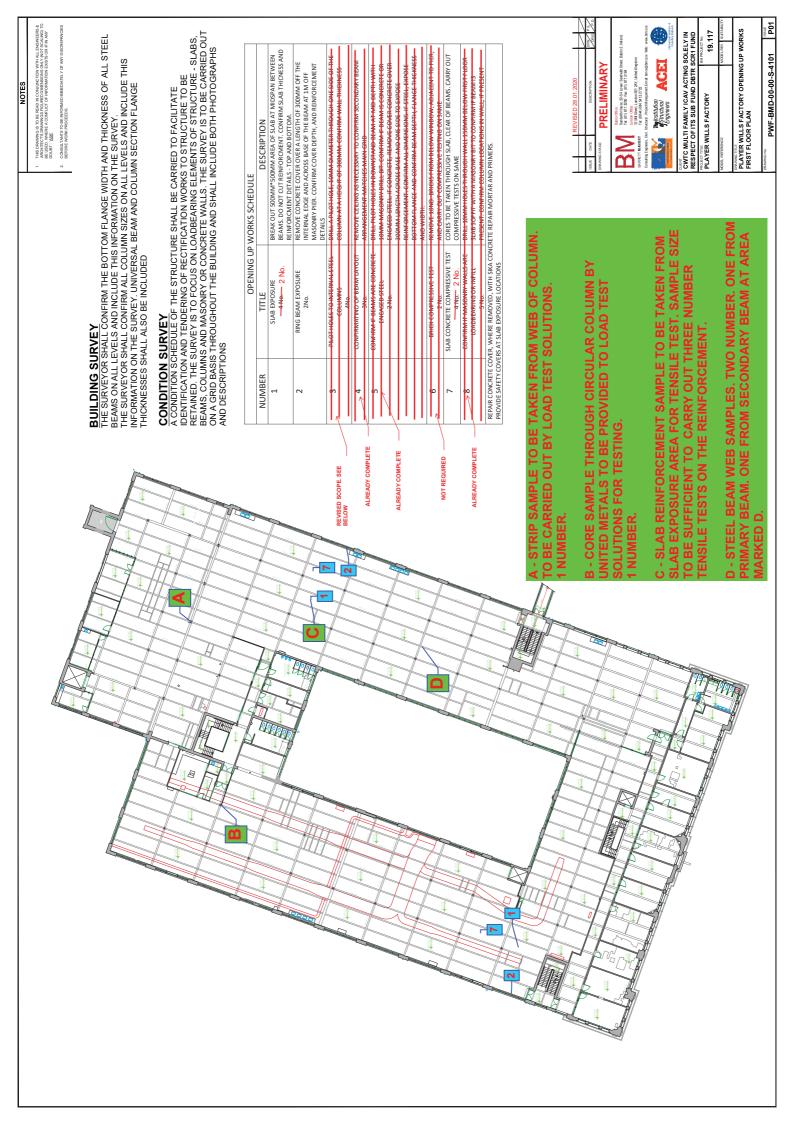


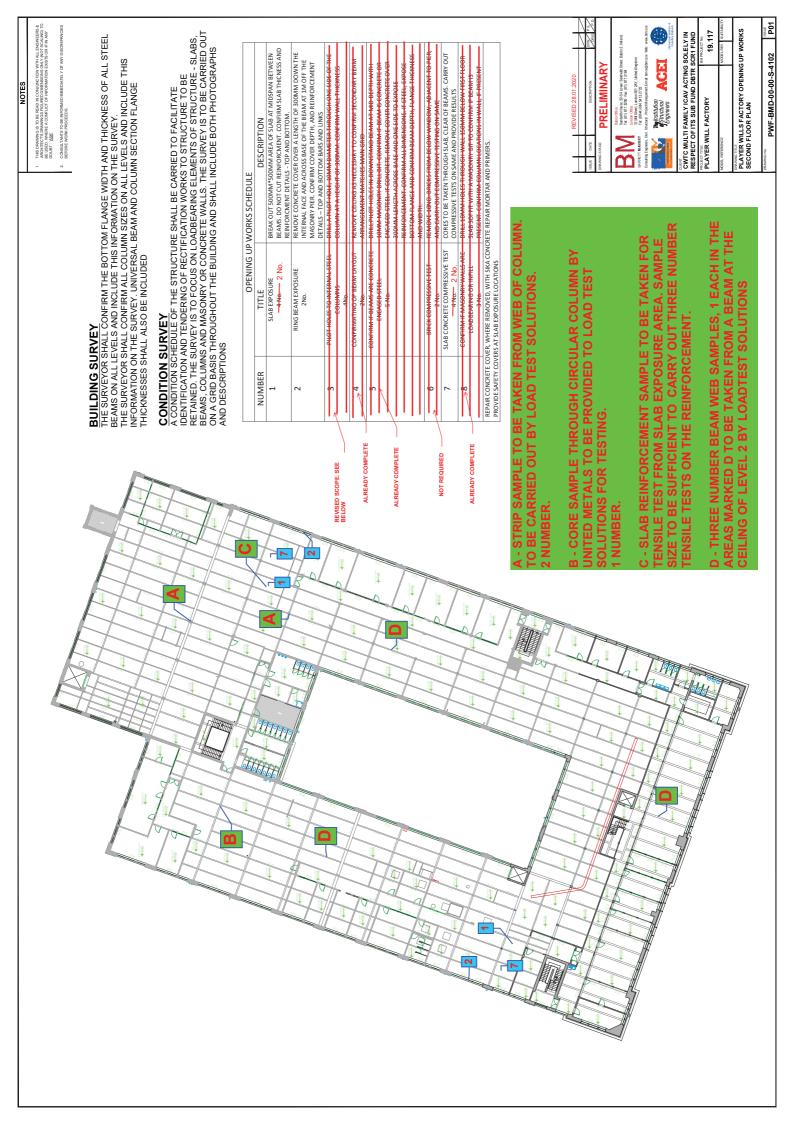
## Steel Investigations – Former Player Wills Factory

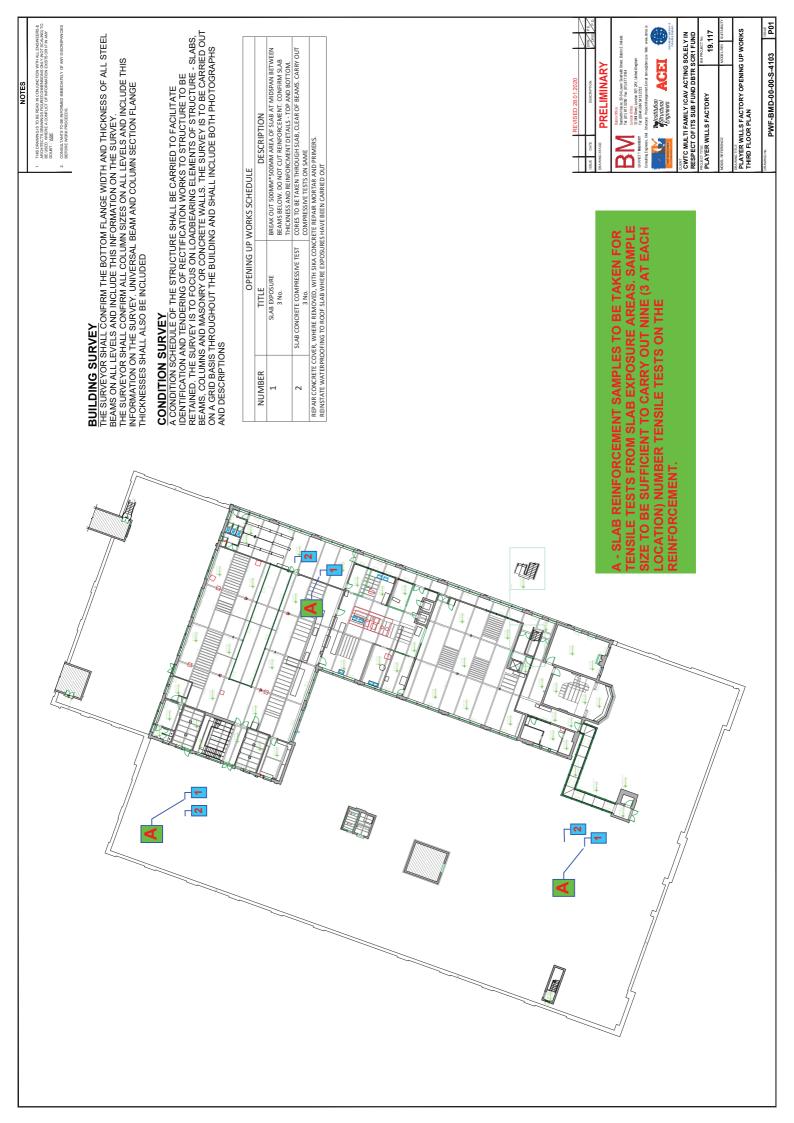
Appendix B

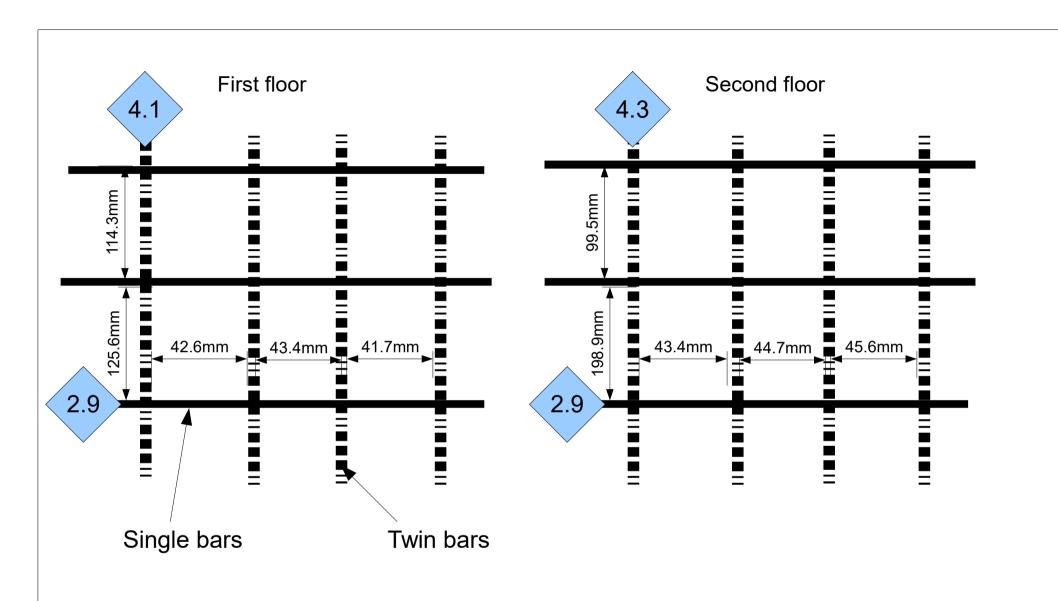
**Drawings** 









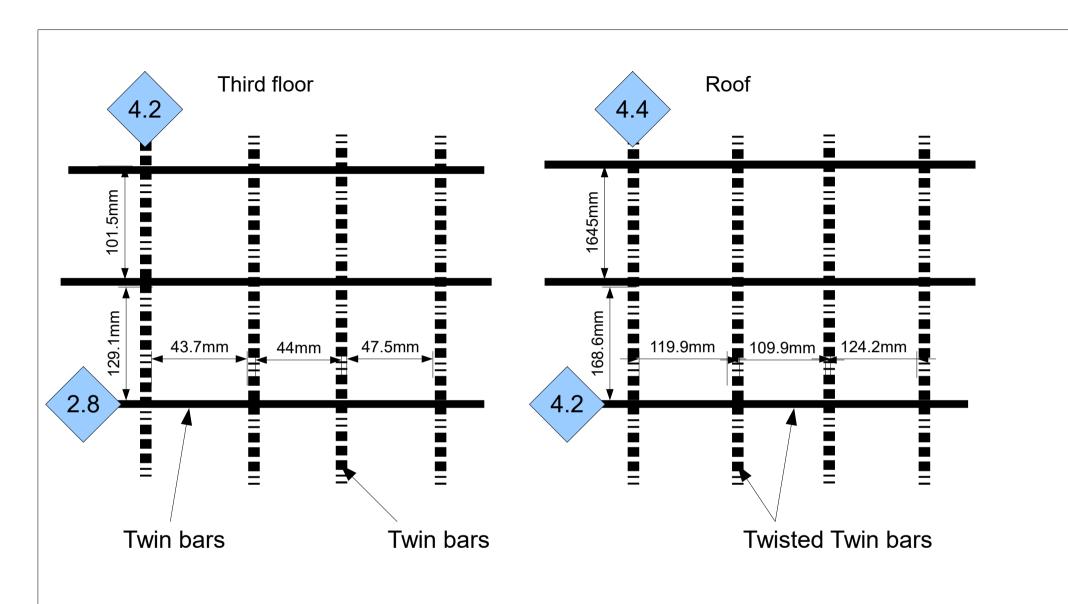




Bar size (mm) per bar



Drawn By: TF Job No. 1510 Scale: Not to scale Date: 27/05/2020

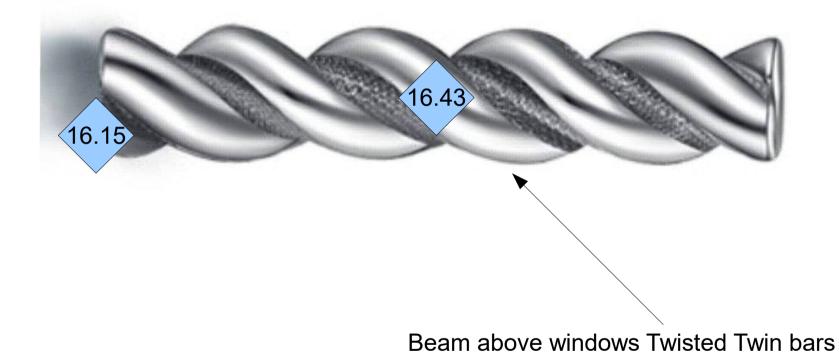


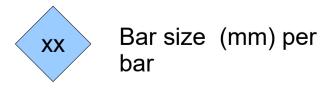


Bar size (mm) per bar



Drawn By: TF Job No. 1510 Scale: Not to scale Date: 27/05/2020







Drawn By: TF Job No. 1510 Scale: Not to scale Date: 27/05/2020

## Steel Investigations – Former Player Wills Factory

**Appendix C** 

**Steel Hardness Test Results** 



### **Steel Hardness Test Results**

Location	Min HV (Vickers)	Max HV (Vickers)	Mean HV (Vickers)
First floor main beam	99	183	133
First floor main beam	112	174	141
First floor main beam	102	162	128
First floor sec beam	84	105	91
First floor sec beam	89	137	118
First floor u column	97	149	121
First floor cast column	116	174	142
Second floor main beam	101	160	129
Second floor main beam	93	108	99
Second floor main beam	128	173	145
Second floor sec beam	86	159	108
Second floor sec beam	100	120	109
Second floor u column	99	182	143
Second floor rivet column	93	164	123
Third floor main beam	100	179	125
Third floor main beam	91	182	120
Third floor main beam	99	159	110
Third floor sec beam	86	145	105
Third floor sec beam	86	102	94
Third floor u column	84	105	91
Third floor u column	86	137	108

## Steel Investigations – Former Player Wills Factory

Appendix D

**Tensile Test Results** 







## TENSILE TEST CERTIFICATE BS EN ISO 6892-1:2016 B

Sandberg LLP 40 Grosvenor Gardens London SW1W 0EB

Tel: 020 7565 7000 Fax: 020 7565 7100 email: bo@sandberg

email: ho@sandberg.co.uk web: www.sandberg.co.uk

Certificate:	66370/M/6	Order Ref:	Proforma No. 2
Samples Received:	13 March 2020	Tested By:	АТ
Test Date:	29 April 2020	Test Procedure:	M10/3/3

Client Details: Load Test Solutions Ltd, Unit 2 Zone 5, Clonminam Business Park, Portlaoise, R32 W2RW, Co Laois, Ireland.

Spec	Specimen Reference		Uppeı	r Yield	Ultimate	e Tensile	Florentier
Met lab Ref	Sample Ref	Area mm²	Load kN	Stress N/mm²	Load kN	Stress N/mm²	Elongation %
MA 324	PB1 - Beam Web. 1 <sup>st</sup> Floor	28.65	7.60	266*	14.64	511	29.0
MA 325	SB1 - Beam Web. 1 <sup>st</sup> Floor	28.65	9.38	328	14.24	497	31.5
MA 326	2A - Col Web. 1 <sup>st</sup> Floor	29.22	8.11	278	12.60	431	37.5
MA 327	1B - Solid Col. 1 <sup>st</sup> Floor (Cored)	28.94	6.21	215*	12.72	440	16.5
MA 331	2B - Solid Col. 2 <sup>nd</sup> Floor (Cored)	28.94	5.44	188*	10.56	365	31.5
MA 332	SFSB1 - Beam Web. 2 <sup>nd</sup> Floor	29.03	9.53	328	13.68	471	35.0
Specification	on:						
BS EN 10025-2:2019 Grade S235 Grade S275 Grade S355				235 min 275 min 355 min		360-510 410-560 470-630	26 min 23 min 22 min

#### **Comments:**

The tensile properties of sample MA 324 would comply with the requirements for a grade S235 structural steel with the exception of its UTS value.

The tensile properties of samples MA 325, MA 326 and MA 332 would comply with the requirements for a grade S275 structural steel.

Cored samples MA 327 & 331 produced lower 0.2% PS results than anticipated which would not comply with any of the principle structural steel grades. These low results could be consequent of the sample's orientation when removed from the structural element, ie 90 degrees to the rolling direction.

For Sandberg LLP

Date: 4 May 2020

Neale Fetter - Assistant Manager Metallurgy Department

 $<sup>^{\</sup>ast}$  Upper yield phenomenon was not exhibited, therefore the 0.2% Proof Stress value has been reported instead.





## TENSILE TEST CERTIFICATE BS EN ISO 6892-1:2016 B

Sandberg LLP 40 Grosvenor Gardens London SW1W 0EB

Tel: 020 7565 7000 Fax: 020 7565 7100

email: ho@sandberg.co.uk web: www.sandberg.co.uk

Certificate:	66370/M/7	Order Ref:	Proforma No. 2
Samples Received:	13 March 2020	Tested By:	АТ
Test Date:	29 April 2020	Test Procedure:	M10/3/3

Client Details: Load Test Solutions Ltd, Unit 2 Zone 5, Clonminam Business Park, Portlaoise, R32 W2RW, Co Laois, Ireland.

Spec	imen Reference	_	Upper Yield		Ultimate	e Tensile	F1
Met lab Ref	Sample Ref	Area mm²	Load kN	Stress N/mm²	Load kN	Stress N/mm²	Elongation %
MA 333	SFSB2 - Beam Web. 2 <sup>nd</sup> Floor	28.94	9.19	318	13.78	476	31.5
MA 334	SFSB3 - Beam Web. 2 <sup>nd</sup> Floor	28.94	8.12	281	12.28	425	37.5
MA 335	SFC1 - Col Web. 2 <sup>nd</sup> Floor	29.22	9.80	336	12.78	437	34.0
MA 336	SFC2 - Col Web. 2 <sup>nd</sup> Floor	29.42	9.96	339	11.76	400	37.5
Specification	Specification:						
	BS EN 10025-2:2019 Grade S235			235 min		360-510	26 min
	Grade S275			275 min		410-560	23 min
	Grade S355			355 min		470-630	22 min

**Comments:** The tensile properties of samples MA 333, MA 334, MA 335 and MA 336 would comply

with the requirements for a grade S275 structural steel with the exception of the UTS value for sample MA 226

for sample MA 336.

For Sandberg LLP Date: 4 May 2020

Neale Fetter - Assistant Manager Metallurgy Department





#### **TENSILE TEST CERTIFICATE** BS EN ISO 6892-1:2016 B

Sandberg LLP 40 Grosvenor Gardens London SW1W 0EB

Tel: 020 7565 7000 Fax: 020 7565 7100

email: ho@sandberg.co.uk web: www.sandberg.co.uk

Certificate:	66370/M/8	Order Ref:	Proforma No. 2
Samples Received:	13 March 2020	Tested By:	NAF
Test Date:	27-28 April 2020	Test Procedure:	M10/3/3

**Client Details:** Load Test Solutions Ltd, Unit 2 Zone 5, Clonminam Business Park, Portlaoise, R32 W2RW, Co Laois, Ireland.

Spec	imen Reference		0.2% Proof Stress		Ultimate Tensile		Flancation
Met lab Ref	Sample Ref	Area mm²	Load kN	Stress N/mm <sup>2</sup>	Load kN	Stress N/mm <sup>2</sup>	Elongation %
MA 328- 1	SFS1 - RC Slab. 1 <sup>st</sup> Floor	12.88	7.62	592	7.76	603	17.5
MA 328- 2	SFS1 - RC Slab. 1 <sup>st</sup> Floor	13.07	7.84	600	8.17	625	17.5
MA 328- 3	SFS1 - RC Slab. 1 <sup>st</sup> Floor	13.07	8.35	639	8.70	665	N/D*
MA 329- 1	SFS1 - RC Slab. 2 <sup>nd</sup> Floor	13.07	8.08	618	8.12	621	15.0
MA 329- 2	SFS1 - RC Slab. 2 <sup>nd</sup> Floor	12.82	8.18	638	8.26	644	15.0
MA 329- 3	SFS1 - RC Slab. 2 <sup>nd</sup> Floor	12.88	7.84	609	8.13	631	17.5

**Comments:** 

\* Elongation not determined - final fracture occurred outside gauge length. Results for the above samples of steel reinforcing wire strand were not assessed for strength grade. This was because no specific client specification was supplied or identified for assessment purposes.

For Sandberg LLP



Date: 4 May 2020





## TENSILE TEST CERTIFICATE BS EN ISO 6892-1:2016 B

Sandberg LLP 40 Grosvenor Gardens London SW1W 0EB

Tel: 020 7565 7000 Fax: 020 7565 7100

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Certificate:	66370/M/9	Order Ref:	Proforma No. 2
Samples Received:	13 March 2020	Tested By:	NAF
Test Date:	27-28 April 2020	Test Procedure:	M10/3/3

Client Details: Load Test Solutions Ltd, Unit 2 Zone 5, Clonminam Business Park, Portlaoise, R32 W2RW, Co Laois, Ireland.

Spec	imen Reference	A	0.2% Proof Stress		Ultimate	e Tensile	Flamastian
Met lab Ref	Sample Ref	Area mm²	Load kN	Stress N/mm <sup>2</sup>	Load kN	Stress N/mm²	Elongation %
MA 330- 1	SFS2 - RC Slab. 2 <sup>nd</sup> Floor	12.95	8.16	630	8.32	643	15.0
MA 330- 2	SFS2 - RC Slab. 2 <sup>nd</sup> Floor	12.82	8.14	635	8.33	650	17.5
MA 330- 3	SFS2 - RC Slab. 2 <sup>nd</sup> Floor	12.38	7.91	639	8.04	650	15.0
MA 337- 1	R1 - RC Slab. 3 <sup>rd</sup> Floor	13.27	7.12	537	8.76	660	15.0
MA 337- 2	R1 - RC Slab. 3 <sup>rd</sup> Floor	13.33	7.12	534	8.82	662	14.0
MA 337- 3	R1 - RC Slab. 3 <sup>rd</sup> Floor	13.14	7.53	573	8.58	653	17.5

**Comments:** Results for the above samples of steel reinforcing wire strand were not assessed for strength grade. This was because no specific client specification was supplied or identified for assessment purposes.

For Sandberg LLP Date: 4 May 2020





## TENSILE TEST CERTIFICATE BS EN ISO 6892-1:2016 B

Sandberg LLP 40 Grosvenor Gardens London SW1W 0EB

Tel: 020 7565 7000 Fax: 020 7565 7100

email: ho@sandberg.co.uk web: www.sandberg.co.uk

Certificate:	66370/M/10	Order Ref:	Proforma No. 2
Samples Received:	13 March 2020	Tested By:	NAF
Test Date:	27-28 April 2020	Test Procedure:	M10/3/3

Client Details: Load Test Solutions Ltd, Unit 2 Zone 5, Clonminam Business Park, Portlaoise, R32 W2RW, Co Laois, Ireland.

Speci	imen Reference		0.2% Pro	of Stress	Ultimate	e Tensile	Flancation
Met lab Ref	Sample Ref	Area mm²	Load kN	Stress N/mm <sup>2</sup>	Load kN	Stress N/mm <sup>2</sup>	Elongation %
MA 338- 1	R2 - RC Slab. 3 <sup>rd</sup> Floor	12.63	4.94	391	5.69	451	22.5
MA 338- 2	R2 - RC Slab. 3 <sup>rd</sup> Floor	12.63	4.85	384	5.73	454	N/D*
MA 339- 1	R3 - RC Slab. 3 <sup>rd</sup> Floor	12.38	8.79	710	8.99	727	14.0
MA 339- 2	R3 - RC Slab. 3 <sup>rd</sup> Floor	12.44	8.87	713	9.02	725	15.0
MA 339- 3	R3 - RC Slab. 3 <sup>rd</sup> Floor	12.44	8.76	704	8.99	723	12.5

Comments:

\* Elongation not determined - final fractured occurred within the test machines grips. Results for the above samples of steel reinforcing wire strand were not assessed for strength grade. This was because no specific client specification was supplied or identified for assessment purposes.

For Sandberg LLP



Date: 4 May 2020





## TENSILE TEST CERTIFICATE BS EN ISO 6892-1:2016 B

Sandberg LLP 40 Grosvenor Gardens London SW1W 0EB

Tel: 020 7565 7000 Fax: 020 7565 7100

email: ho@sandberg.co.uk web: www.sandberg.co.uk

Certificate:	66370/M/3	Order Ref:	Email dated 26/09/2019
Samples Received:	28 October 2019	Tested By:	AT
Test Date:	01 November 2019	Test Procedure:	M10/3/3

**Client Details:** Load Test Solutions Ltd, Unit 2 Zone 5, Clonminam Business Park, Portlaoise, R32 W2RW, Co Laois, Ireland.

Speci	imen Reference		0.2%	Proof	Ultimate	e Tensile	
Met lab Ref	Sample Ref	Area mm²	Load kN	Stress N/mm²	Load kN	Stress N/mm²	Elongation %
MZ 1012	Main Beam	28.56	7.20	252	13.18	462	35.0
MZ 1013	Beam 2	28.46	7.47	263	14.46	508	32.5
MZ 1014	Column	28.56	7.41	260	11.88	416	36.5
MZ 1015	Col B/P	29.22	7.61	261	13.88	475	28.5
Specification							
	BS EN 10025-2:2019 Grade S235 Grade S275 Grade S355			235 min 275 min 355 min		360-510 410-560 470-630	26 min 23 min 22 min

**Comments:** The tensile properties for samples MZ 1012, MZ 1013, MZ 1014 and MZ 1015 all conformed

to the structural steel grade \$235.

For Sandberg LLP Date: 5 November 2019





## TENSILE TEST CERTIFICATE BS EN ISO 6892-1:2016 B

Sandberg LLP 40 Grosvenor Gardens London SW1W 0EB

Tel: 020 7565 7000 Fax: 020 7565 7100

email: ho@sandberg.co.uk web: www.sandberg.co.uk

Certificate:	66370/M/4	Order Ref:	Email dated 6/12/2019
Samples Received:	20 December 2019	Tested By:	NAF
Test Date:	02 January 2020	Test Procedure:	M10/3/3
Client Details:	Load Test Solutions Ltd, Unit 2 W2RW, Co Laois, Ireland.	Zone 5, Clonminam B	usiness Park, Portlaoise, R32

Spec	imen Reference		0.2%	Proof	Ultimate	e Tensile	Elementies
Met lab Ref	Sample Ref	Area mm²	Load kN	Stress N/mm²	Load kN	Stress N/mm²	Elongation %
MZ 1251	Column Sample 7mm Dia. 75mm Iong	19.09	4.280	225	7.60	398	18.0
Specification	on: BS EN 10025-2:2019 Grade S185 Grade S235 Grade S275 Grade S355			185 min 235 min 275 min 355 min		290-510 360-510 410-560 470-630	18 min 26 min 23 min 22 min

**Comments:** The tensile properties for samples MZ 1251 conformed to the structural steel grade S185.

For Sandberg LLP Date: 9 January 2020

Neale Fetter - Assistant Manager - Metallurgy Department

## Steel Investigations – Former Player Wills Factory

Appendix E

**Chemical Composition Results** 





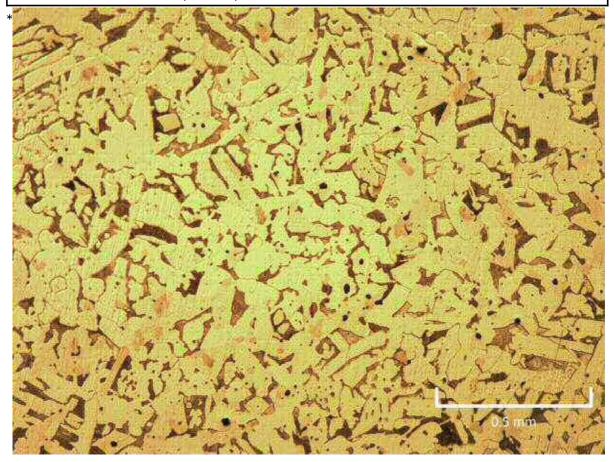


## TEST CERTIFICATE METALLOGRAPHIC EXAMINATION TO BS EN ISO 643 : 2012

Sandberg LLP 40 Grosvenor Gardens London SW1W 0EB

Tel: 020 7565 7000 Fax: 020 7565 7100 email: ho@sandberg.co.uk web: www.sandberg.co.uk

Certificate:	66370/M/5	Order Ref:	Email dated 6/12/2019
Samples Received:	20 December 2019	Tested By:	MC
Test Date:	08 January 2020	Test Procedure:	M/5/3/2 & M13/3/0
Client Details:	Load Test Solutions Ltd, Unit W2RW, Co Laois, Ireland.	2 Zone 5, Clonminam B	usiness Park, Portlaoise, R32



Met Lab Ref: MZ1 25	1		Client Ref: Column Sample	7mm Dia. 75mm long
Examined By: MC	Mag:	X84	Etchant: 2% Nital	Grain Size Index: 5.0

Comments: Metallographic examination revealed a microstructure comprising of pearlite within a ferritic matrix, with a coarse grain structure. This would be typical of that expected of a low alloy carbon steel material.

For Sandberg LLP Date: 9 January 2020

Neale Fetter - Assistant Manager- Metallurgy Department



Sandberg LLP 40 Grosvenor Gardens London SW1W 0EB Tel: 020 7565 7000 Fax: 020 7565 7100 email: ho@sandberg.co.uk web: www.sandberg.co.uk

# **TEST CERTIFICATE**

31 October 2019 OES Test Procedure: Test Date: Load Test Solutions Ltd, Unit 2 Zone 5, Clonminam Business Park, Portlaoise, R32 W2RW, Co Laois, Ireland. Metaltech Services Limited 28 October 2019 Samples Received: Tested By: Email dated 26/09/2019 66370/M/1 **Client Details:** Certificate: Reference:

				CHEMIC	CHEMICAL COMPOSITION %	% NOILIS								
Met Lab Ref	Client Description	C	!S	Mn	S	۵	ï	Cr	Мо	ŋ	>	Nb	ΙΑ	CEV
MZ 1012	Main Beam	0.10	0.02	0.48	0.022	0.011	0.10	<0.01	<0.01	0.10	<0.01	0.005	<0.01	0.199
MZ 1013	Beam 2	0.16	0.02	0.49	0.022	0.017	0.32	<0.01	<0.01	0.10	<0.01	0.005	<0.01	0.276
MZ 1014	Column	0.15	0.09	0.60	0.036	0.032	0.06	<0.01	<0.01	90.0	<0.01	0.003	<0.01	0.261
Specification:	n: BS EN 10025-2:2019 Grade S235 (max) Grade S275 (max) Grade S355 (max)	0.19 0.24 0.27	0.6	1.5	0.045 0.045 0.045	0.045 0.045 0.045				0.60				0.35
Comments	Results contained in this certificate are outside the UKAS accredit Metaltech Services Limited Report No. MSL 4945-1.	te are outs	ide the UK, 4945-1.	AS accredit	ation for this	ation for this laboratory but have been performed on our behalf by another laboratory that is so accredited.	out have be	en perforn	ned on our	rbehalfby	another lak	boratory tha	at is so acc	redited.

For Sandberg LLP

Neale Fetter - Assistant Manager Metallurgy Department

Carbon Equivalent Values (CEV) for the above samples were found to be acceptable, and as such they would be considered readily weldable using standard welding techniques

and consumables as specified in BS EN 1011: Part 2: 2001, which supersedes withdrawn standard BS 5135:1984.

Date: 5 November 2019



**TEST CERTIFICATE** 

40 Grosvenor Gardens London SW1W 0EB Sandberg LLP

email: ho@sandberg.co.uk Tel: 020 7565 7000 Fax: 020 7565 7100

web: www.sandberg.co.uk

31 October 2019 OES Test Procedure: Test Date: Load Test Solutions Ltd, Unit 2 Zone 5, Clonminam Business Park, Portlaoise, R32 W2RW, Co Laois, Ireland. Metaltech Services Limited 28 October 2019 Samples Received: Tested By: Email dated 26/09/2019 66370/M/2 Client Details: Certificate: Reference:

				CHEMIC	CHEMICAL COMPOSITION %	% NOILI								
Met Lab Ref	Client Description	C	Si	Mn	S	Ь	Ä	Ċ	Мо	c	۸	Nb	A	CEV
MZ 1015	Col B/P	0.23	0.01	0.54	0.024	0.052	0.02	<0.01	<0.01	0.02	<0.01	0.002	<0.01	0.329
Specification:	n:     BS EN 10025-2:2019     Grade S235 (max)     Grade S275 (max)     Grade S355 (max)	0.19 0.24 0.27	0.6	1.5	0.045 0.045	0.045 0.045 0.045				0.60				0.35 0.40 0.45

Comments :	Results contained in this certificate are outside the UKAS accreditation for this laboratory but have been performed on our behalf by another laboratory that is so accredited.
	Metaltech Services Limited Report No. MSL 4945-1.
	The above sample MZ 1015 gave high phosphorus content, exceeding the maximum allowable limit for modern structural steels. The CEV value for this sample is within the
	maximum allowable limits, therefore material of this quality would be considered weldable using standard welding techniques and consumables as specified in BS EN 1011
	: Part 2 : 2001, which supersedes withdrawn standard BS 5135 : 1984, however consideration for the high phosphorus content should be made.

For Sandberg LLP



Date: 5 November 2019



Sandberg LLP 40 Grosvenor Gardens London SW1W 0EB Tel: 020 7565 7000 Fax: 020 7565 7100 email: ho@sandberg.co.uk web: www.sandberg.co.uk

# **TEST CERTIFICATE**

Certificate:	66370/M/12	Samples Received:	13 March 2020	Test Date:	07 May 2020
Reference:	Proforma No. 2	Tested By:	RoTech Laboratories	Test Procedure:	ICP
Client Details:	Load Test Solutions Ltd, Unit 2 Zone 5, Clonminam Business	ie 5, Clonminam Business Park, P	Park, Portlaoise, R32 W2RW, Co Laois, Ireland.		

				CHEMI	MICAL COMPOSITION %	SITION %								
Met Lab Ref	Client Description	C	Si	Mn	S	d	Ni	Cr	Мо	no	۸	qN	ΙΑ	CEV
MA 328	SFS1 - First Floor RC Slab (Strand)	0.039	<0.01	0.39	0.071	0.053	0.04	0.01	<0.01	0.04	<0.01	<0.01	<0.003	0.115
MA 330	SFS2 - Second Floor RC Slab (Strand)	0.041	<0.01	0.51	0.052	0.045	0.04	0.01	<0.01	0.04	<0.01	<0.01	<0.003	0.137
MA 337	R1 - Third Floor RC Slab (Twisted Strand)	0.088	<0.01	0.45	0.034	0.069	0.10	0.04	0.02	0.06	<0.01	<0.01	0.003	0.188
Specification:														

Comments :	Results contained in this certificate are outside the UKAS accreditation for this laboratory but have been performed on our behalf by another laboratory that is so accredited.
	RoTech Laboratories Report No. 20-05033.
	Materials are a Carbon-Manganese steel with no intentional alloying, the Sulphur and Phosphorous levels are high for steel. If the materials are to be welded consideration
	on the low CEV, High Sulphur and Phosphorus levels must be taken. The material is not considered readily weldable according to BS EN 1011, thus it would be prudent to seek
	advice of a welding engineer prior to welding the material.

For Sandberg LLP

Neale Fetter - Assistant Manager Metallurgy Department

Date: 11 May 2020

Materials, samples and test specimens are retained for a period of 2 months from the issue of the final report. Opinions and interpretations expressed herein are outside the scope of UKAS accreditation.



Sandberg LLP 40 Grosvenor Gardens London SW1W 0EB Tel: 020 7565 7000 Fax: 020 7565 7100 email: ho@sandberg.co.uk web: www.sandberg.co.uk

# **TEST CERTIFICATE**

Certificate:	66370/M/11	Samples Received:	13 March 2020	Test Date:	14 April 2020
Reference:	Proforma No. 2	Tested By:	Metaltech Services Limited	Test Procedure:	0ES
Client Details:	Load Test Solutions Ltd, Unit 2 Zone	5, Clonminam Business Park, Po	oad Test Solutions Ltd, Unit 2 Zone 5, Clonminam Business Park, Portlaoise, R32 W2RW, Co Laois, Ireland.		

				CHEMIC	ICAL COMPOSITION %	% NOILIS								
Met Lab Ref	Client Description	C	Si	Mn	S	Ь	Ni	Cr	Мо	Cu	^	Nb	AI	CEV
MA 332	SFSB1 - Beam Web. 2 <sup>nd</sup> Floor	0.19	<0.01	0.66	0.038	0.039	0.04	<0.01 <0.01	<0.01	0.02	<0.01	<0.01	0.001	0.310
Specification:	ï													
	BS EN 10025-2:2019													
	Grade S235 (max)	0.19	ı	1.5	0.045	0.045				09.0				0.35
	Grade S275 (max)	0.24	ı	1.6	0.045	0.045				09.0				0.40
	Grade S355 (max)	0.27	9.0	1.7	0.045	0.045				09.0				0.45

Comments :	Results contained in this certificate are outside the UKAS accreditation for this laboratory but have been performed on our behalf by another laboratory that is so accredited.
	Metaltech Services Limited Report No. MSL 5402
	Carbon Equivalent Value (CEV) for the above sample was found to be acceptable, and as the material would be considered readily weldable using standard welding techniques
	and consumables as specified in BS EN 1011 : Part 2 : 2001, which supersedes withdrawn standard BS 5135 :1984.

For Sandberg LLP

Neale Fetter - Assistant Manager Metallurgy Department

Date: 4 May 2020

Materials, samples and test specimens are retained for a period of 2 months from the issue of the final report. Opinions and interpretations expressed herein are outside the scope of UKAS accreditation.



Sandberg 40 Grosvenor Gardens London SW1W 0EB

Tel: 020 7565 7000 Fax: 020 7565 7100 email: ho@sandberg.co.uk web: www.sandberg.co.uk

24 September 2020

Your Ref: Proforma Invoice Paid 02/09/20

Our Ref : 68141/M

Load Test Solutions Ltd Unit 2 Zone 5 Clonminam Business Park Portlaoise R32 W2RW

For the	attention	of Tom	Fox
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**Dear Tom** 

Re: Tensile & Metallographic Testing

Please find attached Certificates 1 to 3 including revised certificate 3 for your records.

Yours sincerely

Amy Tolladay Senior Technician - Metallurgy Department

Enc.

Materials, samples and test specimens are retained for a period of 2 months from the issue of the final report.

Your attention is drawn to the enclosed sample retention form and we would be grateful if you could complete the form and return it within one month from the date of the report.

Tests reported on sheets not bearing the UKAS mark in this report/certificate are not included in the UKAS accreditation schedule for this laboratory.

Opinions and interpretations expressed herein are outside the scope of UKAS accreditation.

This report is personal to the client, confidential, non-assignable and written with no admission of liability to any third party.

This report shall not be reproduced, except in full, without the written approval of Sandberg LLP.

Where our involvement consists exclusively of testing samples, the results and our conclusions relate only to the samples tested.



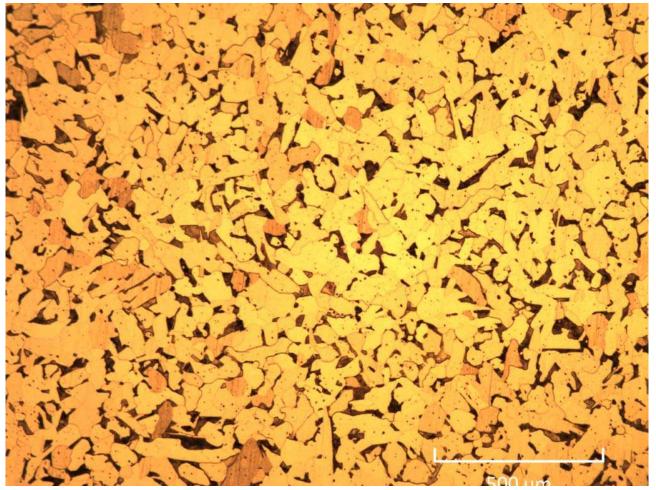


## TEST CERTIFICATE METALLOGRAPHIC EXAMINATION TO BS EN ISO 643:2020

Sandberg LLP 40 Grosvenor Gardens London SW1W 0EB

Tel: 020 7565 7000 Fax: 020 7565 7100 email: ho@sandberg.co.uk web: www.sandberg.co.uk

Certificate:	68141/M/1	Order Ref:	Proforma Paid 02.09.20			
Samples Received:	26 August 2020	Tested By:	MC			
Test Date:	11 September 2020	Test Procedure:	M5/3/2 & M13/3/0			
Client Details:	Load Test Solutions Ltd, Unit 2 Zone 5, Clonminam Business Park, Portlaoise, R32 W2RW.					



Met Lab Ref:	MA 784			Client Ref:	Col 1	
Examined By:	SET	Mag:	x 84	Etchant:	2% Nital	Grain Size Index: 6.5
Comments:	•	•				small amount of pearlite carbon, low alloy steel

For Sandberg LLP



Date: September 16, 2020



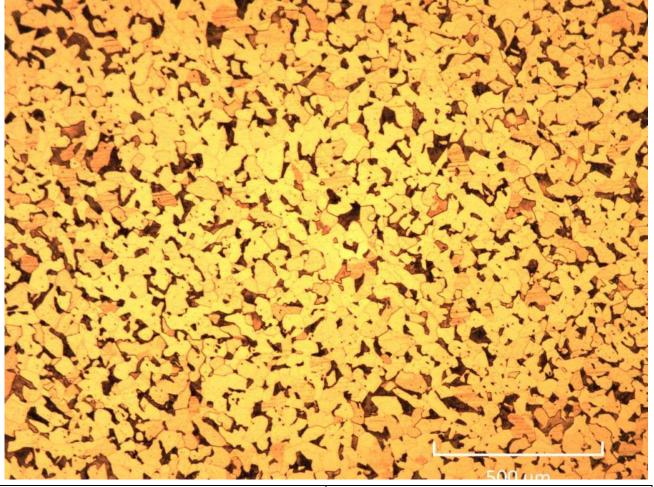


## TEST CERTIFICATE METALLOGRAPHIC EXAMINATION TO BS EN ISO 643:2020

Sandberg LLP 40 Grosvenor Gardens London SW1W 0EB

Tel: 020 7565 7000 Fax: 020 7565 7100 email: ho@sandberg.co.uk web: www.sandberg.co.uk

Certificate:	68141/M/2	Order Ref:	Proforma Paid 02.09.20		
Samples Received:	26 August 2020	Tested By:	MC		
Test Date:	11 September 2020	Test Procedure:	M5/3/2 & M13/3/0		
Client Details:	Load Test Solutions Ltd, Unit 2 Zone 5, Clonminam Business Park, Portlaoise, R32 W2RW.				



Met Lab Ref:	MA 785		c	Client Ref:	Col 2	
Examined By:	SET	Mag: x 84	E	Etchant:	2% Nital	Grain Size Index: 6.5
Comments:	•	•				small amount of pearlite carbon, low alloy steel

For Sandberg LLP



Date: September 16, 2020

#### Simon R P Morris - Senior Associate





## TENSILE TEST CERTIFICATE BS EN ISO 6892-1:2019 B

Sandberg LLP 40 Grosvenor Gardens London SW1W 0EB

Tel: 020 7565 7000 Fax: 020 7565 7100 email: ho@sandberg.co.uk web: www.sandberg.co.uk

Certificate:	68141/M/3/Rev01	Order Ref:	Proforma Paid 02.09.20				
Samples Received:	26 August 2020	Tested By:	АТ				
Test Date:	16 September 2020	Test Procedure:	M10/3/3				
Client Details:	Load Test Solutions Ltd, Unit 2 Zone 5	Load Test Solutions Ltd, Unit 2 Zone 5, Clonminam Business Park, Portlaoise, R32 W2RW.					

Spe	Specimen Reference		O.2% P		Proof Ultimate Tensile		Elongation
Met Lab Ref	Sample Ref	mm²	Load kN	Stress N/mm²	Load kN	Stress N/mm²	%
MA 784	Col 1 (From 180 mm thick solid steel column)	28.65	6.34	222	12.78	446	36.0
MA 785	Col 2 (From 160 mm thick solid steel column)	28.84	6.36	221	12.48	443	36.0
Specification	Specification:						
BS EN 1002	25-2:2019 (150-200 mm						
	thick)						
	Grade S235			185 min		340-490	21 min
	Grade S275			215 min		280-540	18 min
	Grade S355			285 min		450-600	17 min

The tensile properties of samples MA 784 and MA 785 would conform to the requirements for a grade S275 material (150 to 200 mm thick).

For Sandberg LLP Date: September 24, 2020





Sandberg LLP 40 Grosvenor Gardens London SW1W 0EB

Tel: 020 7565 7000 Fax: 020 7565 7100 email: ho@sandberg.co.uk web: www.sandberg.co.uk

## AUTHORISATION FOR THE RETENTION OF MATERIALS, SAMPLES AND TEST SPECIMENS

CLIENT:	Load Test Solutions				
DATE REPORT ISSUED:	24 September 2020	JOB NO:	68141/M		

Materials, samples and test specimens are retained for a period of 2 months from the issue of the final report. Thereafter we will either dispose of them or retain them for a further period, whichever you require. However, we cannot accept requests for indefinite retention and the maximum period of retention without review by yourselves is 6 months.

A charge is made for storage at £50 per 0.025 m³ (approximately one cubic foot) or part thereof per quarter commencing at the end of our standard 2 month retention period. You will be invoiced for the storage charges at the start of each quarterly period.

If you wish to retain them for a specified period, or if you intend to collect any of these items, please complete the form below and return it to the Grosvenor Gardens address with 1 month.

#### PLEASE KEEP UPPER HALF FOR REFERENCE

	P	LEASE COMPLETE 'A' OR 'B	' AND R	ETURN IF APPR	OPRIATE		
A.	· ·	Please RETAIN/PREPARE FOR COLLECTION* all materials.  * Delete as appropriate					
	If materials are to	o be retained please give re	tention	period			
	If materials are to	o be collected please give in	ntended	date of collection	on		
В.	If you require only certain materials, samples or test specimens to be retained or collected pleas describe them below and give retention period or intended collection date.						
		(Any material not	listed wi	ill be disposed)			
TO BE RETAINED/COLLECTED (delete as appropriate)					JOB NO:		
Con	tact Name			Signature			

Date

Company

